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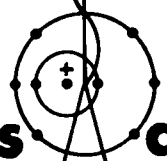
USNDC-6

INFORMAL REPORT

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Compilation of Requests for Nuclear Data

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LOS ALAMOS NATIONAL LABORATORY
3 9338 00390 2524


los alamos
scientific laboratory
of the University of California
LOS ALAMOS, NEW MEXICO 87544

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Compilation of Requests for Nuclear Data



Compiled and edited by

Leona Stewart, Michael S. Moore, and Henry T. Motz

for the

United States Nuclear Data Committee



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I. INTRODUCTION

1

This report is a working document of the U. S. Nuclear Data Committee. It contains a list of cross-section and related measurements important to the U. S. nuclear energy programs. These requests have originated from various Atomic Energy Commission agencies and contractors, Department of Defense laboratories and contractors, National Aeronautics and Space Administration laboratories and contractors, and other interested groups. Requests have also been received from the Advisory Committee on Reactor Physics (ACRP), the United States Nuclear Data Committee (USNDC), the Defense Nuclear Agency (DNA), and others.

Each request which appears in this compilation has been reviewed by subcommittees of the USNDC. In addition, those requests designated as DRDT and DNA have been reviewed by the ACRP; those designated as DCTR were reviewed by an ad-hoc Committee on Controlled Thermonuclear Research; those designated as DNA were reviewed by individuals designated by the DNA; etc.

Requesters' comments have often been edited to conserve space, hopefully without compromising the intended meaning. Status comments are the responsibility of the working subcommittees of the USNDC although editing was often required before inclusion in the final document. In compiling the status comments, the USNDC assumes that the requester has consulted the published literature and the National Neutron Cross Section Center files for available data listed in CINDA documents which are kept current and are available in all AEC depository libraries. Most references to such published literature have therefore been omitted.

This version* of the request list was produced by computer printout. The computer program was written by Myron L. Stein specifically for the MANIAC at Los Alamos. The present printout is untouched and contains slight notation problems which may be confusing. The MANIAC printer allows only a few Greek characters but it does allow overprinting; therefore Roman letters with a bar over the top are chosen to denote many of the common Greek symbols; for example, $\bar{\alpha}$ is Greek α , $\bar{\beta}$ is Greek β , $\bar{\gamma}$ is Greek γ , etc. Throughout the tables, capital σ is used for σ due to the obvious similarity between the two.

It should be noted that this reaction list was originally set up to handle neutron interactions but, at a later date, the list was amended to include other incident particles. Therefore, a channel description such as "Elastic" and "Total" always refers to incident neutrons. If a particle other than a neutron is in the incident channel, the specific particle appears under "REACTION" for each request listed.

*Future request compilations will be the responsibility of the National Neutron Cross Section Center at Brookhaven National Laboratory.

Reaction types are, for the most part, in standard notation. These requests are invariably for microscopic data, and dependence on the incident neutron energy is implied. If the request is for the measurement of a cross section as a function of angle or exit particle energy as well as incident energy, this information is given in the column labeled "REACTION TYPE-VARIABLE."

All requests are ordered by Z, A, and then by reaction type according to an ordering scheme which resembles that chosen for ENDF/B. For example, retrievals are easily made on cross sections, angular distributions, energy spectra, etc. The main body of the requests contains requests for nucleon induced reactions and scattering for energies up to 20 MeV (Table 1). Photon-induced requests are in Table 2 and medium energy requests in Table 3. All of the reaction indices are completely described and defined as prefixes to each of these tables.

ACKNOWLEDGMENTS

The editors of this compilation would like to acknowledge the work of Dr. Myron L. Stein who handled all of the computer programming and operations, and to Mrs. Jane Rasmussen, who keypunched the majority of the requests. Mrs. Juanita Gammel has conscientiously and patiently prepared the input and edited the output for this final version. To all of these people, we express our sincere appreciation.

II. PROCEDURES FOR SUBMITTING REQUESTS

Requests for measurements of nuclear data should be transmitted through the appropriate channels to the U. S. Nuclear Data Committee at which time they will be reviewed by the various USNDC subcommittees. All requests should be completely specified and transmitted in the appropriate format, including the requester's comments regarding the importance and application of the request. They should then be submitted in the following manner:

- A. Fission reactor requests should be transmitted to the Advisory Committee on Reactor Physics which will review and set the priority for each such entry. The present chairman is:

Dr. W. H. Hannum, Chief
Division of Reactor Development & Technology
Reactor Physics Branch
U. S. Atomic Energy Commission
Washington, D. C. 20545

- B. DOD requests should be transmitted to the Radiation Physics Division of the Defense Nuclear Agency. The present contact is:

Capt. Dean Kaul, Radiation Transport Project Officer
 HQ, Defense Nuclear Agency, Attn: RARP
 Department of Defense
 Washington, D. C. 20305

- C. Other requests should be transmitted to:

Dr. George A. Kolstad, Assistant Director for Physics & Mathematics Programs
 Division of Physical Research
 U. S. Atomic Energy Commission
 Washington, D. C. 20545

III. PRIORITY ASSIGNMENTS

The exact meaning of "priority" is difficult to assess but the following definitions,* which closely resemble those used by both EANDC and the EACRP, have been adopted by the USNDC:

PRIORITY I. Nuclear data which satisfy the criteria of Priority II and which have been selected for maximum practicable attention taking into account the urgency of nuclear energy program requirements.**

*The priority has been left blank on all requests for fusion reactor data. These fall under the organization listing of the Division of Controlled Thermonuclear Research (DCTR), AEC, Washington.

**For example, the EACRP assigns its highest priorities for reactor measurements as follows:
 The highest priority should be given to requests for nuclear data for ~~reactors~~ reactors to be built in the near future if:

these data are still necessary to predict the different reactor properties after all information from integral experiments and operating reactors has been used; or

information on an important reactor parameter is in principle attainable through mathematical calculations from nuclear data only; or

these data are needed for materials required in reactor physics measurements.

- PRIORITY II. Nuclear data that will be required during the next few years in the applied nuclear energy programs (for example, in data needed to make the best use of reactor fuel and construction materials such as neutron moderators, absorbers, and radiation shields, space and bio-medical applications; data required for better understanding of some significant aspect of reactor behavior).
- PRIORITY III. Nuclear data of more general interest and data required to fill out the body of information needed for nuclear technology.

IV. SCREENING REQUESTS

All fission reactor requests in this report were reviewed by the ACRP; all fusion reactor requests were reviewed by an Ad Hoc Committee for CTR; and the entire list of requests was reviewed by the following members and Subcommittee members of the USNDC in the Fall of 1972:

Standards

R. S. Caswell, NBS, Chrm.
W. W. Havens, Jr., Col.
W. P. Poenitz, ANL
L. Stewart, LASL
B. R. Leonard, Jr., BNW

Elastic and Inelastic Scattering

A. B. Smith, ANL, Chrm.
J. C. Hopkins, LASL
H. Goldstein, Col.
F. G. J. Perey, ORNL

Gamma-ray Production

H. E. Jackson, ANL, Chrm.
H. T. Motz, LASL
R. E. Chrien, BNL
J. K. Dickens, ORNL
V. J. Orphan, IRT

Total Capture Cross Sections

R. L. Macklin, ORNL, Chrm.
R. C. Block, RPI
M. P. Fricke, SAI
W. P. Poenitz, ANL
J. B. Czirr, LLL

Fission

M. S. Moore, LASL, Chrm.
C. D. Bowman, NBS
G. De Saussure, ORNL
R. W. Hockenbury, RPI
E. Melkonian, Col.
J. A. Grundl, NBS

Resonance Parameters, Resonance Integrals, and Total Cross Sections

R. C. Block, RPI, Chrm.
A. D. Carlson, NBS
J. A. Farrell, LASL
W. W. Havens, Jr., Col.
M. H. Kalos, NYU
O. D. Simpson, ANC

Fast Neutron Reactions

H. Alter, AI, Chrm.
D. W. Barr, LASL
D. E. Gardner, LLL
J. L. Brownlee, LLL
G. W. Butler, LASL

V. TABLES WITH DESCRIPTIVE INFORMATION

Preceding Tables 1, 2, and 3 will be the dictionary describing the quantities in the table which follows. The entire request list is contained in these three tables which are described as:

Table 1 contains the measurement requests for low-energy incident particles, that is, neutrons, protons, deuterons, tritons, and ^3He , ^4He , and ^6Li particles;

Table 2 contains the measurement requests for photons incident; and

Table 3 contains the medium-energy measurement requests for incident charged particles.

The requests which have been deleted from the last publication of the request list (NCSAC 35) have been compiled by hand for inclusion in Table 4. One line retrievals sorted on organization are to be found in Table 5. Each organization comprises a subset of Table 5 with names and organizational addresses given on each title page. A word of explanation is necessary since the one-line computer printout may appear to include erroneous requests. In making a search of this nature, only the first line of the particular request is retrieved even though the first requester (A-1 card and request) may not belong to that particular organization. Therefore, when a request appears in Table 5 without the correct organizational listing, one should take that request number and refer back to the main document in order to determine the energy range, priority, and accuracy associated with that specific request.

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TABLE 1. LOW ENERGY REQUESTS FOR INCIDENT NUCLEONS

<u>Reaction</u>	<u>Variables Allowed</u>	<u>Definition</u>
<u>A. NEUTRONS INCIDENT</u>		
Total		Sum of all partial cross sections
Elastic	$\sigma(\theta_n)$	Cross section for the scattering of the incident particle with the center-of-mass energy unchanged
Elas + 1st	$\sigma(\theta_n)$	Elastic plus first excited state cross section
Elas + In	$\sigma(\theta_n)$	Elastic plus "some" inelastic cross section
Tot n Scat	$\sigma(\theta_n)$	All emitted neutrons including elastic
Emission	$\sigma(\theta_{n,})$	All emitted neutrons except elastic, that is: Emission = $\sigma_{n,n'} + 2\sigma_{n,2n} + 3\sigma_{n,3n} + \bar{\nu}\sigma_{n,f} + \text{etc.}$
	$\sigma(E_{n,})$	
	$\sigma(\theta_{n,}, E_{n,})$	
	$\sigma(55^\circ, E_{n,})$	
	$\sigma(90^\circ, E_{n,})$	
Inelastic	$\sigma(\theta_{n,})$	Total inelastic scattering cross section
	$\sigma(E_{n,})$	
	$\sigma(\theta_{n,}, E_{n,})$	
$\sigma_{n,n'}$	Isom State	Inelastic scattering to an isomeric state
$\sigma_{n,n'}$	1st State	Inelastic scattering to the first excited state
$\sigma_{n,n'}$	2nd State	Inelastic scattering to the second excited state
$\sigma_{n,n'p}$		Reaction cross section for the emission of n and p

TABLE 1. (cont.)

<u>Reaction</u>	<u>Variables Allowed</u>	<u>Definition</u>
$\sigma_{n,n'd}$		Reaction cross section for the emission of n and d
$\sigma_{n,n't}$	$\sigma(\theta_n,)$	Reaction cross section for the emission of n and t
$\sigma_{n,n'3\alpha}$		Cross section for the $^{12}\text{C}(n,n'3\alpha)$ reaction
$\sigma_{n,2n}$		Total cross section for the (n,2n) reaction
$\sigma_{n,2n}$	Isom State	Partial (n,2n) cross section to an isomeric state
$\sigma_{n,2n}$	Act	Activation cross section for the (n,2n) reaction
$\sigma_{n,3n}$		Total (n,3n) cross section
$\sigma_{n,3n}$	Act	Activation cross section for the (n,3n) reaction
$\sigma_{n,4n}$		Total (n,4n) cross section
$\sigma_{n,g}$		$(\sigma_{n,\gamma})$ Total radiative capture cross section
$\sigma_{n,g}$	Act	Activation cross section for the (n, γ) reaction
$\sigma_{n,g}$ wrt	$\sigma_{n,f}^{\text{Pu}^{239}}$	Relative measurement with respect to Pu^{239} fission
$\sigma_{n,p}$		Total (n,p) cross section
$\sigma_{n,p}$	Act	Activation cross section for the (n,p) reaction
$(n,p)\text{Li}^9$	$\bar{b} \rightarrow \text{Be}^{9*} \rightarrow n$	The $\text{Be}^9(n,p)\text{Li}^9$ reaction which β decays to an excited state in Be^9 , which then emits a neutron
$(n,p)\text{N}^{17}$	$\bar{b} \rightarrow \text{O}^{17*} \rightarrow n$	The $\text{O}^{17}(n,p)\text{N}^{17}$ reaction which β decays to an excited state in O^{17} which then emits a neutron
$\sigma_{n,d}$		Total (n,d) cross section
$\sigma_{n,t}$		Total (n,t) cross section

TABLE 1. (cont.)

Reaction	Variables Allowed	Definition
Tot $\bar{a}$ Prod		Total α production cross section; for example, for B^{10} , this would be $\sigma_{n,\alpha_0} + \sigma_{n,\alpha_1} + 2\sigma_{n,t2\alpha} + 2\sigma_{n,2n} + 2\sigma_{n,n'd}$
$\sigma_{n,\bar{a}}$		Total (n, α) cross section
$\sigma_{n,\bar{a}}$	Act	Activation cross section for the (n, α) reaction
$\sigma_{n,\bar{a}}$ Ratio	wrt B^{10}	Measurement of the $Li^6(n,\alpha)$ relative to B^{10}
$\sigma_{n,\bar{a}}$	1st	The $B^{10}(n,\alpha_1\gamma)$ cross section (separate α_0 and α_1)
$\sigma_{n,\bar{a}g}$	$E_g^- = 480$ keV	The $B^{10}(n,\alpha_1\gamma)$ cross section (detect the 480-keV γ)
Tot $\bar{g}$ Prod	$\sigma(\theta_g^-)$ $\sigma(E_g^-)$ $\sigma(\theta_g^-, E_g^-)$ $\sigma(55^\circ, E_g^-)$ $\sigma(90^\circ, E_g^-)$	Total γ -ray production cross section, including all processes such as inelastic, radiative capture, (n,p), (n, α), (n,2n), (n,f), etc.
$\sigma_{n,n'}(\bar{g}'s)$	$\sigma(\theta_g^-)$	A specific γ (or γ 's) which is uniquely identified with inelastic scattering
$\sigma_{n,n'}(\bar{g}_1)$	$\sigma(\theta_g^-)$	A discrete γ -ray associated with the deexcitation of the first excited state of the target. In most cases of interest, the excitation and deexcitation cross sections are identical.

TABLE 1. (cont.)

<u>Reaction</u>	<u>Variables Allowed</u>	<u>Definition</u>
Absorption		Usually specified as $\sigma_{n,\gamma} + \sigma_{n,f}$ but here includes $\sigma_{n,p} + \sigma_{n,d}$
$\sigma_{abs} - \sigma_{n,f}$	no n exit	$\sigma_{n,p} + \sigma_{n,d} + \text{etc.}$
Destruct	of target	All cross sections in which the target is consumed
$\sigma_{n,f}$		Cross section for all processes accompanied by fission
$\sigma_{n,f}$ Ratio	wrt H, B ¹⁰	The fission cross section ratio to hydrogen scattering or B ¹⁰ as the reference standard
Fis Ratio	wrt U ²³⁵	Ratio measurements of fission cross section relative to U ²³⁵
Fis Ratio	wrt Pu ²³⁹	Ratio measurements of fission cross section relative to Pu ²³⁹
$\sigma_{n,f} + \sigma_{n,g}$	at 77° K	Absorption cross section averaged over a spectrum represented by a Maxwellian with temperature 77° K
Eta		Number of neutrons per nonelastic collision
Alpha		Ratio of the capture to fission cross section
Nu Bar		Average number of fission neutrons emitted per fission
Nu Bar	Prompt	Average number of prompt fission neutrons per fission
Nu Bar	Delayed	Average number of delayed fission neutrons per fission
Fis. Spect	$P(E_n,)$	Energy spectrum of the fission neutrons produced by fission
Cap Spect	$P(E_g^-)$	Energy spectrum of the γ 's produced in radiative capture
Prompt n Y	$P(E_n,)$	Energy spectrum of the prompt neutrons
Delayd n Y	$P(E_n,)$	Energy spectrum of the delayed neutrons

TABLE 1. (cont.)

<u>Reaction</u>	<u>Variables Allowed</u>	<u>Definition</u>
Fis n Y	$P(E_n)$	Energy spectrum of the fission neutrons (prompt plus delayed)
Tot f Y		Total fission yield
Prompt f Y		Prompt fission yield
Delayd f Y		Delayed fission yield
Fis $\bar{g}$ Y	$P(E_g)$	Fission gamma spectrum (total)
Prompt $\bar{g}$ Y	$P(E_g)$	Prompt gamma spectrum
Delayd $\bar{g}$ Y	$P(E_g)$	Delayed gamma spectrum
Delayd $\bar{g}$ Y	$P(E_g, T^{1/2})$	Time dependent delayed gamma spectrum
Fis Prod Y	of Xe^{135}	Average number of Xe^{135} produced per fission
Fis Prod Y	of Cs^{137}	Average number of Cs^{137} produced per fission
Fis Prod Y	of Nd^{147}	Average number of Nd^{147} produced per fission
Fis Prod Y	of Sm^{149}	Average number of Sm^{149} produced per fission
Polariz	$P(\theta_n)$	Vector polarization produced in neutron elastic scattering
Res Par		All resonance parameters
Res Int		Resonance Integral
Res Int	Capture	Resonance radiative capture integral
J, π		Spin and parity
$\bar{G}$		Total level width

TABLE 1. (cont.)

<u>Reaction</u>	<u>Variables Allowed</u>	<u>Definition</u>
$\bar{G}_n$		Neutron level width
$\bar{G}_f$		Fission level width
$\bar{G}_g$		Radiative capture level width
$\bar{G}_p$		Proton level width
$\bar{G}_a$		Alpha level width
$\bar{G}_n$ and $\bar{G}_g$		Neutron and radiative capture widths
$\bar{G}_f$ and $\bar{G}_n$		Fission and neutron widths
$\bar{G}_g$ and $\bar{G}_f$		Radiative capture and fission widths
 <u>B. PROTONS INCIDENT</u>		
$\sigma_{p,n}$		Cross section for the (p,n) reaction
$\sigma_{p,\bar{a}}$		Cross section for the (p, α) reaction
$\sigma_{p,n'p}$		Cross section for the (p,n'p) reaction
$(p,p')Li^6$	$d + \bar{a}$	$Li^6(p,p')Li^{6*}$ reaction which decays via $(d + \alpha)$
$(p,d)Be^8$	$2\bar{a}$ decay	$Be^9(p,d)Be^8$ reaction which decays via 2α

TABLE 1. (cont.)

<u>Reaction</u>	<u>Variables Allowed</u>	<u>Definition</u>
<u>C. DEUTERONS INCIDENT</u>		
$\sigma_{d,n}$		Cross section for the (d,n) reaction
$\sigma_{d,n}$	$\text{He}^3 + \bar{a}$	$\text{Li}^6(d,n)\text{Be}^7$ reaction which decays via $(\text{He}^3 + \alpha)$
$\sigma_{d,p}$		Cross section for the (d,p) reaction
$\sigma_{d,p}$	$t + \bar{a}$	$\text{Li}^6(d,p)\text{Li}^7$ reaction which decays via $(t + \alpha)$
$\sigma_{d,n'p}$		Cross section for the (d,n'p) reaction
$\sigma_{d,a}$		Cross section for the (d, α) reaction
$(d,d')\text{Li}^{6*}$	$d + \bar{a}$	$\text{Li}^6(d,d')\text{Li}^{6*}$ reaction which decays via $(d + \alpha)$
<u>D. TRITONS INCIDENT</u>		
t,d		Cross section for the (t,d) reaction
$t,2n$		Cross section for the (t,2n) reaction
$(t,p)\text{Li}^8$	$\bar{b}^- \rightarrow 2\bar{a}$	$\text{Li}^6(t,p)\text{Li}^8$ reaction which β^- decays to Be^8 and then 2α 's are emitted
$(t,n)\text{Be}^8$	$2\bar{a}$ decay	$\text{Li}^6(t,n)\text{Be}^8$ reaction where 2α 's are emitted promptly

TABLE 1. (cont.)

<u>Reaction</u>	<u>Variables Allowed</u>	<u>Definition</u>
<u>E. He's INCIDENT</u>		
${}^3\text{He}, p$		Cross section for the $({}^3\text{He}, p)$ reaction
$({}^3\text{He}, p)$	$2\bar{a}$ decay	$\text{Li}^6({}^3\text{He}^3, p)$ reaction which leads to the emission of 2α 's
$({}^3\text{He}, d)$		Cross section for the $({}^3\text{He}, d)$ reaction
$({}^3\text{He}, n)\text{B}^8$	$\bar{b}^+ \rightarrow 2\bar{a}$	$\text{Li}^6({}^3\text{He}^3, n)\text{B}^8$ reaction which β^+ decays to Be^8 and then 2α 's are emitted
<u>F. α's INCIDENT</u>		
$\sigma_{\bar{a}, n}^-$		Cross section for the (α, n) reaction
$\sigma_{\bar{a}, p}^-$		Cross section for the (α, p) reaction
$(\bar{a}, \bar{a}')\text{Li}^{6*}$	$d + \bar{a}$	$\text{Li}^6(\alpha, \alpha')\text{Li}^{6*}$ reaction which decays by $(d + \alpha)$
<u>G. Li^6 PARTICLES INCIDENT</u>		
${}^6\text{Li} + {}^6\text{Li} \rightarrow$	${}^7\text{Be} + {}^4\text{He} + n$	Cross section for the production of Be^7 , α , and n

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
5	$^1_1\text{H}^3$	$\sigma_{n,2n}$		III			12.5			10		LASL Motz	DMA	65	
					REQ COM: Absolute cross section required,									65	
					STATUS: No active work,									72	
6	$^1_1\text{H}^3$	$\sigma_{p,n}$					1.5-15				<25	ORNL McNally	DCTR	72	
					REQ COM: To estimate feasibility of fusion chain reactions,									72	
					STATUS: No active work,									72	
7	$^1_1\text{H}^3$	$\sigma_{t,2n}$				10-	10				<25	ORNL McNally	DCTR	72	
					REQ COM: To estimate feasibility of fusion chain reactions,									72	
					STATUS: No active work,									72	
8	$^2_2\text{He}^3$	$\sigma_{n,p}$		II		10-	3	1				GGA Nordheim	DRDT	69	
				II		10-	3	1				LMFB Hemmig-AEC	DRDT	69	
				II		1-	3	3				NDG Caswell	DPR	69	
				II		100-	3	3				LASL Diven	DMA	69	
				II			3-10		5			LASL Diven	DMA	69	
					REQ COM: For use as secondary standard,									69	
					Intermediate accuracy useful,									69	
					Absolute values required,									69	
					STATUS: GGA Costello ⁺ , 0.3-1.1 MeV; accuracy 10 percent.									72	

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURAOY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	<15	>15	LAB	PERSON	ORG	
9	${}^3_2\text{He}$	$\sigma_{t,d}$				100-	10				<25	ORNL McNally	DCTR	72	
						REQ COM: To estimate feasibility of fusion chain reactions,									72
						STATUS: No active work,									72
10	${}^4_2\text{He}$	σ_{d,n^1p}					3.3=15				<25	ORNL McNally	DCTR	72	
						REQ COM: To estimate feasibility of fusion chain reactions,									72
						STATUS: No active work,									72
11	${}^7_3\text{Li}$	Tot $\bar{g}$ Prod	$\sigma(E_g)$	II I		258 $\pm$ 10				15*	1	SNPO Fleishman	DSNS	69	
							4-10			15*		SNPO fleishman	DSNS	69	
						REQ COM: *Accuracy 15 percent or 5 mb whichever greater.									69
						Absolute $\sigma(E_g)$ required for all $E_g > 200$ keV.									69
						Neutron energy intervals required:									69
						Res. regions: reproduce major variations in $\sigma(E_g)$									69
						>1MeV: 500-keV intervals,									69
						Gamma-energy resolution required:									69
						<2,5MeV, 10 percent; >2,5MeV, 250 keV,									69
						STATUS: Frankfurt, Presser+Bass. $E_n = 1-9$ MeV,									72
						${}^7\text{Li}(n,n^1)$ 480-keV $\bar{g}$.									72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
12	${}^6_3\text{Li}$	Elastic	$\sigma(\theta_n)$	I		1-100		1-	5			NDC	Caswell	DPR	69
					REQ COM: Accuracy 1 to 5 per, to obtain n, alpha to 2 per, $\sigma(\theta)$ may be required at upper end,										69
					STATUS: Asami ⁺ EANDC(JAP)-13L, 1-10 keV, 4 percent,										70
13	${}^6_3\text{Li}$	Elastic	$\sigma(\theta_n)$			~14			15			AEC	Gough	DCTR	71
					REQ COM: Need for shield, magnet cost estimates, CTR,										71
					STATUS: No data to required accuracy,										72
14	${}^6_3\text{Li}$	Emission	$\sigma(\theta_n, E_n)$	I		8-14			≤10			LASL	Motz	DMA	65
					REQ COM: Absolute $\sigma(\theta_n, E_n)$ at several angles required, Include (n,2n) neutrons,										67
					STATUS: No active work,										72
15	${}^6_3\text{Li}$	$\sigma_{n,2n}$		I		8-16			5			LASL	Motz	DMA	66
					REQ COM: Absolute σ 's, coincidence technique required, Needed to determine true energy dependence, omit 14-MeV point,										66
					STATUS: No active work,										72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
29	${}^6_3\text{Li}$	$(t,p)\text{Li}^8$	$5^- \rightarrow 2\bar{a}$			10-	2					<25	ORNL McNally	DCTR	72
					REQ COM: To estimate feasibility of fusion chain reactions,										72
					STATUS: No active work,										72
30	${}^6_3\text{Li}$	$\sigma_{t,d}$				10-	2					<25	ORNL McNally	DCTR	72
					REQ COM: To estimate feasibility of fusion chain reactions,										72
					STATUS: No active work,										72
31	${}^6_3\text{Li}$	$({}^3\text{He},n)\text{B}^8$	$5^+ \rightarrow 2\bar{a}$				2-8					<25	ORNL McNally	DCTR	72
					REQ COM: To estimate feasibility of fusion chain reactions,										72
					STATUS: No active work,										72
32	${}^6_3\text{Li}$	$({}^3\text{He},p)$	$2\bar{a}$ decay			100-	8					<25	ORNL McNally	DCTR	72
					REQ COM: To estimate feasibility of fusion chain reactions,										72
					STATUS: No active work,										72
33	${}^6_3\text{Li}$	$({}^3\text{He},d)$				100-	8					<25	ORNL McNally	DCTR	72
					REQ COM: To estimate feasibility of fusion chain reactions,										72
					STATUS: No active work,										72

[illegible]

REQ #	TARGET # Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR	
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG		
42	${}_3\text{Li}^7$	$\sigma_{n,n't}$	$\sigma(\theta_{n'})$				~14			15			AEC	Gough	DCTR	71
					REQ COM: Need for shield, magnet cost estimates, CTR.											71
					STATUS: No active work.											72
43	${}_3\text{Li}^7$	$\sigma_{\alpha,n}$		II			4-6	2					NDC	Caswell	DPR	69
					REQ COM: Accuracy 2 percent for inverse reaction,											72
					Energy to correspond to 10 keV to 1 MeV,											69
					for inverse reaction: $B(n, \bar{1}_0)$.											69
					STATUS: No active work.											72
44	${}_4\text{Be}$	Elastic	$\sigma(\theta_n)$	I			7-20			10			LLL	Howerton	DMA	62
					REQ COM: Resolutions: $\Delta E = \pm 250$ keV; $\Delta\theta = 3.0^\circ$											62
					STATUS: NEL Bucher+ NCSAC-33, meas. planned, small angles.											70

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
45	${}^9_4\text{Be}$	Emission	$\sigma(E_n, E_n')$	II			1.8-5			15			LMFB Hemmig	AEC DRDT	62
					REQ COM: For Be moderated fast spectrum reactors and for thermal breeders or convertors and neutron economy calculations, DRDT Need secondary neutron energy and angular distrib, Energy resol, 5 per incident; 500 keV on E_n , DRDT Accuracy 50 mb at 2-3 MeV, DRDT STATUS: No active work,										62 62 62 62 69 69
46	${}^9_4\text{Be}$	$\sigma_{n,\gamma}$		II	1-	100				10			IRT Preskitt	DRDT	69
					REQ COM: To resolve discrepancies in thermionic reactor worths, STATUS: ORNL Macklin+ NCSAC-33, no capture levels <600keV,										69 69 70
47	${}^9_4\text{Be}$	(n,p)Li ⁹	$\bar{\sigma} = \text{Be}^{9*} \rightarrow n$	II			14			10			LASL Walton	DNMS	70
					REQ COM: Background in delayed neutron assays, STATUS: Measurements planned at LASL,										70 72
48	* ${}^{10}_4\text{Be}^7$	$\sigma_{n,p}$		II	Th-	to	15					50	LLL Howerton	DMA	69
					***** REQ COM: Needed for evaluation, * Radioactive target-53 day STATUS: No active work,										69 69 72

REQ #	TARGET * Z A	REACTION TYPE QUANTITY	VARIABLE	PRI OR.	INCIDENT ENERGY ev	PERCENT ACCURACY 1-3 4-9 <15 >15	REQUESTER LAB PERSON	OKG	YR	
49	${}^9_4\text{Be}$	$\sigma_{p,\alpha}$			10-	15	<25	ORNL McNally	DCIR	72
REQ COM: To estimate feasibility of fusion chain reactions.										
STATUS: No active work.										
50	${}^9_4\text{Be}$	(p,d)Be ⁸	2 α decay		10-	15	<25	ORNL McNally	DCIR	72
REQ COM: To estimate feasibility of fusion chain reactions.										
STATUS: No active work.										
51	${}^{10}_5\text{B}$	Total		II	10-	1	1	NDC Caswell	DPR	69
REQ COM: Desired for assessing B(n, α) standard.										
STATUS: No new measurements.										
52	${}^{10}_5\text{B}$	Elastic	$\sigma(e_n)$	II	1-100	1	1-5	NDC Caswell	DPR	69
REQ COM: Desired for assessing B(n, α) standard.										
STATUS: No new measurements.										
72										72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR	
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG		
53	$5B^{10}$	$\sigma_{n,\bar{a}}$		I		1-	10	1-	5				ANL	Avery	DRDT	69
				I		1-	10	1-	5				LMFB	Hennig-AEC	DRDT	69
				I		1-	1		5				LLL	Howerton	DMA	70
				I		1-	10	1-	5				ORNL	Maienschein	DRDT	69
				I		1-	1	2					NDG	Caswell	DPR	69
REQ COM: 1-100 keV, accuracy 1 percent; 3 percent useful,																69
100-300 keV, accuracy 3 percent; 10 percent useful																69
0,3-10 MeV, accuracy 5 percent; 10 percent useful,																69
Needed as standard; absolute σ 's required, DRDT																69
$\bar{a}_0/\bar{a}_1$ ratio needed for both $\bar{a}$ and $\bar{g}$ detection,																69
STATUS: GRT Fricke, New measurements,																72
54	$5B^{10}$	$\sigma_{n,\bar{a}\bar{g}}(\bar{g}_1)$	$E_{\bar{g}} \approx 480 \text{ keV}$	I		1-	10	1-	5				ANL	Avery	DRDT	69
				I		1-	10	1-	5				LMFB	Hennig-AEC	DRDT	69
				I		1-	10	1-	5				ORNL	Maienschein	DRDT	69
				I		50-	1		2				NDG	Caswell	DPR	72
REQ COM: 1-100 keV, accuracy 1 percent; 3 percent useful,																69
100-300 keV, accuracy 3 percent; 10 percent useful																69
0,3-10 MeV, accuracy 5 percent; 10 percent useful,																69
Needed as standard; absolute σ 's required,																69
STATUS: GRT Friesenhahn ⁺ , Gulf-RT=A12210, 1 to 1000 keV,																72
accuracy 1,5 to 4,5 percent,																72
HAR Coates ⁺ preliminary data from ~1-240 keV,																72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
57	$_{6}^{12}\text{C}$	Elastic	$\sigma(\theta_n)$	III			2-14			10		KAPL Ehrlich	DNR	62	
					REQ COM: 20 percent accuracy acceptable.									62	
					Energy resolution 50 keV from 7 to 8.2MeV, 100 keV									62	
					from 8.2-10MeV, and larger from 10-14 MeV,									62	
					Angular resolution 3 deg from 7 to 8.4 MeV;									62	
					10 deg, from 8.4-14 MeV,									62	
					For shielding and for resonance or optical									62	
					model fitting,									62	
					STATUS: ORNL Perey ⁺ up to 8.5 MeV, ORNL-4441.									72	
					U. Ky, Galati ⁺ up to 7 MeV,									72	
					YALE Firk, NIM 43, 312 1.6 MeV to 10 MeV,									66	
					Knitter, EANDC Standards Conf, data 0.5-2.5 MeV,									70	
					ANL Smith ⁺ preliminary data to 3.8 MeV,									72	
58	$_{6}^{12}\text{C}$	Emission	$\sigma(\theta_{n'}, E_{n'})$	II			8-15			10		AFWL Enz	DNA	69	
				II			7-15		5			LASL Biggers	DNA	66	
				II			6-15			10		NEL Eccleshall	DNA	66	
					REQ COM: Every 250 keV; $\sigma(\theta)$ if significantly anisotropic,									66	
					$\Delta\sigma = \pm 5^\circ$ ($<30^\circ$) and $\pm 10^\circ$ ($>30^\circ$); $\Delta E = 250$ keV,									66	
					All neutrons, including low energy needed,									66	
					Must include absolute $\sigma(\theta_{n'}, E_{n'})$ from $(n, n', 3\bar{a})$.									66	
					STATUS: ORNL Perey ⁺ up to 8.5 MeV, ORNL-4441.									72	

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≥15	>15	LAB	PERSON	ORG	
63	${}^6\text{C}^{12}$	Polaris.	$P(\theta_n)$	II			4-5.5				15	KAPL	Ehrlich	DNR	69
					REQ COM: Energy Resolution ~ 50 keV, Needed to resolve discrepancy between theory and experiment,										69
					STATUS: No active work,										72
64	${}^7\text{N}$	Elastic	$\sigma(\theta_n)$	I			7-15		5			AC	Greenhow	DNA	69
							7-15		5			AFWL	Eng	DNA	69
							8-15		5			LASL	Biggers	DNA	69
					REQ COM: Every 500 keV or as dictated by structure, $\Delta\theta = \pm 2.5^\circ (30^\circ)$ and $\pm 5^\circ (>30^\circ)$; include $\theta < 20^\circ$, $\Delta E_n = 100 \text{ keV}$ or 10 percent, More data needed to resolve discrepancies										69
					STATUS: No active work,										72
65	${}^7\text{N}$	Elastic	$\sigma(\theta_n)$	I			7-15		5			NEL	Eccleshall	DNA	69
					REQ COM: Every 500 keV with 5 percent energy resolution $\Delta\theta = \pm 1^\circ$ every 5° for $\theta \leq 20^\circ$; needed to check importance of small angle data, $\Delta\theta = \pm 1.5^\circ$ every 10° for $\theta > 20^\circ$ Data needed to resolve discrepancies,										69
					STATUS: No active work,										72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≥15	>15	LAB	PERSON	ORG	
66	7 ^N	Emission	$\sigma(E_n, E_n')$	I			7-15			10		AG	Greenhow	DNA	69
				I			7-15			10		AFWL	Eng	DNA	69
				I			3-15			10		LASL	Biggers	DMA	69
				I			7-15			10		NEL	Eccleshall	DNA	69
REQ COM: 250-keV intervals or as dictated by structure,															69
Res: $\Delta E = 100$ keV or 10 percent, LASL															69
Res: $\Delta\theta = \pm 2.5^\circ$ ($0-30^\circ$), $\pm 5^\circ$ ($30-180^\circ$) or as dictated by the anisotropy,															69
Low-energy (<1 MeV) neutrons must be included,															69
STATUS: No active work,															72
67	7 ^N	Absorption		I			1-15			5		AG	Greenhow	DNA	66
				I			1-15			5		AFWL	Eng	DNA	66
				I			2-16			5		LASL	Biggers	DMA	66
REQ COM: Large discrepancies must be resolved <7.5 MeV,															69
No data available above ~ 7.5 MeV,															69
Data on $(n, \bar{\alpha}_0)$, (n, p_0) and (n, d_0) may suffice,															69
STATUS: No active work,															72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
68	${}^7\text{N}$	Tot $\bar{e}$ Prod	$\sigma(\theta_{\bar{e}}, E_{\bar{e}})$	I			8=15			10		AC	Greenhow	DNA	69
				I			8=15			10		AFWL	Eng	DNA	69
				I			8=20			10		LASL	Biggers	DMA	69
				I			9=20			10		LLL	Howerton	DMA	69
				I			8=15			10		NEL	Eccleshall	DNA	70
					REQ COM: Must include contributions of continuum gammas Resolution: $\Delta E_n \leq 250 \text{ keV}$, $\Delta E_{\bar{e}} \leq 250 \text{ keV}$, $\Delta \theta = 5^\circ (5-30^\circ)$ and $10^\circ (>30^\circ)$ or as dictated by anisotropy,										69
					STATUS: ORNL, Dickens ⁺ , $\theta_{\bar{e}} = 125 \text{ deg}$, $E_n = 2-20 \text{ MeV}$ in progress,										72
					Lund, Nyberg ⁺ , $E_n = 15 \text{ MeV}$, PS 4, 165 (1971).										72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
71	δ^0	Absorption		I			10-15		5			AFWL Enz	DNA	66	
				I			8-15		5			LASL Biggers	DMA	66	
					REQ COM: $\Delta E_n = 250$ keV at 250-keV intervals, Filling the energy gap and supporting evidence for $(n, \bar{\alpha}_0)$ likely to suffice; if so, integral of inverse will satisfy,									69	
					STATUS: No active work,									72	
72	δ^0	Tot $\bar{\alpha}$ Prod	$\sigma(\theta_{\bar{\alpha}}, E_{\bar{\alpha}})$	I			10-15		10			LASL Biggers	DMA	62	
												AFWE Enz	DNA	70	
					REQ COM: Absolute cross sections required,									62	
					STATUS: Lund, Nyberg ⁺ , $E_n = 15$ MeV, PS 4, 165, ORNL, Dickens ⁺ , $\theta_{\bar{\alpha}} = 125$ degrees, $E_n = 6-20$ MeV, in progress, also NSE 40, 283, $E_n = 6.7-11$ MeV, GRT, Orphan ⁺ , NSE 42, 352, $E_n = 6.4-16.5$ MeV,									72	
														72	
73	δ^{017}	$\sigma_{\alpha, n}$		II	***** Ths-7						20	KAPL Ehrlich	DNR	72	
					REQ COM: Alpha energy resolution 0.1 MeV, For calculation of neutron source strengths									66	
					STATUS: Sample not readily available,									66	
														72	

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
78	9^F	$\sigma_{n,\bar{g}}$		II		1-	1			10		ORNL Perry	ORNL	66	
					REQ COM: To calculate neutron loss in Molten Salt Breeder,									66	
					STATUS: ORNL Macklin has experiment in progress,									70	
					FGA Nystroem ⁺ , PS 4 95. (1971). 20-80 keV,									72	
79	9^F	Absorption			Th-	to	1k			10		AEC Gough	DOE	71	
					REQ COM: Needed for CTR applications using LiF.									71	
					STATUS: No active work,									72	
80	9^F	$\sigma_{n,\bar{a}}$		I			9-1k			10		LLL Howerton	ORNL	69	
					REQ COM: Absolute values at a few energies.									69	
					STATUS: Crumpton, NIM 92, 533 (1971),									72	
81	11^{Na}	Total		I		10-	5		3-	5		ORNL Clifford	ORNL	69	
					REQ COM: Fast reactor deep penetrations; 1 percent in valley									69	
					STATUS: No active work,									72	

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≥15	>15	LAB	PERSON	ORG	
85	$_{11}\text{Na}$	Absorption		II		1-100					20	GE	Snyder	DRDT	69
												LMFB	Hennig-AEC	DRDT	69
												WARD	Pitterle	DRDT	72
					REQ COM: Accuracy 20per or 0.5mb whichever is greater.										69
					Intermediate accuracy useful,										69
					STATUS: Measurements at Columbia and ORNL underway,										72
86	$_{11}\text{Na}$	$\bar{\sigma}_n$ and $\bar{\sigma}_g$		I		3					10	ANL	Avery	DRDT	62
												LMFB	Hennig-AEC	DRDT	69
					REQ COM: $\bar{\sigma}_n$ and $\bar{\sigma}_g$ desired for 3 keV resonance,										62
					STATUS: Yamamuro, NSE 41, 445 to 10 per, though										70
					discrepancies still exist,										70
87	$_{11}\text{Na}$	Cap Spect	$P(E_g)$	I		3					10	ANL	Avery	DRDT	72
					REQ COM: Capture Spectrum at 3 KeV required,										72
					Sufficient accuracy in E_g (3 KeV) to compare with										72
					E_g (thermal),										72
					STATUS: No measurements to required accuracy,										72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
91	^{13}Al	Inelastic	$\sigma(E_n)$			Ths-	1k			15		AEC	Gough	DCTR	72
						REQ COM: Needed to calculate neutron transport in blanket and shield, CTR,									71
						STATUS: ORNL Kinney ⁺ data to 8.5 MeV, ORNL-4516, U, Ky, Brandenberger, data at 8 and 9 MeV,									72
92	^{13}Al	Emission	$\sigma(\bullet_n, E_n)$	I			8-15			10		AFWL	Enz	DNA	69
				II			8-15			10		NEL	Eccleshall	DNA	69
						REQ COM: ΔE_n = 250 keV at 250 keV intervals, or as dictated by structure,									69
						$\Delta\theta = \pm 2.5^\circ$ (0-30°), $\pm 5^\circ$ (30-180°) or as dictated by anisotropy,									69
						STATUS: ORNL Kinney ⁺ data to 8.5 MeV, ORNL-4516, U, Ky, Brandenberger, data at 8 and 9 MeV,									72
93	^{13}Al	$\sigma_{n,\bar{g}}$					1k			20		AEC	Gough	DCTR	71
						REQ COM: Needed to calculate formation of higher mass isotopes, CTR,									71
						STATUS: No active work,									72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
97	¹³ Al	Cap Snect	P(E _R)	I	Th						10		SNPO Fleishman	DSNS	69
					Th-	res.					15		AEC Gough	DCTR	72
					REQ COM: For shielding calculations.										69
					Both line and continuum spectra are required,										69
					Needed to calculate heat generation,										72
					in blanket and shield, CTR,										72
					STATUS: Stecher-Rasmussen ⁺ , thermal NP A181, 225.										72
					Orphan ⁺ , GGA report GA-10248,										72
98	¹³ Al	Tot $\bar{\nu}$ Prod	$\sigma(E_R)$	II		5-200					15*		SNPO Fleishman	DSNS	69
				I			1-10				15*		SNPO fleishman	DSNS	69
					REQ COM: (*) Accuracy 15 per or 5 mb whichever is greater.										69
					Absolute $\sigma(E_R)$ required for all $E_R > 200$ keV,										69
					Neutron energy intervals required:										69
					Res. region: reproduce major variations in $\sigma(E_R)$										69
					> 1 MeV: 500-keV intervals										69
					Gamma-energy resolution required:										69
					< 2.5 MeV, 10 percent; > 2.5 MeV, 250 keV,										69
					STATUS: GRT Orphan ⁺ , Gulf-RT-10743, Line + Continuum										72
					gamma rays, $E_n = 0.86-16.7$ MeV,										72
					ORNL, Linac+NaI $E_n = 1-20$ MeV in progress,										72
					Dickens, PR C5, 100 (1972), $E_n = 3.53-9.0$ MeV,										72
					USSR Kravcov ⁺ , 72 Kiev, Gamma-Spectrum with Ge(Li)										72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
102	$_{14}\text{Si}^{30}$	$\sigma_{n,\bar{e}}$	Act	III	.025	to	15				30	LLL	Howerton	DMA	69
					REQ COM: Required is cross section for activation of Si^{31} , in naturally occurring element, Accuracy 30 per if $\sigma > 100$ mb, 50 per if $25 \text{ mb} < \sigma < 100 \text{ mb}$, Accuracy to a factor of 2 if $1 \text{ mb} < \sigma < 25 \text{ mb}$; to a factor of 10 if $\sigma < 1 \text{ mb}$, STATUS: FGA Nystroem ⁺ , PS 4, 95 (1971). 20-80 keV,										69 69 69 69 69 72
103	$_{16}\text{S}^{34}$	$\sigma_{n,\bar{e}}$	Act	I	.025	to	15				30	LLL	Howerton	DMA	69
					REQ COM: Required is cross section for activation of S^{35} in naturally occurring element. Accuracy 30 per if $\sigma > 100$ mb, 50 per if $25 \text{ mb} < \sigma < 100 \text{ mb}$, Accuracy to a factor of 2 if $1 \text{ mb} < \sigma < 25 \text{ mb}$; to a factor of 10 if $\sigma < 1 \text{ mb}$, STATUS: Kappe, Diss, Abstr, 27B 919 gives thermal value, FGA Nystroem ⁺ , PS 4, 95 (1971). 20-80 keV,										69 69 69 69 69 70 72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	<1-3	4-9	>15	>15	LAB	PERSON	ORG	
104	$^{19}\text{K}^{41}$	$\sigma_{n,\bar{g}}$	Act	II	.025	to	15				30	LLL	Howerton	DMA	69
					REQ COM: Required is cross section for activation of K^{42} in naturally occurring element. Accuracy 30 per if $\sigma > 100$ mb, 50 per if 25 mb $< \sigma < 100$ mb, Accuracy to a factor of 2 if 1 mb $< \sigma < 25$ mb; to a factor of 10 if $\sigma < 1$ mb,										69
					STATUS: Kappe, Diss, Abstr, 27B 919 gives thermal value, Stupegia ⁺ JNE 22, 267, 0, 16-25 MeV, to 10 percent INC Schuman WASH-1127 gives 2keV value, 310 ± 100 mb,										70
															72
105	^{20}Ca	Elastic	$\sigma(\theta_n)$	II			8-15			10		NEL	Eccleshall	DNA	69
					REQ COM: Resolutions: Energy 0,25 MeV; angular 3 degrees Intervals: Energy 0,5 MeV; angular 10 degrees,										69
					STATUS: No active work,										72
106	^{20}Ca	Emission	$\sigma(\theta_n, E_n)$	II			8-15			10		NEL	Eccleshall	DNA	69
					REQ COM: Resolutions: Energy 0,25 MeV; angular 3 degrees, Increments: Energy 0,5 MeV; angular 10 degrees,										69
					STATUS: No active work,										72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≥15	>15	LAB	PERSON	ORG	
107	^{20}Ca	Tot $\bar{\kappa}$ Prod	$\sigma(\theta_{\bar{\kappa}}, E_{\bar{\kappa}})$	II			5-15			10		NEL	Eccleshall	DNA	69
					REQ COM: Need energy spectrum of all gammas, Resolution: 5 per in $E_{\bar{\kappa}}$, 5 degrees in θ , Increments of 0.5 MeV, 10 degrees,										69
					STATUS: ORNL Dickens, $E_n = 4.8-8$ MeV, $\theta_{\bar{\kappa}} = 125$ degrees,										72
108	$^{20}\text{Ca}^{44}$	$\sigma_{n,\bar{g}}$	Act	I	.025	to	15				30	LLL	Howerton	DMA	69
					REQ COM: Required is cross section for activation of Ca^{45} in naturally occurring element, Accuracy 30 per if $\sigma > 100$ mb, 50 per if 25 mb $< \sigma < 100$ mb, Accuracy to a factor of 2 if 1 mb $< \sigma < 25$ mb, to a factor of 10 if $\sigma < 1$ mb,										69
					STATUS: No active work,										72
109	^{21}Sc	$\sigma_{n,\bar{g}}$	Act	II		1-	18			10		HEDL	McElroy	DRDT	69
					REQ COM: For use as fluence monitor,										69
					STATUS: No active work,										72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≥15	>15	LAB	PERSON	ORG	
113	$^{46}_{22}\text{Ti}$	$\sigma_{n,p}$	Act	II III			1-18 1-12,5			10 10			HEDL McElroy NEL Eccleshall	DRDT DNA	69 69
					REQ COM: Resolution in energy 100 keV, 500-keV intervals For use as a fluence monitor.										69 69
					STATUS: Ghorai, JNE 25, 319 (1971). ANL Meadows has measurements 4-6 MeV.										72 72
114	$^{47}_{22}\text{Ti}$	$\sigma_{n,p}$	Act	II III			>1 1-15			10 *			HEDL McElroy NEL Eccleshall	DRDT DNA	69 69
					REQ COM: Resolution in energy 100 keV, 1-MeV intervals * For $\sigma > 5$ mb, $\Delta\sigma = 2,5$ mb. For use as fluence monitor.										69 69 69
					STATUS: ANL Meadows, NCSAC-42, 10 (1972). Ghorai, JNE 25, 319 (1971).										72 72
115	$^{48}_{22}\text{Ti}$	$\sigma_{n,p}$	Act	II II III			>1 3,2-10 3-12,5			10 10		20	HEDL McElroy KAPL Ehrlich NEL Eccleshall	DRDT DNR DNA	69 69 69
					REQ COM: Resolution in energy 100 keV, 500-keV intervals. For use as fluence monitor, activation analysis.										69 69
					STATUS: Ghorai, JNE 25, 319 (1971). ANL Meadows ⁺ has measurements 4,5-6 MeV.										72 72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≥15	>15	LAB	PERSON	ORG	
119	^{23}V	Inelastic	$\sigma(E_n)$	III			1.5-10				15	ANL	Avery	DRDT	62
												GE	Snyder	DRDT	62
												LMFB	Hemmig-AEC	DRDT	62
					REQ COM: Total integral over $h\nu$ required, Spectra at several angles if significantly anisotropic										62
					STATUS: AE Almen ⁺ , 2 to 4.5 MeV, Helsinki Conf. II, p. 349										72
120	^{23}V	Inelastic	$\sigma(E_n)$			Ths-	14			15		AEC	Gough	DCTR	72
					REQ COM: Needed to calculate neutron transport in blanket and shield, GTR,										71
					STATUS: AE Almen ⁺ , 2 to 4.5 MeV, Helsinki Conf. II, p. 349										72
121	^{23}V	$\sigma_{n,\bar{g}}$					14				20	AEC	Gough	DCTR	71
					REQ COM: Needed to calculate formation of higher mass isotopes, GTR,										71
					STATUS: No active work,										72
122	^{23}V	$\sigma_{n,\bar{g}}$	Act	II	Th					5		AFIT	Dooley	DNA	62
					REQ COM: Activation cross section desired at 0.025 eV										62
					STATUS: No active work,										72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
127	²³ V	Cap Spect	P(E _g)		Th-	res.				15		AEC	Gough	DCTR	71
					REQ COM: Needed to calculate heat generation in blanket and shield, CTR,										71
					STATUS: ORNL Bird ⁺ , ORNL-TM-3379 E _n =20-60 MeV,										72
128	²⁴ Cr	Total		II		1-	20	3				LMFB	Hennig-AEC	DNDT	72
					REQ COM: One percent accuracy in deep minima, Energy resolution sufficient to resolve major structure,										72
					STATUS: No active work,										72
129	²⁴ Cr	Elastic	σ(θ _n)	II			2-14		4-9			KAFL	Ehrlich	DNR	69
					REQ COM: Res: 100keV, Δθ = 5°										69
					STATUS: ANL measurements in progress,										72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
133	^{24}Cr	$\sigma_{n,2n}$	$\sigma(\theta_n, E_n)$				14			15		AEC	Gough	DCTR	71
					REQ COM: Energy and angular dependence of secondary neutrons needed to calculate neutron transport in blanket and shield, CTR,										71
					STATUS: No active work,										72
134	^{24}Cr	$\sigma_{n,\bar{g}}$		II		1-	1			15		GE	Snyder	DRDT	72
												LMFB	Hennig-AEC	DRDT	65
												ORNL	Clifford	DRDT	65
					REQ COM: Incident resolution 20 percent, Resonance parameters needed, espec, gamma widths,										69
					STATUS: RPI Stieglitz ⁺ , NP A163, 592 (1971), To 200 keV, LLL Baglan ⁺ NCSAC-33, from threshold photoneut,										72
135	^{24}Cr	$\sigma_{n,\bar{g}}$					14			20		AEC	Gough	DCTR	71
					REQ COM: Needed to calculate formation of higher mass isotopes, CTR,										71
					STATUS: No active work,										72
136	^{24}Cr	$\sigma_{n,p}$					14			20		AEC	Gough	DCTR	71
					REQ COM: Needed for radiation damage estimates, CTR,										71
					STATUS: No active work,										72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
141	24Cr	Tot $\bar{g}$ Prod	$\sigma(E_{\bar{g}})$	I	500-	20				15*		SNPO	Fleishman	DSNS	69
				I				1-10		15*		SNPO	Fleishman	DSNS	69
				II				1-14		15*		NEL	Eccleshall	DNA	70
				REQ COM: (*) Accuracy 15 per or 5 mb whichever is greater, Absolute $\sigma(E_{\bar{g}})$ required for all $E_{\bar{g}} > 200$ keV, Neutron Energy intervals required: Res. regions: reproduce major variations in $(E_{\bar{g}})$ > 1 Mev: 500-keV intervals Gamma-energy resolution required: <2.5MeV, 10 percent; >2.5MeV, 250keV.											
142	24Cr	Tot $\bar{g}$ Prod	$\sigma(E_{\bar{g}})$	II	up	to	10			10		BET	Bayard	DNR	69
												LMFB	Hemmig-AEC	DNDT	72
REQ COM: The above accuracy (10 percent) is requested, in 0,5 MeV gamma-ray resolution intervals, for shielding calculations,															
STATUS: Degtjarev ⁺ , IZV 35 2341, $E_n = 1.0-3.4$ MeV.															

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
143	$^{53}_{24}\text{Cr}$	$\bar{\sigma}_n$		II		1-600			4-9				KAPL Ehrlich	DNR	69
					REQ COM: None,										69
					STATUS: KFK Moeller and Rohr, NP A164, 97 (1971), report										72
					J. $\bar{\sigma}_n$ for 30 res. in ^{53}Cr from 17 to 250 keV.										72
					KFK Plan measurements on separated isotopes,										72
144	$^{55}_{25}\text{Mn}$	$\sigma_{n,\bar{g}}$		II	Th=	1				10			LLL Howerton	DMA	66
					REQ COM: Energy dependence of $\sigma_{n,\bar{g}}$ should be well defined,										69
					STATUS: No active work,										72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
145	25Mn	Tot $\bar{\nu}$ Prod	$\sigma(E_{\bar{\nu}})$	I	300-	120				15*	SNPO	Fleishman	DSNS	69	
				I					15*	SNPO	Fleishman	DSNS	69		
				II					15*	NEL	Eccleshall	DNA	70		
				REQ COM: (*) Accuracy 15 per or 5 mb whichever is greater, Absolute $\sigma(E_{\bar{\nu}})$ required for all $E_{\bar{\nu}} > 200$ keV, Neutron Energy intervals required: Res. regions reproduce major variations in $(E_{\bar{\nu}})$ > 1 Mev: 500-keV intervals Gamma-energy resolution required: <2.5MeV, 10 percent; >2.5MeV, 250keV.										69 69 69 69 69 69	
					STATUS: BNL Chrien reports spectra for 4 res, WASH-1136, BNL Chrien, 2 keV capture spectrum from MTR, IN-1317, p. 116 (1970).										69 72 72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
147	26 ^{Fe}	Elastic	$\sigma(\theta_n)$	I			7-14		4-9			KAPL Ehrlich	DNR	69	
				I		500-	3		5		ORNL Clifford	DRDT	69		
				I		1-	10			10	ANL Avery	DRDT	69		
				I		1-	10			10	LMFB Hemmig-AEC	DRDT	69		
					REQ COM: Resolutions: 100keV, $\Delta\theta = 5^\circ$, KAPL.										69
					Resolutions: 1 percent energy at several peaks.										69
					and valleys: $\sigma(\theta_n)$ required in valleys										69
					for shielding, ORNL,										69
					Resolution to at least resolve intermediate										69
					structure, ANL,										69
					STATUS: ANL Smith ⁺ data available satisfying intermediate										72
					requirements to 3.8 MeV,										72
					ORNL Perey ⁺ data 4.19-8.56 MeV, ORNL-4515.										72
					AE Holmquist ⁺ , AE-337; Helsinki Conf., to 8 MeV.										72
148	26 ^{Fe}	Elastic	$\sigma(\theta_n)$	I			8-16		5			LASL Biggers	DMA	66	
					REQ COM: $\Delta E_n = 250\text{keV}$, intervals dictated by structure,										66
					$\Delta\theta = \pm 2.5^\circ (\leq 30^\circ)$, $\pm 5^\circ (> 30^\circ)$.										62
					STATUS: No active work,										72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR					
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG						
149	^{26}Fe	Inelastic	$\sigma(E_n)$	I		850-	2		5				GE	Snyder	DRDT	66				
				I		850-	2		5				LMFB	Hemmig-AEC	DRDT	66				
				II			2-10		10				GE	Snyder	DRDT	66				
				II			2-10		10				LMFB	Hemmig-AEC	DRDT	66				
REQ COM: Resolution 20 keV for incident and scattering neutrons. Total integral over k_x required. Spectra at several angles if significantly anisotropic,																72				
STATUS: ANL Smith ⁺ , preliminary results to 3.8 MeV. Case Lindow ⁺ NSCAC-31, have data 5.0-5.5 MeV. AE Almen ⁺ , Helsinki Conf. to 4.5 MeV. ORNL Perey ⁺ , 0.85-2, 4-8.5 MeV, Knoxville Conf. ORNL Dickens ⁺ , ORNL-4515. CEA Naouat ⁺ , Knoxville Conf. 2-14 MeV.																72				
150	^{26}Fe	Inelastic	$\sigma(E_n)$			Ths-	14			15			AEC	Gough	DCTR	72				
				REQ COM: Needed to calculate neutron transport in blanket and shield, CTR,																71
				STATUS: ANL Smith ⁺ , preliminary results to 3.8 MeV. CASE Lindow ⁺ NSCAC-31, have data 5.0-5.5 MeV. Almen ⁺ , Helsinki Conf. to 4.5 MeV. ORNL Perey ⁺ , 0.85-2, 4-8.5 MeV, Knoxville Conf. ORNL Dickens ⁺ , ORNL-4515. CEA Naouat ⁺ , Knoxville Conf. 2-14 MeV.																72
																				71

[illegible]

REQ #	TARGET * Z A	REACTION TYPE QUANTITY VARIABLE	PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
				eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
157	^{26}Fe	$\sigma_{n,p}$				14				20	AEC	Gough	DCTR	71
				REQ COM: Needed for radiation damage estimates, CTR,										71
				STATUS: No active work,										72
158	$^{26}\text{Fe}^{56}$	$\sigma_{n,\alpha}$	II	Th	to	10			15		GE	Hutchins	DRDT	72
				REQ COM: To determine He production in fast reactors,										72
				STATUS: No active work,										72
159	^{26}Fe	$\sigma_{n,\alpha}$				14				20	AEC	Gough	DCTR	71
				REQ COM: Needed for radiation damage estimates, CTR,										71
				STATUS: No active work,										72
160	^{26}Fe	$\sigma_{n,n'}(\bar{\gamma}'s)$		Ths-		14			15		AEC	Gough	DCTR	72
				REQ COM: Needed are gamma ray spectra to calculate heat generation in blanket and shield, CTR,										71 71
				STATUS: ORNL Dickens ⁺ , $E_n = 0.85-20$ MeV, ORNL-4798,										72

REQ #	TARGET		REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
	* Z	A	QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
161	26	Fe	Cap Spect	$P(E_{\gamma})$		Th-	res.				15		AEC	Gough	DCTR	71
						REQ COM: Needed to calculate heat generation in blanket and shield, CTR,										71
						STATUS: Kenny, Aust, J, Phys, 24, 805 (1961),										72
162	26	Fe	Absorption		I		1-	1.5		5	to	20	ANL	Avery	DRDT	69
													GE	Snyder	DRDT	69
													LMFB	Hennig-AEC	DRDT	69
						REQ COM: Capture in 1-5 keV range of particular interest. Accuracy 5 per below 175 keV, 20 per above, Resolution 20 percent,										69
																69
						STATUS: No active work,										72
163	26	Fe	Tot $\bar{\nu}$ Prod	$\sigma(E_{\gamma})$	II		1-650				15*		SNPO	Fleishman	DSNS	69
					I			1-10			15*		SNPO	fleishman	DSNS	69
						REQ COM: *Accuracy 15 per or 5 mb whichever is greater. Absolute $\sigma(E_{\gamma})$ required for all $E_{\gamma} > 200$ keV, Neutron energy intervals required: Res. regions reproduce major variations in (E_{γ}) , > 1 MeV: 500-keV intervals, Gamma-energy resolution required: <2.5 MeV, 10 percent; >2.5 MeV, 250 keV,										69
																69
																69
						STATUS: No active work,										72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≥15	>15	LAB	PERSON	ORG	
164	^{26}Fe	Tot $\bar{\nu}$ Prod	$\sigma(E_{\bar{\nu}})$	I	Th	to	10					<15	LMFB Hemmig-AEC	DRDT	66
					REQ COM: All gamma energies of interest for fast reactor shielding,										66
					STATUS: No active work,										72
165	^{26}Fe	Tot $\bar{\nu}$ Prod	$\sigma(E_{\bar{\nu}}, E_{\gamma})$	II			8-15				10		GDFW Western	DNA	69
				I			8-16				10		LASL Biggers	DNA	69
				II			7-15				10		NEL Eccleshall	DNA	69
													AFWL. Enz	DNA	70
					REQ COM: $\Delta E = 250$ keV at 500-keV intervals										69
					$\Delta\theta = \pm 5^{\circ} (<30^{\circ}), \pm 10^{\circ} (>30^{\circ})$										69
					$\sigma(55^{\circ})$ only unless significantly anisotropic.										69
					STATUS: GRT Orphan ⁺ , Gulf-RT-A10743, $E_n = 0.86 \pm 16.7$ MeV.										72
					ORNL Dickens ⁺ , $E_n = 0.85 \pm 20$ MeV, ORNL-4798,										72
					USSR Kravcov ⁺ , 72 Kiev, $E_n = 14$ MeV,										72
166	^{26}Fe	Res Int	Capture	I	.5-	up					10-	15	KAPL Ehrlich	DNR	69
					REQ COM: Remove or correct for n,p contribution,										69
					STATUS: No active work,										72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
167	^{26}Fe	$\bar{\sigma}_n$ and $\bar{\sigma}_g$		II		to	1				10		KAPL Ehrlich	DNR	72
					REQ COM: Need $\bar{\sigma}_n$ and $\bar{\sigma}_g$ for peaks near various minima for theoretical construction of scattering and capture cross sections. A "minimum" is roughly any total cross section below 1 barn. Sample composition should be known well enough to permit isotopic synthesis of the theoretical cross section. Potential scattering for resonance analysis is also needed.										72
					STATUS: COL Rahn⁺, NSE 47, 372: $\text{Sigma}_{\text{TOT}}$ minima. RPI Block⁺, USNDC-1: $\text{Sigma}_{\text{TOT}}$ minima. ORNL Harvey⁺, USNDC-1: $\text{Sigma}_{\text{TOT}}$ minima. ORNL Harvey⁺, experiments on separated isotopes underway.										72
															72
															72
															72
															72
															72
168	^{26}Fe	J. π		III		to	1						KAPL Ehrlich	DNR	72
					REQ COM: Needed to remove ambiguities in multilevel resonance analyses. The largest resonances, and ones near deep minima, are the most important.										72
					STATUS: No active work.										72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≥15	>15	LAB	PERSON	ORG	
169	$^{54}_{26}\text{Fe}$	$\sigma_{n,\bar{g}}$	Act	II	0.025-	to	15				30	LLL	Howerton	DMA	69
					REQ COM: Required is cross section for activation of Fe^{55} in naturally occurring element, Accuracy 30 per if $\sigma > 100$ mb, 50 per if $25 \text{ mb} < \sigma < 100 \text{ mb}$; Accuracy to a factor of 2 if $1 \text{ mb} < \sigma < 25 \text{ mb}$; to a factor of 10 if $\sigma < 1 \text{ mb}$,										69
					STATUS: RPI Hockenbury ⁺ , USNDC-1: 0.1-200 keV, separated isotopes,										72
170	$^{54}_{26}\text{Fe}$	$\sigma_{n,p}$	Act	III			1-18			15		BET	Bayard	DNR	72
				II			1-18			10		HEDL	McElroy	DRDT	69
				III			6.2-13			10		NEL	Eccleshall	DNA	69
					REQ COM: Energy resolution 250 keV, 500-keV intervals For use as fluence monitor,										69
					STATUS: GEEL Paulsen, experiments underway, 1.5-6 MeV and from 12-20 MeV, ANL Meadows ⁺ has measurements underway,										72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
173	^{58}Fe	$\sigma_{n,\bar{g}}$	Act	II	.025	to	15				30	LLL	Howerton	DMA	69
				II		1-	18				10		REDL	McElroy	DRDT
					REQ COM: Required is cross section for activation of Fe^{59} in naturally occurring element, (LLL) Accuracy 30 per if $\sigma > 100$ mb, 50 per if $25 \text{ mb} < \sigma < 100 \text{ mb}$. Accuracy to a factor of 2 if $1 \text{ mb} < \sigma < 25 \text{ mb}$; to a factor of 10 if $\sigma < 1 \text{ mb}$, (LLL) For use as fluence monitor (PNWL)										69
					STATUS: RPI Hockenbury ⁺ , USNDC-1, 0.1-200 keV underway. KFK Beer, measurements planned.										72
															72
174	^{27}Co	Res Par		II	132				1			ANG	Brugger	DRDT	62
					REQ COM: 1 percent in parameters of this resonance, Needed as flux monitor,										62
					STATUS: Lucas HTS, Bird ⁺ , AAEC/PR33, p. 14(1970): $\bar{\sigma}_R$.										72
175	^{27}Co	$\sigma_{n,\bar{g}}$		II	132				1			ANG	Brugger	DRDT	62
					REQ COM: 1 percent in $\bar{\sigma}_R$ for this resonance. Needed as flux monitor,										62
					STATUS: No active work,										72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≥15	>15	LAB	PERSON	ORG	
176	^{27}Co	$\sigma_{n,\bar{g}}$	Act	I II	.025	to 1=	15 18				30	LLL HEDL	Howerton McElroy	DMA DRDT	69 69
REQ COM: Required is cross section for activation of Co^{60} in ground plus isomeric states. Accuracy 30 per if > 100 mb, 50 per if $25 \text{ mb} < \sigma < 100 \text{ mb}$, Accuracy to a factor of 2 if $1 \text{ mb} < \sigma < 25 \text{ mb}$; to a factor of 10 if $\sigma < 1 \text{ mb}$, (LLL) For use as fluence monitors, (PNWL) STATUS: KFK Beer, measurements planned.															69 69 69 69 69 69 72
177	^{27}Co	Tot $\bar{g}$ Prod	$\sigma(E_{\bar{g}})$	I I II	100=	100				15*		SNPO SNPO NEL	Fleishman Fleishman Eccleshall	DSNS DSNS DMA	69 69 70
REQ COM: (*) Accuracy 15 per or 5 mb whichever is greater. Absolute $\sigma(E_{\bar{g}})$ required for all $E_{\bar{g}} > 200 \text{ keV}$, Neutron Energy intervals required: Res. regions: reproduce major variations in $(E_{\bar{g}})$ $> 1 \text{ Mev}$: 500-keV intervals Gamma-energy resolution required: $< 2.5 \text{ MeV}$, 10 percent; $> 2.5 \text{ MeV}$, 250keV. STATUS: No active work.															69 69 69 69 69 69 69 72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
178	* $^{58}_{27}\text{Co}$	$\sigma_{n,\bar{g}}$		II	Th	to	10			10		BET	Bayard	DNR	72
					REQ COM: Thermal cross section most important; RI also needed for interpretation of $\text{Ni}^{58}(n,p)$ fluence monitor data, *Radioactive target, 9 hour isomer,										72
					STATUS: No active work,										72
179	* $^{58}_{27}\text{Co}$	$\sigma_{n,\bar{g}}$		II	Th	to	10			10		BET	Bayard	DNR	72
					REQ COM: Thermal cross section most important; RI also needed for interpretation of $\text{Ni}^{58}(n,p)$ fluence monitor data, *Radioactive target, 71.4 d half-life,										72
					STATUS: No active work,										72
180	* $^{58}_{27}\text{Co}$	J,π		III		25-	3					KAPL	Ehrlich	DNR	66
					REQ COM: Need spins and parities of excited states for Calculation of threshold reaction $\text{Ni}^{58}(n,p)$,										66
					STATUS: No active work,										72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
183	^{28}Ni	Inelastic	$\sigma(E_{n'})$	II			1-10			10		GE	Snyder	DRDT	66
												LMFB	Hennig-AEC	DRDT	66
					REQ COM: ΔE_0 and $\Delta E_{n'}$ = 10 percent, Energy resolution required to determine major structure, Total integral over kx required, Spectra at several angles if significantly anisotropic.										72
					STATUS: ORNL Perey ⁺ , ORNL-4523, 6.5-8.5 MeV, ANL Smith ⁺ , preliminary data to 3.0 MeV.										72
184	^{28}Ni	Inelastic	$\sigma(E_{n'})$			Ths-	1k			15		AEC	Gough	DOCTR	72
					REQ COM: Needed to calculate neutron transport in blanket and shield, CTR,										71
					STATUS: ANL Smith ⁺ preliminary data to 3.0 MeV, ORNL Perey ⁺ , ORNL-4523, 6.5-8.5 MeV.										72
185	^{28}Ni	$\sigma_{n,2n}$					1k			10		AEC	Gough	DOCTR	71
					REQ COM: Accuracy needed to reduce uncertainty in neutron multiplication estimates for CTR,										71
					STATUS: No active work,										72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≥15	>15	LAB	PERSON	ORG	
197	$^{58}\text{Ni}_{28}$	$\sigma_{n,p}$		II			<10		5			BET	Bayard	DNR	72
					REQ COM: For use as fast fluence monitor,										72
					STATUS: Geel Paulsen ⁺ , has measurements 1-6 MeV,										72
					ANL Meadows ⁺ , has measurements to 6 MeV,										72
198	$^{58}\text{Ni}_{28}$	$\sigma_{n,p}$	Act	III			9.4-14		10			NEL	Eccleshall	DNA	69
					REQ COM: Resolution in energy 5 per, 500-keV intervals										69
					STATUS: Geel Paulsen ⁺ , measurements in progress .02-20 MeV										72
					ANL Meadows ⁺ , measurements to 6 MeV,										72
199	$^{60}\text{Ni}_{28}$	$\sigma_{n,p}$	Act	III			2-12.5		10			NEL	Eccleshall	DNA	69

					REQ COM: Resolution in energy 5 per, 500-keV intervals										69
					STATUS: RPI Hockenbury ⁺ , USNDC-1, plan measurements,										72
200	$^{61}\text{Ni}_{28}$	$\bar{\sigma}_n$		I			1-600		4-9			KAPL	Ehrlich	DNR	69

					REQ COM: None,										69
					STATUS: RPI Hockenbury ⁺ , USNDC-1, plans measurements,										72

[illegible]

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
211	29Cu ⁶³	σ _{n,ᾱ}	Act	III II	.025	to 1-	15 18				30 10	LLL HEDL	Howerton McElroy	DMA DRDT	69 69
REQ COM: Required is cross section for activation of Cu ⁶⁴ in naturally occurring elements, (LLL) Accuracy 30 per if σ > 100 mb, 50 per if 25 mb < σ < 100 mb, Accuracy to a factor of 2 if 1 mb < σ < 25 mb; to a factor of 10 if σ < 1 mb, (LLL) For use as fluence monitor (PNwL)															
STATUS: No active work,															
212	29Cu ⁶³	σ _{n,ᾱ}	Act	II		>6				10		HEDL	McElroy	DRDT	69
REQ COM: For use as fluence monitor,															
STATUS: Hamburg, Bormann, to be published,															

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≥15	>15	LAB	PERSON	ORG	
213	$^{65}_{29}\text{Cu}$	$\sigma_{n,2n}$	Act.	III			Ths-15				30	LLL	Howerton	DMA	69
					REQ COM: Required is cross section for activation of Cu^{64} in naturally occurring element, Accuracy of 30 per if $\sigma > 100$ mb, 50 per if $25 \text{ mb} < \sigma < 100 \text{ mb}$, Accuracy to a factor of 2 if $1 \text{ mb} < \sigma < 25 \text{ mb}$; to a factor of 10 if $\sigma < 1 \text{ mb}$.										69
					STATUS: Kanda, At. Energy Research Inst. Tokyo p. 1207. Qaim, NP A185, 164 (1972), Mogharrab, Atomkernenergie 19, 107 (1972),										72
214	$^{65}_{29}\text{Cu}$	$\sigma_{n,\bar{e}}$		II	Th-	1		2-	5			ACRP Hannum	DRDT		67
					REQ COM: Accuracy 2 per near thermal Accuracy 5 per near above thermal For detector applications										67
					STATUS: HAR Moxon has data 5eV-100keV in progress,										72
215	$^{70}_{30}\text{Zn}$	Cap Spect	$P(E_{\gamma})$	I	Th					10		SNPO Fleishman	DSNS		69
					REQ COM: For shielding calculations, Both line and continuum spectra are required, Bartholomew's spectrum does not give correct B.E.										69
					STATUS: ORNL Maerker ⁺ ORNL-4382,										72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR		
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≥15	>15	LAB	PERSON	ORG			
216	^{30}Zn	Tot $\bar{n}$ Prod	$\sigma(E_{\bar{n}})$	I	200-	25				15*		SNPO	Fleishman	DSNS	69		
				I				1-10		15*		SNPO	Fleishman	DSNS	69		
				II				1-14		15*		NEL	Eccleshall	DVA	70		
				REQ COM: (*) Accuracy 15 per or 5 mb whichever is greater. Absolute $\sigma(E_{\bar{n}})$ required for all $E_{\bar{n}} > 200$ keV, Neutron Energy intervals required: Res. regions: reproduce major variations in $(E_{\bar{n}})$ > 1 Mev: 500-keV intervals Gamma-energy resolution required: < 2,5 MeV, 10 percent; > 2,5 MeV, 250 keV.													
217	$^{30}\text{Zn}^{64}$	$\sigma_{n,\bar{n}}$	Act	I	.025	to	15				30	LLL	Howerton	DMA	69		

				REQ COM: Required is cross section for activation of Zn^{65} in naturally occurring element, Accuracy of 30 per if $\sigma > 100$ mb, 50 per if 25 mb < $\sigma < 100$ mb, Accuracy to a factor of 2 if 1 mb < $\sigma < 25$ mb; to a factor of 10 if $\sigma < 1$ mb,													
				STATUS: No active work,													

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
221	³³ As	Elastic	$\sigma(\sigma_n)$	II	Th	to	1k			15		IRT	Russell	DNA	69
					REQ COM: For radiation effects,										69
					STATUS: No active work,										72
222	³³ As	Emission	$\sigma(\sigma_{n1})$	II		Ths=	1k			15		IRT	Russell	DNA	69
					REQ COM: For radiation effects,										69
					STATUS: No active work,										72
223	³⁶ Kr ⁸³	Total		II	.001-	1				10		BET	Bayard	DNR	67
												KAPL	Ehrlich	DNR	67
					REQ COM: Accuracy 10 per thermal										67
					Accuracy 10 percent in RI above 1 eV,										67
					For fission product absorption calculation										67
					STATUS: No active work,										72
224	³⁶ Kr ⁸³	$\sigma_{n,g}$		II	.001-	1				10		BET	Bayard	DNR	67
												KAPL	Ehrlich	DNR	67
					REQ COM: Accuracy 10 per thermal										67
					Accuracy 10 percent in RI above 1 eV,										67
					For fission product absorption calculation										67
					STATUS: No active work,										72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
233	^{90}Zr	$\sigma_{n,\bar{g}}$					14				20	AEC	Gough	DCTR	71
					REQ COM: Needed to calculate formation of higher mass isotopes, CTR,										71
					STATUS: No active work,										72
234	^{90}Zr	Res Int	Capture	I	.5-	up			5			KAPL	Ehrlich	DNR	69
					REQ COM: Discrepancies in existing measurements,										69
					STATUS: No active work,										72
235	^{90}Zr	$\sigma_{n,p}$					14				20	AEC	Gough	DCTR	71
					REQ COM: Needed for radiation damage estimates, CTR,										71
					STATUS: U, of Ark, Bari, activation X-section at 14.8 MeV,										72
236	^{90}Zr	$\sigma_{n,\bar{a}}$					14				20	AEC	Gough	DCTR	71
					REQ COM: Needed for radiation damage estimates, CTR,										71
					STATUS: U, of Ark, Bari, activation X-section at 14.8 MeV,										72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
237	40Zr	Cap Spect	P(E _g)	I	Th						10		SNPO Fleishman	DSNS	69
					REQ COM: For shielding calculations.										69
					Both line and continuum spectra are required.										69
					Bartholomew's spectrum does not give correct B.E.										69
					STATUS: MIT Rasmussen ⁺ , GA-10248/DASA-2570, thermal neutron capture spectrum.										72
															72
238	40Zr	σ _{n,n'} (E _n)			Th-	14				15			AEC Gough	DCTR	72
					REQ COM: Needed are gamma ray spectra to calculate heat generation in blanket and shield, CTR.										71
					STATUS: BET Glickstein ⁺ , E _n = 1,2-2,4 MeV ⁹¹ Zr. Knoxville Conf.=710301, p. 241.										72
															72
239	40Zr	Cap Spect	P(E _g)		Th-	res.				15			AEC Gough	DCTR	71
					REQ COM: Needed to calculate heat generation in blanket and shield, CTR.										71
															71
					STATUS: MIT Rasmussen ⁺ , GA-10248/DASA-2570, thermal neutron capture spectrum.										72
															72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
240	^{90}Zr	Tot $\bar{\sigma}$ Prod	$\sigma(E_{\bar{n}})$	II	100=	20				15*		SNPO	Fleishman	DSNS	69
				I			1-10			15*		SNPO	Fleishman	DSNS	69
				II			1-14			15*		REL	Eccleshall	DMA	70
					REQ COM: (*) Accuracy 15 per or 5 mb whichever is greater.										69
					Absolute $\sigma(E_{\bar{n}})$ required for all $E_{\bar{n}} > 200$ keV.										69
					Neutron Energy intervals required:										69
					Res, region: reproduce major variations in $(E_{\bar{n}})$										69
					> 1 Mev: 500-keV intervals										69
					Gamma-energy resolution required:										69
					<2.5MeV, 10 percent; >2.5MeV, 250keV.										69
					STATUS: None which satisfy criteria.										72
241	* ^{88}Zr	$\sigma_{n,\bar{g}}$		I	*****										69
					.1-300					50		LLL	Howerton	DMA	69
					REQ COM: Needed for evaluation,										69
					* Radioactive target-85 day(neutron deficient)										69
					STATUS: No active work,										72
242	* ^{89}Zr	$\sigma_{n,\bar{g}}$		I	*****										69
					.1-300					50		LLL	Howerton	DMA	69
					REQ COM: Needed for evaluation,										69
					* Radioactive target-78 hour(neutron deficient)										69
					STATUS: No active work,										72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
246	$_{40}\text{Zr}^{90}$	Inelastic	$\sigma(E_n)$	I			5-15			10		BET	Bayard	DNR	72
					REQ COM: To determine the split of the total Zr cross section between nonelastic and elastic,										72
					STATUS: U. Ky. McEllistrem ⁺ preliminary data to 6 MeV, ANL Smith preliminary results 1.5-3.0 MeV,										72
247	$_{40}\text{Zr}^{90}$	Emission	$\sigma(e_n, E_n)$	I			1-15			10		BET	Bayard	DNR	67
					REQ COM: Individual excitation cross sections desired to 20 per accuracy										67
					Needed for the design of pressurized water reactors with Zr										67
					Wanted from threshold up										67
					STATUS: U. Ky. McEllistrem ⁺ preliminary results 1.5-6 MeV, ANL Smith ⁺ , preliminary results 1.5-3.0 MeV,										72
248	$_{40}\text{Zr}^{90}$	Res Int	Capture	II	.5-	up				20		KAPL	Ehrlich	DNR	69
					REQ COM: Needed for evaluating meas. resonance parameters,										69
					STATUS: No active work,										72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR	
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG		
249	$_{40}\text{Zr}^{90}$	$\bar{\sigma}_n$ and $\bar{\sigma}_K$		II	*	-15					10		KAPL Ehrlich BET Bayard	DNR DNR	69 72	
250	$_{40}\text{Zr}^{90}$	J,π		II			1.8-5						KAPL Ehrlich	DNR	69	
															69	
															70	
															72	
251	$_{40}\text{Zr}^{91}$	Elastic	$\sigma(\theta_n)$	I	*****		100-		10			10		BET Bayard	DNR	67
																67
																67
																72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR			
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG				
252	$_{40}\text{Zr}^{91}$	Inelastic	$\sigma(\sigma_n,)$	II			2.5-10			10		BET	Bayard	DNR	72			
				II			14			15	KAPL	Ehrlich	DNR	69				
				REQ COM: Resolve discrete levels up to 2 MeV excitation,														
				To compute direct inelastic scattering and														
				investigate isotopic spin-dependent coupling														
					between ground and excited states,													
					To determine the split of the total Zr cross													
					section between nonelastic and elastic,													
					STATUS: U, Ky, McEllistrem ⁺ preliminary results 1.5-6 MeV,													
					ANL Smith ⁺ , preliminary results 1.5-3.0 MeV,													
253	$_{40}\text{Zr}^{91}$	$\sigma_{n,\alpha}$	III			14				30	KAPL	Ehrlich	DNR	69				
				REQ COM: No data available,														
				STATUS: No active work,														
254	$_{40}\text{Zr}^{91}$	Res Int	Capture	I	.5	up			5		KAPL	Ehrlich	DNR	69				
					REQ COM: Verification of existing data required,													
					STATUS: No active work,													

REQ #	TARGET * Z A	REACTION TYPE QUANTITY VARIABLE		PRI OR,	INCIDENT ENERGY eV keV MeV			PERCENT ACCURACY 1=3 4=9 <15 >15				REQUESTER LAB PERSON ORG			YR											
255	$_{40}\text{Zr}^{91}$	$\bar{\sigma}_n$ and $\bar{\sigma}_g$		I	*	-10				10		KAPL Ehrlich	DNR	69												
														BET Bayard	DNR	72										
														REQ COM: Needed to resolve serious discrepancies <4 keV and extend resolved resonance data to 10 keV, (*) energy to include lowest resolved resonance, Discrepancies still exist, incl. RPI, GGA work,												69
														STATUS: ORNL Macklin, measurements underway,												72
256	$_{40}\text{Zr}^{91}$	J, π		II			1-4					KAPL Ehrlich	DNR	69												
														REQ COM: J, π of all Zr^{91} levels <4 MeV desired for calculating compound elastic and inelastic,												69
														STATUS: No active work,												72
257	$_{40}\text{Zr}^{92}$	Elastic	$\sigma(\theta_n)$	I		100=	10			10		BET Bayard	DNR	72												
														REQ COM: Scattering from the separated isotopes 90=91, 92=94 and 96 is desired to check the shell effect on optical potential and derive useful parameters												67
														STATUS: U. Ky. McEllistrem ⁺ preliminary results 1.5-6 MeV, ANL Smith ⁺ , preliminary results 1.5=3.0 MeV,												72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
258	$_{40}\text{Zr}^{92}$	Inelastic	$\sigma(E_{n'})$	II			14				15	KAPL Ehrlich	DNR	69	
					REQ COM: Resolve discrete levels up to 2 MeV excitation, To compute direct inelastic scattering and investigate isotopic spin-dependent coupling between ground and excited states,									69	
					STATUS: No active work,									72	
259	$_{40}\text{Zr}^{92}$	Inelastic	$\sigma(E_{n'})$	I			2.5-10			10		BET Bayard	DNR	72	
					REQ COM: To determine split of total Zr cross section between nonelastic and elastic									72	
					STATUS: U. Ky, McEllistrem ⁺ preliminary results 1.5-6 MeV, ANL Smith preliminary results 1.5-3.0 MeV,									72	
260	$_{40}\text{Zr}^{92}$	Res Int	Capture	II	.5-	up					20	KAPL Ehrlich	DNR	69	
					REQ COM: Needed for evaluating meas, resonance parameters,									69	
					STATUS: No active work,									72	

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
261	^{92}Zr	$\bar{\sigma}_n$ and $\bar{\sigma}_g$		I	*	15					10		KAPL Ehrlich BET Bayard	DNR DNR	69 72
					REQ COM: (*): Energy to include lowest resolved resonance, Needed for verification of existing data, incl, recent RPI results,										69 70 70
					STATUS: ORNL Macklin measurements underway,										72
262	^{92}Zr	J, π		II			1-4						KAPL Ehrlich	DNR	69
					REQ COM: J, π of all Zr^{92} levels <4 MeV desired for calculating compound elastic and inelastic.										69 69
					STATUS: No active work,										72
263	^{94}Zr	Elastic	$\sigma(\theta_n)$	I	.5	to	10				10		BET Bayard	DNR	67

					REQ COM: Scattering from the separated isotopes 90-91 92-94 and 96 is desired to check the shell effect on the optical potential and derive useful parameters,										67 67 67 67
					STATUS: U. Ky. underway,										72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
264	$^{94}_{40}\text{Zr}$	Inelastic	$\sigma(\bullet_{n'})$	II			14			15			KAPL Ehrlich	DNR	67
					REQ COM: Resolve discrete levels up to 2 MeV excitation, To compute direct inelastic scattering and investigate isotopic spin-dependent coupling between ground and excited states,										69
					STATUS: No active work,										72
265	$^{94}_{40}\text{Zr}$	$\bar{\sigma}_n$ and $\bar{\sigma}_g$		II	*	-15				10			KAPL Ehrlich	DNR	69
					REQ COM: (*): Energy to include lowest resolved resonance, Needed for verification of existing data, incl, recent RPI results,										69
					STATUS: GRNL Macklin, measurements underway,										72
266	$^{94}_{40}\text{Zr}$	J,π		II		950-	4						KAPL Ehrlich	DNR	69
					REQ COM: J,π of all Zr^{94} levels <4 MeV desired for calculating compound elastic and inelastic,										69
					STATUS: No active work,										72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	OMG	
267	* $_{40}\text{Zr}^{95}$	$\sigma_{n,\bar{g}}$		II	.5-	10				10-	20	BET	Bayard	DNR	67
												KAPL	Ehrlich	DNR	67
					REQ COM: Accuracy: 10 percent in σ_{ABS} , if > 100 barns; 20 percent in σ_{ABS} , if from 10-100 barns Above 1 eV: 10 percent in RI, if > 1000 barns; 20 percent in RI, if from 100-1000 barns The decay is to an important fission product, *Radioactive target, 65 day,										69
					STATUS: No active work,										72
268	$_{40}\text{Zr}^{96}$	Elastic	$\sigma(\sigma_n)$	I	100-	10				10		BET	Bayard	DNR	72
					***** REQ COM: Scattering from the separated isotopes 90=91 92=94 and 96 is desired to check the shell effect on optical potential and derive useful parameters										67
					STATUS: ANL no adequate sample available,										72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
269	$_{40}\text{Zr}^{96}$	$\sigma_{n,\bar{g}}$		II	Th					5			KAPL Ehrlich	DNR	69
					REQ COM: Need to resolve discrepancies in σ 's and res. par. Preferably meas, with natural target or other isotopes. Note: Zr^{97} half-life is 16.8 hours.										69
					STATUS: No active work,										72
270	$_{41}\text{Nb}$	Inelastic	$\sigma(\Sigma_{n,1})$		Ths=	14				15			AEC Gough	DCTR	72
					REQ COM: Needed to calculate neutron transport in blanket and shield, CTR,										71
					STATUS: ANL Smith ⁺ data to 4.0 MeV in detail.										72
					AWRE Coles, 1.5-5 MeV, AWRE-O-66-71.										72
					AE Almen ⁺ , 2 to 4.5 MeV Helsinki Conf. II, p. 349.										72
271	$_{41}\text{Nb}$	$\sigma_{n,n'}$	Isom State	I	Ths=	15				20			LLL Howerton	DMA	69
					REQ COM: Needed is inelastic cross section to 13.6y isomer of Nb^{93} .										69
					STATUS: No active work,										72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
272	$^{41}_{41}\text{Nb}$	Emission	$\sigma(\theta_n, E_n)$	I			1.5-15			10			LASL Streetman	DSNS	69
					REQ COM: Low-energy neutrons must be included, Absolute spectra at 30° and 75° may suffice, Time scale requiring associated $\bar{\nu}$ -production data not yet established, Incident and exit energy resol. 10 per										69
					STATUS: ANL Smith ⁺ data to 4.0 MeV in detail. AURE Coles, 1.5-5 MeV, AURE-O-66-71, AE Almen ⁺ , 2 to 4.5 MeV Helsinki Conf, II, p. 349.										72
273	$^{41}_{41}\text{Nb}$	$\sigma_{n,2n}$					14			10			AEC Gough	DCTR	71
					REQ COM: Accuracy needed to reduce uncertainty in neutron multiplication estimates for CTR,										71
					STATUS: No active work,										72
274	$^{41}_{41}\text{Nb}$	$\sigma_{n,2n}$	$\sigma(\theta_n, E_n)$				14			15			AEC Gough	DCTR	71
					REQ COM: Energy and angular dependence of secondary neutrons needed to calculate neutron transport in blanket and shield, CTR,										71
					STATUS: No active work,										72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
275	^{41}Nb	$\sigma_{n,2n}$	Act.	I			Ths-15		≤5			LLL	Howerton	DMA	70
					REQ COM: Measurements with less accuracy not helpful,										70
					STATUS: No data to required accuracy,										72
276	^{41}Nb	$\sigma_{n,\bar{g}}$		II		1-100				10		AI	Alter	DRDT	62
				II		1-100				10		ANL	Avery	DRDT	62
				II		1-100				10		IRT	Preskitt	DRDT	62
					REQ COM: Look for non-1/v below 1 eV,										69
					For fast reactor calculations, to resolve										69
					discrepancies in thermionic reactor worths,										69
					Accuracy: 5 per in calculated dilute and self-										67
					shielded resonance integral										67
					STATUS: ORNL Macklin plans,										72
277	^{41}Nb	$\sigma_{n,\bar{g}}$					1k				20	AEC	Gough	DCTR	71
					REQ COM: Needed to calculate formation of higher										71
					mass isotopes, CTR,										71
					STATUS: No active work,										72
278	^{41}Nb	$\sigma_{n,p}$					1k				20	AEC	Gough	DCTR	71
					REQ COM: Needed for radiation damage estimates, CTR,										71
					STATUS: No active work,										72

[illegible]

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
283	$_{41}\text{Nb}$	Tot $\bar{g}$ Prod	$\sigma(E_{\bar{g}})$	II	30-	75				15*	SNPO Fleishman	DSNS	69		
				I			1-10		15*	SNPO Fleishman	DSNS	69			
				II		1-14		15*	NEL Eccleshall	DNA	70				
				REQ COM: (*) Accuracy 15 per or 5 mb whichever is greater, Absolute $\sigma(E_{\bar{g}})$ required for all $E_{\bar{g}} > 200$ keV, Neutron Energy intervals required: Res. regions: reproduce major variations in $\sigma(E_{\bar{g}})$ > 1 Mev: 500-keV intervals Gamma-energy resolution required: <2.5MeV, 10 percent; >2.5MeV, 250keV,											
284	$_{41}\text{Nb}$	Tot $\bar{g}$ Prod	$\sigma(E_{\bar{g}})$	STATUS: ORNL Dickens ⁺ , NCSAC-42, p. 195 6 MeV,										72	
				Th-	to	14		15		AEC Gough	DCTR	71			
				REQ COM: Needed for CTR applications,										71	
285	* $_{41}\text{Nb}^{91}$	$\sigma_{n,\bar{g}}$	I	STATUS: ORNL Dickens ⁺ , NCSAC-42, p. 195, 6 MeV,										72	
				***** ,1-300										69	
				REQ COM: Needed for evaluation, * Radioactive target-neutron deficient,										69	
STATUS: No active work,										72					

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
286	* $_{41}\text{Nb}^{92}$	$\sigma_{n,\bar{g}}$		I		.1-300					50	LLL	Howerton	DMA	69
					REQ COM: Needed for evaluation,										69
					* Radioactive target=10 ⁷ year (neutron deficient)										69
					STATUS: No active work,										72
287	* $_{41}\text{Nb}^{93}$	$\sigma_{n,\bar{g}}$		I		.1-300					50	LLL	Howerton	DMA	69
					REQ COM: Needed for evaluation,										69
					* Radioactive target=required is the cross										69
					section for capture by the 13.6 year Nb ⁹³ isomer										69
					STATUS: No active work,										72
288	* $_{41}\text{Nb}^{95}$	$\sigma_{n,\bar{g}}$		I	Th						20	KAPL	Ehrlich	DNR	67
					REQ COM: Thermal average will be useful										67
					Want 20 per accuracy if absorption										67
					cross section is 10-100 barns										67
					10 per if greater										67
					Decays to an important fission product poison,										67
					*Radioactive target = 35d,										69
					STATUS: No active work,										72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
289	^{42}Mo	Inelastic	$\sigma(E_{n'})$	III			1.5-3				20	ANL	Avery	DRDT	72
												LMFB	Hemmig-AEC	DRDT	62
					REQ COM: ΔE_0 and $\Delta E_{n'}$ = 20 percent, Total integral over 4π required, Spectra at several angles if significantly anisotropic.										62
					STATUS: AWRE Coles, AWRE-89/70, data to 5.0 MeV, ANL Smith ⁺ , all even isotopes to 1.6 MeV, extending to > 5 MeV. U. Ky, McEllistrem ⁺ even isotope data, 1.5-6 MeV,										72
															72
															72
290	^{42}Mo	Inelastic	$\sigma(E_{n'})$		Th=	14			15			AEC	Gough	DCTR	72
					REQ COM: Needed to calculate neutron transport in blanket and shield, CTR,										71
															71
					STATUS: AWRE Coles, AWRE-89/70, data to 5.0 MeV, ANL Smith ⁺ , all even isotopes to 1.6 MeV, extending to > 5 MeV, U. Ky, McEllistrem ⁺ even isotope data, 1.5-6 MeV.										72
															72
															72
291	^{42}Mo	$\sigma_{n,2n}$				14			10			AEC	Gough	DCTR	71
					REQ COM: Accuracy needed to reduce uncertainty in neutron multiplication estimates for CTR,										71
															71
					STATUS: No data to required accuracy,										72

[illegible]

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
299	^{42}Mo	$\sigma_{n,n'}(\bar{g})$				Th-	14			15		AEC	Gough	DCTR	71
						REQ COM: Needed are gamma ray spectra to calculate heat generation in blanket and shield, CTR.									71
						STATUS: No active work,									72
300	^{42}Mo	Cap Spect	$P(E_{\bar{g}})$			Th-	res.			15		AEC	Gough	DCTR	71
						REQ COM: Needed to calculate heat generation in blanket and shield, CTR.									71
						STATUS: Wasson ⁺ , USNDC-1, pp. 27 and 134, 6-100 keV, Cole ⁺ , NCSAC-42, 185, 10-100 keV, Chrien ⁺ , NCSAC-42, 40, 12-48 keV.									72
301	^{42}Mo	Tot $\bar{g}$ Prod	$\sigma(E_{\bar{g}})$			Th-	to	14		15		AEC	Gough	DCTR	71
						REQ COM: Needed for CTR applications,									71
						STATUS: No active work except n, Gamma below 100 keV,									72

REQ #	TARGET * Z A	REACTION QUANTITY	TYPE VARIABLE	PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR	
					eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG		
302	^{42}Mo	Tot $\bar{g}$ Prod	$\sigma(E_{\bar{g}})$	I I II	10-	9				15*		SNPO	Fleishman	DSNS	69	
							1-10			15*		SNPO	Fleishman	DSNS	69	
							1-14			15*		NEL	Eccleshall	DNA	70	
REQ COM: (*) Accuracy 15 per or 5 mb whichever is greater,																69
Absolute $\sigma(E_{\bar{g}})$ required for all $E_{\bar{g}} > 200$ keV,																69
Neutron Energy intervals required:																69
Res, regions: reproduce major variations in $\sigma(E_{\bar{g}})$																69
> 1 Mev: 500-keV intervals																69
Gamma-energy resolution required:																69
<2.5MeV, 10 percent; >2.5MeV, 250keV,																69
STATUS: ORNL Wasson* some data on 92 and 98,																72
303	* $^{42}\text{Mo}^{99}$	$\sigma_{n,\bar{g}}$		II	.001-	1					20	BET	Bayard	DNR	67	
												KAPL	Ehrlich	DNR	67	
REQ COM: Accuracy 20 per if absorption X-section in																67
range 10-100 barns, 10 per if larger,																67
Above 1eV want 20 per in RI if in range 100-1000																69
barns, 10 per if larger,																67
Decays to an important fission product,																67
*Radioactive target-67h,																67
STATUS: No active work,																72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≥15	>15	LAB	PERSON	ORG	
304	* $^{103}_{44}\text{Ru}$	$\sigma_{n,\bar{R}}$		II	.001-	1					20	RET	Bayard	DNR	67
												KAPL	Ehrlich	DNR	67
					REQ COM: 20 percent accuracy desired if cross section in range 10-1000 barns, 10 per if larger, Above 1eV want 20 per in RI if in range 100-1000 barns, 10 per if larger, Wanted for fission product poison calculations in thermal reactors, *Radioactive target= ^{104}Ru ,										67
					STATUS: No active work,										72
305	$^{45}_{45}\text{Rh}$	$\sigma_{n,\bar{R}}$		II	.5-	1					10	KAPL	Ehrlich	DNR	67
				II	.001-1						10	GE	Snyder	DRDT	67
					REQ COM: Accuracy 10 per in RI, KAPL, Energies above 1eV of interest, Want to calculate fission product poisons,										67
					STATUS: No active work,										72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
306	* $_{45}\text{Rh}^{105}$	$\sigma_{n,\bar{g}}$		II	.001-1					10		GE	Snyder	DRDT	67
					REQ COM: For calculation of fission product poisons, *Radioactive target - 36h, STATUS: No active work,										67 69 72
307	* $_{46}\text{Pd}^{107}$	$\sigma_{n,\bar{g}}$		II	.001-	10				10		BET	Bayard	DNR	67
					REQ COM: For calculation of fission product poisons Above 1eV want RI to 10 per *Radioactive target - 7×10^6 y, STATUS: No active work,										67 67 69 72
308	$_{47}\text{Ag}^{109}$	$\sigma_{n,\bar{g}}$		II	.001-1					10		GE	Snyder	DRDT	67
					REQ COM: Fission product poison STATUS: No active work,										67 72

REQ #	TARGET * Z A	REACTION TYPE QUANTITY VARIABLE	PRI OR,	INCIDENT ENERGY eV keV Mev	PERCENT ACCURACY 1-3 4-9 ≤15 >15	REQUESTER LAB PERSON ORG	YR	
309	* 52Te127	σn,γ	II	.001-1	20	KAPL Ehrlich DNR	67	
				REQ COM: 0,025eV value or thermal average useful Request pertains to the metastable state Needed for calculation of fission product poisons *Radioactive target - 105d isomer				67 67 67 69
				STATUS: No active work,				72
310	* 52Te132	σn,γ	II	.001-1	20	BET Bayard DNR	67	

				REQ COM: Accuracy 10 per if X-sec larger than 2500 barns For calculation of fission product poison Above 1eV RI wanted to 20 per if in range 2500-25000 barns, 10 per if larger, *Radioactive target-7Ah,				67 67 67 67 67
				STATUS: No active work,				72
311	* 53I133	σn,γ	II	.001- 1	20	BET Bayard DNR	67	
				REQ COM: Accuracy 10 per if X-sec larger than 9000 barns Wanted for fission product poison calculations Above 1eV RI wanted to 20 per if in range 9000-90000 barns, 10 per if larger, *Radioactive target-21h,				67 67 67 67 67
				STATUS: No active work,				72

REQ #	TARGET * Z A	REACTION TYPE		PRI OK.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR	
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ONG		
312	* $^{131}_{54}\text{Xe}$	$\sigma_{n,\bar{f}}$		II	.001-	1					10		BET GE	Bayard Snyder	DNR DRDT	67 67
					REQ COM: Fission product.											67
					Above 1eV want RI to 10 per											67
					STATUS: No active work,											72
313	* $^{133}_{54}\text{Xe}$	$\sigma_{n,\bar{f}}$		II	Th						10		GE	Snyder	DRDT	67

					REQ COM: Thermal average or 0.025eV value wanted											67
					Wanted for fission product poison calculations											67
					*Radioactive target - 5.3d,											67
					STATUS: No active work,											72
314	* $^{135}_{54}\text{Xe}$	$\sigma_{n,\bar{f}}$		II	.001-2						5		GGA	Nordheim	DRDT	67

					REQ COM: For design of thorium cycle reactors.											67
					*Radioactive target - 9.3h,											67
					STATUS: No active work,											72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
317	55 ^{Cs}	$\sigma_{n,\bar{\gamma}}$		I	.5-	1				10		GE	Snyder	DNBT	67
												BET	Hayard	DNR	67
												REQ COM: Accuracy 10 per in RI			67
												Energies above 1eV of interest			67
												For fission product poison calculations			67
												STATUS: No active work.			72
318	60 Nd 143	$\sigma_{n,\bar{\gamma}}$		I	.001-	1				10		BET	Hayard	DNR	67
												GE	Snyder	DNBT	67
												REQ COM: Accuracy 10 per in RI			67
												Energies above 1eV of interest			67
												Needed for fission product poison calculations			67
												Energy 0-1eV, 10 per in cross section			67
												STATUS: No active work.			72

REQ #	TARGET * Z A	REACTION TYPE QUANTITY VARIABLE	PRI OR.	INCIDENT ENERGY eV keV MeV			PERCENT ACCURACY 1-3 4-9 ≤15 >15				REQUESTER LAB PERSON ORG			YR
319	$^{145}_{60}\text{Nd}$	$\sigma_{n,\bar{r}}$	I	.001-	1				10		BEI	Hayard	DNR	67
											GE	Snyder	DDDT	67
											KAPL	Ehrlich	DNR	67
				REQ COM: Accuracy 10 per in RI										67
				Wanted for fission product poison calculations,										67
				Energies above 1eV of interest										67
				Energy 0-1eV, 10 per in cross section										67
				STATUS: No active work,										72
320	* $^{147}_{60}\text{Nd}$	$\sigma_{n,\bar{r}}$	I	.001-	1			5	to	20	KAPL	Ehrlich	DNR	67
											RET	Hayard	DNR	67
											GE	Snyder	DDDT	67
				REQ COM: Thermal average or 0.025 eV value wanted										67
				Accuracy 20 per if absorption X-sec in range										67
				10-100 barns										67
				10 per in range 100-1000 barns, 5 per if larger,										67
				Above 1eV want RI to 20 per in range 100-1000b,										67
				10 per in range 1000-10000 barns, 5 per if larger.										67
				Decays to important fission product,										67
				*Radioactive target-11d,										67
				STATUS: No active work,										72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
321	* $_{61}\text{Pm}^{147}$	$\sigma_{n,\bar{g}}$		I	.001-	1				10		BET	Bayard	DNR	67
												GE	Snyder	DRDT	67
												REQ COM: Needed for calculation of fission poison.			67
												Want interval 0-1eV to 10 per.			67
												Above 1eV to 10 per in RI,			67
322	* $_{61}\text{Pm}^{148}$	$\sigma_{n,\bar{g}}$		I	.001-	1				10		BET	Bayard	DNR	67
												GE	Snyder	DRDT	67

												REQ COM: Calculation of fission product poisons			67
												Cross section is wanted for the 41d isomer,			67
												*Radioactive target - 41d,			67
												< 1 eV 10 percent in G; > 10 eV, 10 percent in RI			67
												STATUS: No active work,			72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≥15	>15	LAB	PERSON	ORG	
323	* $_{61}\text{Pr}^{148}$	$\sigma_{n,\bar{e}}$		I	.001=1						10		BET Bayard GE Snyder KAPL Ehrlich	DNR DRDT DNR	67 67 67
REQ COM: Cross section for 5,4d isotope, Value at 0.025 or thermal wanted Interval .001=1eV of interest For fission product poison calculations Is X-sec 1/V, above 1 eV *Radioactive target = 5,4d.															
STATUS: No active work,															
324	* $_{61}\text{Pr}^{149}$	$\sigma_{n,\bar{e}}$		I	.001=	1						20	BET Bayard GE Snyder KAPL Ehrlich	DNR DRDT DNR	67 67 67
REQ COM: 0.025 eV value or thermal average wanted For 0=1 eV want 20 per if X-sec in range 10=1000 barns, 10 per if larger, Above 1 eV want RI to 20 per in range 1000-10000b, to 10 percent for larger X-section, *Radioactive target=53h,															
STATUS: No active work,															

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
325	* $_{61}^{151}\text{Pm}$	$\sigma_{n,\alpha}$		II	.001-	1				10		BET	Bayard	DNR	67
												GE	Snyder	DRDT	67
												REQ COM: Needed for calculation of fission product poisons			67
												0,025eV or thermal average wanted			67
												Interval 0-1eV of interest			67
326	* $_{62}^{150}\text{Sm}$	$\sigma_{n,\alpha}$		I	.001-	1		2-	5			BET	Bayard	DNR	67
												GE	Snyder	DRDT	67
												REQ COM: For calculation of fission product poisons			67
												Above 1eV want RI to 2-5 per			67
												STATUS: No active work,			72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR	
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG		
327	* 62Sm ¹⁵¹	σ _{n,g}		I	.001-	1			5				BET Bayard	DNR	67	
													GE Snyder	DRDT	67	
													KAPL Ehrlich	DNR	67	
					REQ COM: Desired energy resolution 5 per											67
					Wanted for calculation of fission product poisons											67
					Energies above 2eV of interest											67
					Want RI to 10 per											67
					*Radioactive target - 90y.											67
					STATUS: No active work,											72
328	62Sm ¹⁵²	σ _{n,g}		II	.001-	1					10		BET Bayard	DNR	67	
													GE Snyder	DRDT	67	
					REQ COM: Fission product poison											67
					Above 1eV want RI to 10 per											67
					Below 1eV, want σ to 10 per											67
					STATUS: Harker, USNDC-1, page 1,											72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
329	* $^{62}_{34}\text{Sm}^{153}$	$\sigma_{n,\gamma}$		II	.001-	1					20	BET	Bayard	DNR	67
												KAPL	Ehrlich	DNR	67
					REQ COM: For calculation of fission product poison 10 per error if X-sec is above 30000 barns Above 1eV want RI to 20 per if in range 30-300 barns, 10 per if larger, *Radioactive target-47h,										67
					STATUS: No active work,										72
330	$^{63}_{29}\text{Eu}$	$\sigma_{n,\gamma}$		II	100-	200				10		LASL	Motz	DMA	66
					REQ COM: Capture spectrum also desired to 40 per accuracy,										66
					STATUS: No active work,										72
331	$^{63}_{29}\text{Eu}$	Tot γ Prod	$\sigma(E_{\gamma})$	III		1-	15					LASL	Motz	DMA	66
					REQ COM: (*): An upper limit on $\sigma(E_{\gamma})$ spectrum as a function of neutron energy will suffice,										66
					STATUS: No active work,										72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
332	* ${}^{63}\text{Eu}^{148}$	$\sigma_{n,\bar{e}}$		I		.1-300					50	LLL	Howerton	DMA	69
					REQ COM: Needed for evaluation,										69
					* Radioactive target=54 day(neutron deficient)										69
					STATUS: No active work,										72
333	* ${}^{63}\text{Eu}^{149}$	$\sigma_{n,\bar{e}}$		I		.1-300					50	LLL	Howerton	DMA	69
					REQ COM: Needed for evaluation,										69
					*Radioactive target=97day(neutron deficient),										70
					STATUS: No active work,										72
334	* ${}^{63}\text{Eu}^{150}$	$\sigma_{n,\bar{e}}$		I		.1-300					50	LLL	Howerton	DMA	69
					REQ COM: Needed for evaluation,										69
					*Radioactive target=35 year(neutron deficient),										70
					STATUS: No active work,										72
335	${}^{63}\text{Eu}^{151}$	$\sigma_{n,2n}$	Act.	I			14			15		LLL	Howerton	DMA	69
					REQ COM: Needed for evaluation, Required is the n, 2n										69
					cross section to each isomer of Eu^{150} ,										69
					STATUS: No active work,										72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≥15	>15	LAB	PERSON	ORG	
336	$^{151}_{63}\text{Eu}$	$\sigma_{n,\bar{g}}$		II	0.001-	1		2-	5			SRL	Dessauer	DPMM	67
					REQ COM: Accuracy 2 per near thermal										67
					Accuracy 5 per in resonance region										67
					For calculation of fission product poison										67
					Energies greater than 1eV of interest to										67
					give RI to 10 per,										67
					STATUS: No active work,										72
337	$^{151}_{63}\text{Eu}$	$\sigma_{n,\bar{g}}$		I	.1-300						20	LLL	Howerton	DMA	69
					REQ COM: Needed for evaluation,										69
					STATUS: No active work,										72
338	* $^{152}_{63}\text{Eu}$	$\sigma_{n,\bar{g}}$		I	.1-300						30	LASL	Bell	DMA	70
					REQ COM: Needed for evaluation,										70
					*radioactive target, 12,ky,										70
					STATUS: LASL Harlow+ WASH-1127, prelim, data to 6keV,										70

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
339	$^{153}_{63}\text{Eu}$	$\sigma_{n,\bar{e}}$		II	.001-	1		2-	5			GE	Snyder	DRDT	67
												SRL	Dessauer	DPMM	67
					REQ COM: 2 per near thermal										67
					5 percent accuracy in resonance region										67
					For calculation of fission product poison										67
					Energies above 1eV of interest to give										67
					RI to 10 per										67
					STATUS: No active work.										72

340	* $^{154}_{63}\text{Eu}$	$\sigma_{n,\bar{e}}$		II	.001-	1				10		BET	Bayard	DNR	67
												GE	Snyder	DRDT	67
					REQ COM: Resonance parameters wanted for the calculation										67
					of fission product poisons										67
					RI wanted to 10 per										67
					Interval above 1eV of interest										67
					*radioactive target - 16y.										67
					STATUS: No active work,										72
341	* $^{154}_{63}\text{Eu}$	$\sigma_{n,\bar{e}}$		I	.1-300					30		LASL	Bell	DMA	70
					REQ COM: Needed for evaluation,										70
					*radioactive target-16y.										70
					STATUS: No active work.										72

REQ #	TARGET * Z A	REACTION TYPE QUANTITY VARIABLE	PRI OR.	INCIDENT ENERGY eV keV MeV	PERCENT ACCURACY 1-3 4-9 ≤15 >15	REQUESTER LAB PERSON ORG	YR
342	* 63Eu ¹⁵⁵	σ _{n,ē}	II	.001- 1	10	H&T Havard DNR GE Snyder DRDT	67 67
				REQ COM: Res, param needed to calculate fission product poisons Resonance integral wanted to 10 per, *radioactive target - 1.8v,			67 67 67 67
				STATUS: Can, Jour, Physics 48, 1933 gives eff, sigma thermal = 4040 ± 125 barns,			72 72
343	64Gd	Elastic σ(θ _n)	I	1.5-10	10	GE Snyder DRDT	67
				REQ COM: Desired error in (1-Cosθ)			67
				STATUS: No active work,			72
344	64Gd	Emission σ(θ _n , E _n)	I	1.5-10	15	GE Snyder DRDT	67
				REQ COM: For design of thermal reactors having appreciable quantities of Gd. Incident and exit resolution 15 per			67 67 67
				STATUS: No active work.			72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
345	64Gd	σ _{n,γ̄}		II	100-	200				10		LASL Motz	DMA	66	
					REQ COM: Capture spectrum also desired to 40 per accuracy,										66
					STATUS: No active work,										72
346	64Gd	Tot γ̄ Prod	σ(E _{γ̄})	III		1-	15				*	LASL Motz	DMA	66	
					REQ COM: (*): An upper limit on σ(E _{γ̄}) spectrum as a function of neutron energy will suffice,										66
					STATUS: No active work,										72
347	64Gd	Res Int	Capture	I	.5-	up			5			GE Snyder	DRDT	69	
					REQ COM: For evaluating resonance parameters,										69
					STATUS: No active work with natural samples,										72
348	64Gd ¹⁵⁵	σ _{n,γ̄}		I	.5-	1			5			GE Snyder	DRDT	67	
					REQ COM: Accuracy 5 per in RI										67
					Energies above 1eV of interest										67
					STATUS: No active work,										72

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REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
349	$^{155}_{64}\text{Gd}$	Res Int	Capture	I	.5-	up			5			GE	Snyder	DRDT	69
					REQ COM: For evaluating resonance parameters,										69
					STATUS: No active work,										72
350	$^{155}_{64}\text{Gd}$	$\bar{\sigma}_n$ and $\bar{\sigma}_K$		I	*-	.5			10			GE	Snyder	DRDT	69
					REQ COM: Required to verify existing measurements,										69
					* energy to include lowest resolved resonance,										69
					STATUS: No active work,										72
351	$^{156}_{64}\text{Gd}$	$\sigma_{n,R}$		I	***** .001-	1			5			GE	Snyder	DRDT	67
					REQ COM: In range .001-1eV 5 per accuracy is wanted										67
					Above 1eV want to calculate RI to 5 per										67
					For calculation of burn up in thermal reactors										67
					STATUS: No active work,										72
352	$^{156}_{64}\text{Gd}$	Res Int	Capture	I	.5-	up			5			GE	Snyder	DRDT	69
					REQ COM: For evaluating resonance parameters,										69
					STATUS: No active work,										72

REQ #	TARGET * Z A	REACTION TYPE QUANTITY VARIABLE	PRI OR,	INCIDENT ENERGY eV keV MeV	PERCENT ACCURACY 1-3 4-9 ≤15 >15	REQUESTER LAB PERSON ORG	YR
357	⁶⁶ Dv	$\sigma_{n,\bar{g}}$	II	100- 200	10	LASL Motz DMA	66
				REQ COM: Capture spectrum also desired to 40 per accuracy,			66
				STATUS: No active work,			72
358	⁶⁶ Dv	Tot $\bar{g}$ Prod $\sigma(E_{\bar{g}})$	III	1- 15	*	LASL Motz DMA	66
				REQ COM: (*): An upper limit on $\sigma(E_{\bar{g}})$ spectrum as a function of neutron energy will suffice,			66
				STATUS: No active work,			72
359	* ⁶⁹ Tm ¹⁶⁷	$\sigma_{n,\bar{g}}$	I	.1-300	50	LLL Howerton DMA	69
				REQ COM: Needed for evaluation,			69
				*Radioactive target-9,3day(neutron deficient),			70
				STATUS: No active work,			72
360	* ⁶⁹ Tm ¹⁶⁸	$\sigma_{n,\bar{g}}$	I	.1-300	50	LLL Howerton DMA	69

				REQ COM: Needed for evaluation,			69
				*Radioactive target-93day(neutron deficient),			70
				STATUS: No active work,			72

[illegible]

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR										
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG											
364	* $_{80}\text{Tl}^{171}$	$\sigma_{n,\bar{g}}$		1	Th-	1				10		BMA	Leonard	DPMH	67										
												SRL	Dessauer	DPMH	67										
												REF. COM: For production and burn up of thulium.													66
												*radioactive target - 1.9 year.													69
												STATUS: No active work.													72
365	* $_{71}\text{Lu}^{173}$	$\sigma_{n,\bar{g}}$		1		.1-300					50	LLL	Howerton	DMA	69										
												REF COM: Needed for evaluation.													69
												* radioactive target-1.4 year(neutron deficient)													69
												STATUS: No active work.													72
366	* $_{71}\text{Lu}^{174}$	$\sigma_{n,\bar{g}}$		1		.1-300					50	LLL	Howerton	DMA	69										

												REF COM: Needed for evaluation.													69
												*radioactive target-isomeric pair. Lu^{174m} 140 d.													70
												Lu^{174g} 1200 d.													70
367	$_{71}\text{Lu}^{175}$	$\sigma_{n,2n}$	Act.	1		Ths-15						LLL	Howerton	DMA	70										
												REF COM: Measurements with less accuracy not helpful.													70
												STATUS: No active work.													72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	kev	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
368	$_{71}^{175}\text{Lu}$	$\sigma_{n,\bar{g}}$		I	1,-300						20	LLL	Hovertan	DMA	69
					REQ COM: Needed for evaluation,										69
					STATUS: Hacken ⁺ (NCSAG-12, 61).										72
369	$_{72}^{\text{Hf}}$	Elastic	$\sigma(E_n)$	II	1.5-10					10		BET	Hayard	DNR	66
					REQ COM: Accuracy 10 per in avg. (1-cos).										66
					Wanted for thermal reactor design,										66
370	$_{72}^{\text{Hf}}$	Emission	$\sigma(E_n)$	II	1.5-10					15		BET	Hayard	DNR	66
					REQ COM: For design of thermal reactors having										66
					appreciable quantities of Hf.										66
370	$_{72}^{\text{Hf}}$	Emission	$\sigma(E_n)$	II	1.5-10					15		BET	Hayard	DNR	66
					Incident and exit energy resolution 15 per.										66
					STATUS: No active work,										72

REQ #	TARGET * Z A	REACTION TYPE QUANTITY VARIABLE	PRI OR.	INCIDENT ENERGY eV keV MeV			PERCENT ACCURACY 1-3 4-9 ≤15 >15				REQUESTER LAB PERSON ORG			YR	
371	72Hf	$\sigma_{n,\bar{\gamma}}$	II	200-	50					20	HET	Hayard	DNR	62	
			I	.001-1						2	HET	Hayard	DNR	62	
			I	.001-1						2	KAPL	Enrlich	DNR	62	
				REQ COM: Needed for Monte Carlo calculations of burn up in thermal reactors, <1ev.										62	
				S-wave strength functions are wanted to 20 per at energies > 1ev.										62	
				For fast reactor calc. incl. burn up, > 200 ev.										62	
				STATUS: No active work on natural sample.										72	
372	72Hf ¹⁷⁴	$\sigma_{n,\bar{\gamma}}$	I	.001-	5					10-	20	KAPL	Enrlich	DNR	66
				REQ COM: Thermal value wanted to 20 percent, 10-100 ev, $\bar{\sigma}_{\text{tot}}$, $\bar{\sigma}_n$, and $\bar{\sigma}_{\bar{\gamma}}$ to 10 percent.										66	
				0.1- 5 keV, $\bar{\sigma}_{\text{tot}}$, $\bar{\sigma}_n$, and $\bar{\sigma}_{\bar{\gamma}}$ to 20 percent.										66	
				Needed for Monte Carlo burn up calculations,										66	
				Need average p-wave capture width to 20 per.										66	
				STATUS: No active work.										72	

REQ #	TARGET * Z A	REACTION TYPE QUANTITY VARIABLE	PRI OR,	INCIDENT ENERGY eV keV MeV	PERCENT ACCURACY 1-3 4-9 ≤15 >15	REQUESTER LAB PERSON ORG	YR
373	72 ^{Hf} 176	σ _{n,ḡ}	I	.001- 5	10- 40	BET Bayard DNR KAPL Ehrlich DNR	62 62
REQ COM: Detailed accuracies as stated below:							66
Thermal value wanted to 20 percent,							66
Less than 1 eV to 40 percent.							66
10-100 eV, ḡ _{tot} , ḡ _n , and ḡ _ḡ to 10 percent.							66
0.1- 5 keV, ḡ _{tot} , ḡ _n , and ḡ _ḡ to 20 percent,							66
P-wave ḡ _ḡ avg, to 20 percent.							66
S-wave strength function to 40 percent,							66
Needed for Monte Carlo burn up calculations.							66
STATUS: No active work,							72
374	72 ^{Hf} 177	σ _{n,ḡ}	I	.001- 5	4 to 20	BET Bayard DNR KAPL Ehrlich DNR	62 62
REQ COM: Detailed accuracies as stated below:							66
Less than 1 eV to 4 percent,							66
10-100 eV, ḡ _{tot} , ḡ _n , and ḡ _ḡ to 10 percent,							66
0.1- 5 keV, ḡ _{tot} , ḡ _n , and ḡ _ḡ to 20 percent.							66
5.89, 6.57, and 8.87 eV res. widths to 5 per.							66
1,099 and 2,385 eV res. widths to 3 percent,							66
S-wave strength function to 20 percent,							66
Needed for Monte Carlo burn up calculations,							66
Need average p-wave capture width to 20 per,							66
STATUS: BCNN Rohr, Budapest Conf,							72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
375	72Hf ¹⁷⁸	σ _{n,ġ}		I	.001-	5		3-	=	to	20	BET	Bayard	DNR	62
												KAPL	Ehrlich	DNR	62
					REQ COM: Detailed accuracies as stated below:										66
					Less than 1 eV to 5 percent,										66
					10-100 eV, Ġ _{tot} , Ġ _n , and Ġ _ġ to 10 percent,										66
					0.1- 5 keV, Ġ _{tot} , Ġ _n , and Ġ _ġ to 20 percent,										66
					P-wave Ġ _ġ avg. to 20 percent,										66
					7.78 - eV res, width to 3 percent,										66
					S-wave strength function to 20 percent,										66
					Needed for Monte Carlo burn up calculations,										66
					STATUS: No active work,										72
376	72Hf ¹⁷⁹	σ _{n,ġ}		I	.001-	5		5	to	20	BET	Bayard	DNR	62	
												KAPL	Ehrlich	DNR	62
					REQ COM: Detailed accuracies as stated below:										66
					Less than 1 eV to 5 percent,										66
					10-100 eV, Ġ _{tot} , Ġ _n , and Ġ _ġ to 10 percent,										66
					0.1- 5 keV, Ġ _{tot} , Ġ _n , and Ġ _ġ to 20 percent,										66
					P-wave Ġ _ġ wanted to 20 percent,										66
					5.68 - eV res, widths to 5 per,										66
					S-wave strength function to 20 percent,										66
					Needed for Monte Carlo burn up calculations,										66
					STATUS: No active work,										72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR									
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG										
377	72Hf ¹⁸⁰	σ _{n,ḡ}		I	.001-	5			4	to	20	BET	Bayard	DNR	67									
												KAPL	Ehrlich	DNR	67									
												REQ COM: Detailed accuracies as stated below:												
												Less than 1 eV to 4 percent,												
												10-100 eV, Ḡ _{tot} , Ḡ _n , and Ḡ _ḡ to 10 percent,												
												0.1- 5 keV, Ḡ _{tot} , Ḡ _n , and Ḡ _ḡ to 20 percent,												
378	73Ta	Emission	σ(θ _n , E _n)	III			1.5-15			10		LASL	Streetman	DSNS	69									
												REQ COM: Low-energy neutrons must be included,												
												Absolute spectra at 30° and 75° may suffice,												
												Time scale requiring associated ḡ-production data												
												not yet established,												
												STATUS: None which satisfy criteria,												

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
379	^{73}Ta	$\sigma_{n,\bar{g}}$		I		1-	10		5-	10			AI Alter	DNDT	69
				II	1-	500			5-	10			KAPL Ehrlich	DNR	69
				II	1-	500			5-	10			LMFB Hennig-AEC	DRDT	69
					REQ COM: ~1 eV-1keV, accuracy 10 percent, 20 useful, 1-150 keV, accuracy 5 percent, 10 useful, 150-500 keV, accuracy 10 percent, 20 useful, For fast breeder control and burnup calculation,										69
					STATUS: LLL Czirr ⁺ , USNDC-1, RPI Block ⁺ , USNDC-1, plan measurements to 80 keV,										72
380	^{73}Ta	Tot $\bar{g}$ Prod	$\sigma(E_{\bar{g}})$	I	4-	1.4				15*			SNPO Fleishman	DSNS	69
				I			1-10			15*			SNPO Fleishman	DSNS	69
					REQ COM: (*) Accuracy 15 per or 5 mb whichever is greater, Absolute $\sigma(E_{\bar{g}})$ required for all $E_{\bar{g}} > 200$ keV, Neutron Energy intervals required: Res. regions: reproduce major variations in $\sigma(E_{\bar{g}})$ > 1 MeV: 500-keV intervals Gamma-energy resolution required: <2.5MeV, 10 percent; >2.5MeV, 250keV,										69
					STATUS: ORNL Morgan ⁺ , X-sections and spectra from $E_{\bar{g}} = 1$ to 10.5 MeV, $E_n = 7$ keV to 20 MeV observed at 90 and 125 degrees, ORNL-TM-3702,										72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
381	74 ^W	Emission	$\sigma(E_n, E_n')$	I			4-14			10		AFWL	Enz	DNA	69
				II			4-14			10		GDFW	Western	DNA	66
				III			1.5-15			10		LASL	Streetman	DSNS	69
				II			2-15			10		NEL	Eccleshall	DNA	69
				I			4-16			5		ORNL	Clifford	DRDT	66
				REQ COM: $\Delta\theta = 10^\circ$; spectra at a few angles <u>may</u> suffice, ΔE (Inc. and Exit) = 500 keV; 500-keV increments or as required by structure, DASA, DSNS ΔE (Inc.) ≤ 5 per; $\Delta E_n < 500$ keV. DRDT Low-energy neutrons must be included. Absolute σ 's for shielding required. Time scale requiring associated gamma production data not yet established. DSNS											
STATUS: ANL work planned,													72		

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
382	^{74}W	Tot $\bar{\nu}$ Prod	$\sigma(E_{\bar{\nu}})$	I	2-	2.5				15*		SNPO	Fleishman	DSNS	69
				I			1-10		15*		SNPO	Fleishman	DSNS	69	
				II		1-1k		15*		NEL	Eccleshall	DNA	70		
				REQ COM: (*) Accuracy 15 per or 5 mb whichever is greater, Absolute $\sigma(E_{\bar{\nu}})$ required for all $E_{\bar{\nu}} > 200$ keV, Neutron Energy intervals required: Res, regions: reproduce major variations in $\sigma(E_{\bar{\nu}})$ > 1 MeV: 500-keV intervals Gamma-energy resolution required. <2.5 MeV, 10 percent; >2.5 MeV, 250 keV,											
383	^{74}W	Tot $\bar{\nu}$ Prod	$\sigma(E_{\bar{\nu}}, E_{\gamma})$	I		100-	16			20	ORNL	Clifford	ORNL	63	
				REQ COM: For space reactor shielding. All gamma energies of interest,											
				STATUS: ANL work planned, TNC Tucker ⁺ , DASA-2333, 5-11 MeV. ORNL Morgan ⁺ , $E_{\gamma} = 1-20$ MeV, in progress.											

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
384	74^{180}	$\sigma_{n,\bar{e}}$	Act	I	0.025-	to	15				30	LLL	Howerton	DMA	69
					REQ COM: Required is cross section for activation of ^{181}W in naturally occurring element, Accuracy of 30 per if $\sigma > 100 \text{ mb}$, 50 per if $25 \text{ mb} < \sigma < 100 \text{ mb}$, Accuracy to a factor of 2 if $1 \text{ mb} < \sigma < 25 \text{ mb}$; to a factor of 10 if $\sigma < 1 \text{ mb}$.										69
					STATUS: No active work,										72
385	74^{182}	$\sigma_{n,2n}$	Act.	I	*****						30	LLL	Howerton	DMA	69
					REQ COM: Required is cross section for activation of ^{181}W in naturally occurring element, Accuracy of 30 per if $\sigma > 100 \text{ mb}$, 50 per if $25 \text{ mb} < \sigma < 100 \text{ mb}$, Accuracy to a factor of 2 if $1 \text{ mb} < \sigma < 25 \text{ mb}$; to a factor of 10 if $\sigma < 1 \text{ mb}$.										69
					STATUS: No active work,										72
386	74^{182}	$\sigma_{n,\bar{e}}$		I	1-	10			10			AI	Alter	DRDT	69
					REQ COM: Fast breeder control and burn up calculations,										69
					STATUS: ANL work planned, COL Camarda ⁺ to be published in PR/C.										72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
387	74^{183}	$\sigma_{n,\bar{e}}$		I		1-	10			10		AI	Alter	DNDD	69
					REQ COM: Fast breeder control and burn up calculations,										69
					STATUS: ANL work planned (Sample not available),										72
					COL Camarda ⁺ to be published in PR/C,										72
388	74^{184}	$\sigma_{n,\bar{e}}$		I		10-	10			10		AI	Alter	DNDD	69
					REQ COM: Fast breeder control and burn up calculations,										69
					STATUS: ANL work planned,										72
					COL Camarda ⁺ to be published in PR/C,										72
389	74^{184}	$\sigma_{n,\bar{e}}$	Act	I	.025-	100				30		LLL	Howerton	DMA	69
					REQ COM: Required is cross section for activation of w^{185} ,										69
					in naturally occurring element,										69
					STATUS: No active work,										72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	.keV	MeV	1-3	4-9	≥15	>15	LAB	PERSON	ORG	
390	74^{186}W	$\sigma_{n,2n}$	Act.	I			Ths-15				30	LLL	Howerton	DMA	69
					REQ COM: Required is cross section for activation of ^{185}W , in naturally occurring element, Accuracy of 30 per if $\sigma > 100$ mb, 50 per if 25 mb $< \sigma < 100$ mb, Accuracy to a factor of 2 if 1 mb $< \sigma < 25$ mb; to a factor of 10 if $\sigma < 1$ mb, STATUS: No active work,										69 69 69 69 69 72
391	74^{186}W	$\sigma_{n,\bar{g}}$		I		10-	10			10		AI	Alter	DRDT	69
					REQ COM: Fast breeder control and burn up calculations, STATUS: C&L Camarda ⁺ to be published in PR/C, ANL work planned,										69 72 72
392	76^{186}Os	$\sigma_{n,\bar{g}}$		III		1-100				4-9		ORNL	Macklin	DPR	70
					REQ COM: Need avg, capture for Maxwellian spectrum with kT = 30 keV, for nucleosynthesis studies. STATUS: No active work,										70 70 72

[illegible]

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
396	^{82}Pb	Emission	$\sigma(\theta_n, E_n)$	II			3-15			10		NEL	Eccleshall	DNA	69
				II			2-16		5			ORNL	Clifford	DNDT	63
					REQ COM: Energy intervals 500 keV; ΔE (res.)=250 keV, $\sigma(\theta)$ only if significantly anisotropic; then $\Delta\theta = \pm 3^\circ$ at 10-degree intervals.										69
					STATUS: No active work.										72
397	^{82}Pb	Tot $\bar{R}$ Prod	$\sigma(E_g)$	II			8-15			10		NEL	Eccleshall	DNA	69
					REQ COM: Spectra at a few energies would suffice, $\Delta E_n = 1 \text{ MeV}$, $\Delta E_g = 500 \text{ keV}$ Omit 14.8 MeV point.										69
					STATUS: ORNL Dickens ⁺ , NCSAC=42, 194, 4.9-8.0 MeV, TNC Buchanan ⁺ , ORG=2791=32, Pb=206, 207, 208; (1-5 MeV, 14.8 MeV).										72
															72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
398	82Pb	Tot $\bar{\nu}$ Prod	$\sigma(E_{\bar{\nu}})$	II I	80-	800				15*		SNPO Fleishman	DSNS	69	
							1=10			15*		SNPO Fleishman	DSNS	69	
					REQ COM: (*) Accuracy 15 per or 5 mb whichever is greater, Absolute $\sigma(E_{\bar{\nu}})$ required for all $E_{\bar{\nu}} > 200$ keV,									69	
					Res. regions: reproduce major variations in $\sigma(E_{\bar{\nu}})$ > 1 MeV: 500-keV intervals Gamma-energy resolution required: <2.5MeV, 10 percent; >2.5MeV, 250keV,									69	
					STATUS: GRNL Dickens ⁺ , NCSAC-42 194, 4.9-8.0 MeV, USSR Degtjarev ⁺ , IZV 35 2341, 0.1-3.4 MeV, TNC Buchanan ⁺ , ORG-2791-32, Pb-206, 207, 208; (1-5 MeV, 14.8 MeV),									72	
399	82Pb ²⁰⁴	$\sigma_{n,n'}$	Isom State	I	*****			Ths=15			30	LLL Howerton	DMA	69	
					REQ COM: Required is $\sigma_{n,n'}$ to 2.2 MeV isomer (67 min.)									69	
					STATUS: No active work,									72	

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
400	82 ^{Pb} 208	$\sigma_{n,\bar{f}}$	Act	II	.025	to	15				30	LLL	Howerton	DMA	69
REQ COM: Required is cross section for activation of Pb ²⁰⁹ , in naturally occurring element, Accuracy of 30 per if $\sigma > 100$ mb, 50 per if 25 mb < $\sigma < 100$ mb, Accuracy to a factor of 2 if 1 mb < $\sigma < 25$ mb; to a factor of 10 if $\sigma < 1$ mb,															
STATUS: ORNL Allen ⁺ , to be published.															
401	90 Th	Elastic	$\sigma(E_n)$	III			1-5			10		ANL	Avery	DRDT	72
REQ COM: None															
STATUS: No active work.															
402	90 Th	Inelastic	$\sigma(E_{n'})$	III			1-4		5			ANL	Avery	DRDT	72
REQ COM: Accuracy 20 percent in $(1-\cos\theta)$ if anisotropic, Incident and exit energy resolution 20 per,															
STATUS: No active work.															
403	90 Th	$\sigma_{n,2n}$		I			$T_{hs}=10$			10		GE	Snyder	DRDT	67
REQ COM: Needed for control of U ²³² production,															
STATUS: No active data.															

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR	
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG		
404	90Th	$\sigma_{n,\bar{e}}$		I	.5-	2			5-	10			BET	Bayard	DNR	62
					REQ COM: Need < 5 per in res, integ., 10 per useful For thermal breeder calculations,										62	
					STATUS: CGL, Rahn ⁺ , data to be published, should give at least 10 per in RI; see NCSAC-42,										72	
405	90Th	Absorption		II	100	to	1	3-	5				BET	Bayard	DNR	69
					REQ COM: Accuracy 5 per below 10 keV, 3 per above, Intermediate accuracy would be useful,										69	
					STATUS: CGL, Rahn ⁺ , data to be published, see NCSAC-42,										72	
406	90Th	Tot $\bar{e}$ Prod	$\sigma(E_{\bar{e}})$	II		500	~15			10			AFWL	Enz	DNA	69
					REQ COM: Spectra at a few energies may suffice, $\Delta E_n = 10$ percent; $\Delta E_{\bar{e}} = 250$ keV,										69	
					STATUS: No active data,										72	
407	90Th	Tot $\bar{e}$ Prod	$\sigma(E_{\gamma}, E_{\bar{e}})$	II	.5	to	10			10			BET	Bayard	DNR	67
					REQ COM: Need gamma spectrum at intervals of 0.5 MeV, DRDT Gammas of all energies of interest, DRDT Data needed for shielding and gamma heating calc,										67	
					STATUS: BNL von Egidy ⁺ , fast chopper, Resonance spectra for first 4 resonances + thermal,										72	
															72	

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
412	92U ²³³	Emission	$\sigma(E_n)$	I			5-15				20	LLL	Howerton	DMA	70
					REQ COM: Energy range of interest: $0.2\text{MeV} \leq E_n \leq E_n$.										70
					STATUS: No active data.										72
413	92U ²³³	$\sigma_{n,2n}$		II			Ths=15			10		LASL	Barr	DMA	67
				III			Ths=15			10		ACRP	Hannum	DRDT	67
					REQ COM: For contamination of U ²³³ by U ²³² , DRDT.										67
					STATUS: No active data.										72
414	92U ²³³	$\sigma_{n,f}$		I	.001-	1		.5-	5			BET	Bayard	DNR	62
										10		GGA	Nordheim	DRDT	62
												ORNL	Perry		62
					REQ COM: Want eta to 1/4 per below 1eV.										69
					Want integral eta to 1 per below 1 keV										69
					STATUS: LLL Behrens ⁺ have measurements in progress above										72
					0.01 eV, see NCSAC-42,										72
					BCM ⁺ Deruytter ⁺ , relative to ¹⁰ B, from 0.01-45 eV,										72
					in progress, EANDC(E)150/U,										72
					SAC Blons, data at liquid N temp., to be pub, NSE.										72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR	
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG		
415	92U ²³³	$\sigma_{n,f}$		III		1-30			5				ANL	Avery	DRDT	62
													BET	Bayard	DNR	62
													GGA	Nordheim	DRDT	62
													LMFB	Hemmig-AEC	DRDT	62
													ORNL	Perry	DRDT	62
					REQ COM: Want 2 per in eta and integral eta										69	
					STATUS: LLL Behrens ⁺ measurements in progress; NCSAC-42.										72	
					RPI Block ⁺ plan measurements,										72	
					SAC Blons. data at liquid N temp., to be pub, NSK,										72	
416	92U ²³³	Fis Ratio	wrt U ²³⁵	I	10-	15	1					LASL	Hansen	DMA	67	
				II	1-	10	1					LMFB	Hemmig-AEC	DRDT	69	
				REQ COM: Calibration in energy 1 per, resolution 3 per Accuracy of 2-3 per would be useful										69		
					STATUS: LLL Behrens ⁺ measurements in progress; NCSAC-42.										72	
					RPI Block ⁺ plan measurements below 200 keV,										72	
					ANL Poenitz ⁺ measurements in progress, .15-3.5 MeV										72	

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
417	$^{233}_{92}\text{U}$	Nu Bar		I	,001-	30		,25	-2			BET	Bayard	DNR	69
												GGA	Nordheim	DRDT	66
												ORNL	Perry	DRDT	69
												REQ COM: Need 1/4 per to 30 eV, 1 per 0.3 eV - 1 keV			69
												Need 2 per 1-30 keV			69
												Intermediate accuracy of 1.5 per useful			69
												STATUS: RPI Reed ⁺ have measurements in progress, thermal			72
												to 200 eV and 24 keV.			72
												BET	Bayard	DNR	69
												GGA	Nordheim	DRDT	69
418	$^{233}_{92}\text{U}$	Nu Bar		II		30-	3	1-3				ORNL	Perry	DRDT	69
												REQ COM: Is there structure below 1 MeV.			69
												STATUS: AUA Walsh ⁺ find evidence for structure (~2 per)			72
												below 1 MeV,			72
												LLL Howe ⁺ plan measurements, NCSAC-42,			72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
419	$^{92}\text{U}^{233}$	Alpha		I	,001-	1		2-	8			BET	Bayard	DNR	62
												GGA	Nordheim	DRDT	62
												ORNL	Perry	DRDT	62
												REQ COM: 1/4 per in eta below 1eV, 1 per useful			69
												1/4 per in eta to 3eV,			69
420	$^{92}\text{U}^{233}$	Alpha		II		1-	3					1 per in eta 30eV to 1 keV, 5 per useful			69
												Capture cross section equally useful,			69
												STATUS: Weston ⁺ estimate uncertainties in eta 0.5 per < .2			72
												eV up to 1 per at 1eV; <2 keV ~2 per integral eta			72
												ANL	Avery	DRDT	62
421	$^{92}\text{U}^{233}$	Nu Bar	Prompt	I			7-20	3				BET	Bayard	DNR	62
												GGA	Nordheim	DRDT	62
												LMFB	Hemmig=AEC	DRDT	67
												ORNL	Perry	DRDT	62
												REQ COM: Want 2 per in eta and integral eta			69
422	$^{92}\text{U}^{233}$	Nu Bar	Prompt	I			7-20	3				from 1 keV to 30 keV			69
												Capture cross section equally useful			69
												STATUS: No active work,			72
												LLL	Howerton	DMA	62
												REQ COM: Inconsistent results obscure energy dependence,			62
423	$^{92}\text{U}^{233}$	Nu Bar	Prompt	I			7-20	3				STATUS: LLL Howe ⁺ plan measurements to 15 MeV; NCSAC=42,			72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	10-15	>15	LAB	PERSON	ORG	
422	92U ²³³	Res Par		II	Th-	5					10-	30	ANL Avery	DRDT	67
													BET Bayard	DNR	67
													LMFB Hennig-AEC	DMDT	67
					REQ COM: For thermal breeder calculations										67
					Multilevel params., statistical dist, in eV range,										67
					Want 10 per accuracy to 100 eV, 20-30 per to 5 keV										67
					STATUS: COL Felvinci ⁺ have analysis in progress, USNDC-1,										72
					LASL Keyworth ⁺ have measurements of J, K in										72
					progress at GRELA,										72
					Blons ⁺ single-level analysis completed to 100 eV,										72
					100-150eV in progress, EANDC(E) 150/U,										72
423	92U ²³³	Cap Spect	P(E _γ)	II	.01-15						15		BET Bayard	DNR	67
					REQ COM: ΔN(E)/N(E) needed to 15 per every 50keV in E _γ ,										67
					Gammas of 100 keV and above desired, for shielding										67
					Are thermal and resonance spectra the same,										67
					STATUS: No active work,										72
424	92U ²³³	Delayed γ Y	P(E _γ , T ^{1/2})	I		2, 14					35		BNL Kouts	DNMS	69
					REQ COM: Accuracy refers to rel, intensities of delayed										70
					gammas from fission, E _γ > 2MeV and 10 usec < t < 1 hr										70
					Absolute gamma yields to factor of 2 also useful,										70
					STATUS: No active work,										72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR	
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG		
425	92 ^{U233}	Fis Prod Y	of Xe ¹³⁵	II	Th				3				BET	Bayard	DNR	67
					REQ COM: For calculation of fission product poisons, Cumulative and direct yields required, inclusive of 15 minute isomer,											67
					STATUS: GE Meek and Rider compilation reviews status, NEDG-12154,											72
426	92 ^{U233}	Fis Prod Y	of Cs ¹³⁷	II	Th				1				BET	Bayard	DNR	67
					REQ COM: For burnup indicator standards,											67
					STATUS: GE Meek and Rider compilation reviews status, NEDG-12154,											72
427	92 ^{U233}	Fis Prod Y	of Nd ¹⁴⁷	II	Th				3				BET	Bayard	DNP	67
					REQ COM: For calculation of fission product poisons,											67
					STATUS: GE Meek and Rider compilation reviews status, NEDG-12154,											72
428	92 ^{U233}	Fis Prod Y	of Sm ¹⁴⁹	II	Th				3				BET	Bayard	DNR	67
					REQ COM: For calculation of fission product poisons,											67
					STATUS: GE Meek and Rider compilation reviews status, NEDG-12154,											72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
429	92U ²³⁴	σ _{n,2n}	Act.	I			Ths=15		≤5			LLL	Howerton	DMA	70
					REQ COM: Measurements with less accuracy not helpful,										70
					STATUS: No active work,										72
430	92U ²³⁴	σ _{n,3n}		II			Ths=15				20	LASL	Barr	DMA	67
					REQ COM: None,										67
					STATUS: No active work,										72
431	92U ²³⁴	σ _{n,γ}		II	.001	to	10	3	to	10		AI	Alter	DRDT	69
												ANL	Avery	DRDT	69
					REQ COM: To evaluate isotope buildup in thermal reactors,										67
					Accuracy 3 per below 2 eV, 6 per below 10 keV,										69
					STATUS: RPI Block ⁺ , plan to make capture measurements,										72
432	92U ²³⁴	Nu Bar	Prompt	I		500-	20	3				LLL	Howerton	DMA	62
					REQ COM: None,										62
					STATUS: No active work,										72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ONG	
433	92U ²³⁵	Elastic	$\sigma(\theta_n)$	II II II			1-5 1-5 1-7				20 20 10	ANL LMFB LASL	Avery Hemmig-AFC Diven	DRDT DRDT DMA	69 69 66
					REQ COM: Needed for analyzing fast critical experiments, Energy resolution at least 0.5 MeV										69 69
					STATUS: BCMN Coppola and Knitter have data to 5.5 MeV. ANL Smith, measurements to 3.5 MeV,										72 72
434	92U ²³⁵	Inelastic	$\sigma(E_n)$	II II I		50- 50- 1.5-6	6 6 6			10 10 5		ANL LMFB LLL	Avery Hemmig-AFC Howerton	DRDT DRDT DMA	69 72 69
					REQ COM: Incident and exit energy resolutions 10 per, DRDT Discrim. between inelastic and fission neutrons, required, LLL Low energy neutrons must be included (~300 keV). Absolute spectra at 30° and 75° may suffice.										69 69 69 69 69
					STATUS: BCMN Coppola and Knitter have data to 5.5 MeV, ANL Smith, measurements to 3.5 MeV,										72 72
435	92U ²³⁵	Emission	$\sigma(E_n)$	I			5-15				20	LLL	Howerton	DMA	70
					REQ COM: Energy range of interest: $0.2\text{MeV} \leq E_n \leq E_n$.										70
					STATUS: BCMN Coppola and Knitter have data at 5.5 MeV.										72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
436	92U ²³⁵	Emission	$\sigma(\theta_n, E_n)$	I			6-20		5			LLL	Howerton	DMA	62
				I			6-16		5			LASL	Diven	DMA	69
				II			1-7		5-10			LASL	Diven	DMA	69
				REQ COM: Low-energy neutrons must be included (~300 keV). Absolute spectra at 30° and 75° may suffice,											69
437	92U ²³⁵	$\sigma_{n,2n}$	Act.	I			Ths-15		≤5			LLL	Howerton	DMA	70
				REQ COM: Needed for evaluation. Measurements with less accuracy not helpful,											69
				STATUS: No active work,											72
				REQ COM: None											69
438	92U ²³⁵	$\sigma_{n,3n}$		II			Ths-16			10		LASL	Barr	DMA	67
				REQ COM: None											69
				STATUS: No active work,											72

REQ #	TARGET * Z A	REACTION TYPE QUANTITY VARIABLE	PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
				eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
439	92U ²³⁵	σ _{n,f}	II	1-	1		3				GE	Snyder	DRDT	69
				REQ COM: Used as standard at higher energies,										69
				STATUS: LLL Czirr ⁺ have measurements in progress rel to										72
				Li(n,α); NCSAC=k2,										72
				BCMN Theobald ⁺ in progress to 2keV; EANDC(E) 150/U										72
				BCMN Deruytter ⁺ in progress, rel to ¹⁰ B,										72
				EANDC(E) 150/U,										72
				SAC Blons, NSE to be published,										72
440	92U ²³⁵	σ _{n,f}	II	1.10 100	1.10 100	1.10	3				KAPL	Ehrlich	DNR	69
				REQ COM: Isolated values needed for normalization purposes,										69
				Choice of energy is influenced by experimental										69
				requirements, but values every decade useful,										69
				Where cross section has structure, energy average										69
				over carefully specified range is desired;										69
				STATUS: LLL Czirr ⁺ have linac measurements in progress,										72
				NCSAC=k2, covering this energy range,										72
				ANL Poenitz ⁺ have completed measurements, 30, 150,										72
				500 keV,										72

[illegible]

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
442	92U ²³⁵	$\sigma_{n,f}$		I		10-	15	1					LASL Hansen	DMA	66
				I		10-	14	1					NDC Caswell	DPR	69
					REQ COM: Excitation cross sections at many energies req. Absolute calibration at several different energies Energy resolution 3 per, energy calibration 1 per										69
					STATUS: LASL Barton ⁺ , meas. at 1.5-7 MeV; plan 6-15 MeV. LLL Czirr ⁺ , meas. rel. H > 50keV; rel ⁶ Li(n, $\bar{\alpha}$) < 1 ANL Poenitz ⁺ measurements in progress 30-150 keV. Absolute points at 500, 966 keV planned. ORNL de Saussure ⁺ meas. rel. ¹⁰ B(n, $\bar{\alpha}$) and ⁶ Li(n, $\bar{\alpha}$) up to 1.5 MeV. ORNL Peele ⁺ meas. rel H planned to 15 MeV. ORNL Gwin ⁺ , rel. ¹⁰ B, to 200 keV, USNDC-3. AFRE Gayther ⁺ measuring 1 keV-1 MeV, <5 percent. BCMN Deruytter ⁺ to 100 keV, rel. ¹⁰ B, EANDC(E) 150/U, CEA Szabo finds older data should be normalized upward by 2-4 percent, EANDC(E) 150/u,										72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
443	$^{92}\text{U}^{235}$	$\sigma_{n,f}$ Ratio	wrt H, B^{10}	I		1-	14	1					ANL Avery	DRDT	69
													LMFB Henning-AEC	DRDT	69
													ORNL Maiese	DRDT	69
					REQ COM: Required is ratio of $\text{U}^{235}(n,f)$ to $\text{B}^{10}(n,\alpha)$ and to $\text{H}^1(n,p)$ to 1 percent, Intermediate accuracy of 3 per would be useful, Needed to compare standards,										69
					STATUS: LASL Barton⁺, meas. at 1.5-7 MeV; plan 6-15 MeV. LLL Czirr⁺ meas, rel. H > 50 keV; rel $^6\text{Li}(n,\alpha) < 1$ ANL Poenitz⁺ measurements in progress 30-150 keV. Absolute points at 500, 966 keV planned. GPNL de Saussure⁺ meas, rel. $^{10}\text{B}(n,\alpha)$ and $^6\text{Li}(n,\alpha)$ up to 1.5 MeV, GRNL Peele⁺ meas, rel. H planned to 15 MeV, GRNL Gwin⁺, rel. ^{10}B, to 200 keV, USNDC=3, AERE Gayther⁺ measuring 1 keV-1 MeV, <5 percent. BCMN Deruytter⁺ to 100 keV, rel. ^{10}B, EANDC(E) 150/U, CEA Szabo finds older data should be normalized upward by 2-4 percent, EANDC(E) 150/u,										72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
447	$^{235}_{92}\text{U}$	Nu Bar		I	Th =	to	3	1				ANL	Avery	DRDT	69
												GE	Snyder	DNDT	69
												LMFB	Hennig-AEC	DNDT	69
												REQ COM: Needed as a cross check with other isotopes,			69
												Accuracy of 1,5 to 2 per would be useful,			69
448	$^{235}_{92}\text{U}$	Fis n Y	$P(E_{n'})$	II	Th	to	3	1	5			ANL	Avery	DRDT	69
												BET	Bayard	DNR	72
												KAPL	Ehrlich	DNR	69
												LMFB	Hennig-AEC	DRDT	69
												REQ COM: Verification of fission spectrum needed,			69
												$\Delta E_{n'} = 5\text{per}$ for $E_{n'} < 0,3\text{MeV}$ and from 10-20MeV, KAPL,			69
												STATUS: ANL Smith ⁺ have measurements in progress < 1,6 MeV			72
												AERE Rose ⁺ find evidence for nonlinearity > 6 MeV,			72
												at $E_n = 130\text{ keV}$,			72
												LASL Auchampaugh ⁺ have verified spectrum			72
												linearity to 12 MeV at $E_n = 1,85\text{ MeV}$, USNDC-3,			72
												CEA Abramson ⁺ have data to be analyzed at			72
												$E_n = 8-50\text{ keV}$, EANDC(E) 150/U,			72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≥15	>15	LAB	PERSON	ORG	
452	$_{92}\text{U}^{235}$	Cap Spect	$P(E_{\gamma})$	II	Th=15					10		BET	Bayard	DNR	67
				II	Th						20	KAPL	Ehrlich	DNR	67
				REQ COM: E_n thermal, gamma resol, $dn(E)/n(E) = 20$ per, KAPL											67
				E_n 0.001 to 15 eV, $dn(E)/n(E) = 10$ per at											67
				50 keV intervals for E_{γ} above 100 keV, BET											67
				Does spectrum change for thermal and resonances,											67
453	$_{92}\text{U}^{235}$	Delayed $\bar{\nu}_e \gamma$	$P(E_{\gamma}, T^{1/2})$	I		2.14				35	BNL	Kouts	DNMS	69	
				REQ COM: Accuracy refers to rel. intensities of delayed											70
				gammas from fission, $E_{\gamma} > 2\text{MeV}$ and $10 \text{ usec} < t < 1 \text{ hr}$											70
				Absolute gamma yields to factor of 2 also useful,											70
				STATUS: BNL Chrien+ have some data for ^{235}U and ^{239}Pu ,											70
				Large+, Phys., Chem., Fission give some data on U,											69

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR										
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG											
454	92U ²³⁵	Res Par		I	Th-200						10		ANL	Avery	DRDT	69									
													BET	Bayard	DNR	69									
													GE	Snyder	DRDT	69									
													LMFB	Hennig-AEC	DRDT	69									
													REQ COM: Needed for extrapolation to unresolved resonance region,												69
													Multilevel fit wanted where feasible,												69
													Need 10 per accuracy below 100 eV,												69
													Needed to as high an energy as possible,												69
													STATUS: ORNL de Saussure has res. par. to 100 eV, ORNL-180												69
													LASL Keyworth ⁺ measuring J, K in progress, USNDC-3												72
455	92U ²³⁵	Fis Prod Y	of Xe ¹³⁵	II	Th			3					BET	Bayard	DNR	67									
													REQ COM: For calculation of fission product poisons												67
													Cumulative and direct (inclusive of 15M isomer)												67
													yields wanted,												67
													STATUS: GE Meek and Rider, compilation summarizes status,												72
													NEDC = 12154,												72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR	
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG		
456	92U ²³⁵	Fis Prod Y	of Cs ¹³⁷	II	Th				1				BET	Bayard	DNR	67
					REQ COM: For burn up indicator standards,											67
					STATUS: GE Meek and Rider, compilation summarizes status, NEDG=1215k,											72
																72
457	92U ²³⁵	Fis Prod Y	of Sm ¹⁴⁹	II	Th				.3				BET	Bayard	DNR	67
					REQ COM: For calculation of fission product poisons											67
					STATUS: GE Meek and Rider, compilation summarizes status, NEDG=1215k,											72
																72
458	92U ²³⁵	Fis Prod Y	of Nd ¹⁴⁷	II	Th				3				BET	Bayard	DNR	67
					REQ COM: For calculation of fission product poisons											67
					STATUS: GE Meek and Rider, compilation summarizes status, NEDG=1215k,											72
																72
459	92U ²³⁶	Nu Bar	Prompt	I		500-	1k		3				LLL	Howerton	LMA	62

					REQ COM: None,											69
					STATUS: Conde and Holmberg, 0.8-6.7 MeV; <2 percent,											72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
460	$^{92}\text{U}^{236}$	Fis Spect	$P(E_n)$	II			*			10			LASL Walton	DNMS	70
					REQ COM: Background corr. in ^{235}U spent fuel assays.										70
					* Needed at one energy above fission threshold.										70
					STATUS: BCMN Coppola ⁺ have data at 1.5, 1.9, 2.3 MeV to be analyzed, EANDC(E) 150/u.										72
															72
461	$^{92}\text{U}^{236}$	Delayed n γ		I			3.14			10			LASL Walton	DNMS	70
					REQ COM: Background corr. in ^{235}U spent fuel assay.										70
					STATUS: No active work.										72
462	$^{92}\text{U}^{236}$	$\sigma_{n,\bar{f}}$		I	Th=	1				10			GE Snyder	DRDT	69
					REQ COM: Needed for control of U^{232} production GE										69
					Needed for isotope build up in thermal										69
					and fast reactors and for Np^{237} production.										69
					Required 10 percent accuracy in capture widths.										69
					STATUS: GRT Carlson ⁺ reports radiation widths to 10 per.										72
					NP A141, 577.										72
					BCMN Rohr ⁺ , in progress to 3 keV.										72
463	* $^{92}\text{U}^{237}$	$\sigma_{n,f}$		II	100=		16			10			LASL Barr	DMA	67

					REQ COM: *Short-lived radioactive target, 6,7d										69
					STATUS: LASL McNally, LA 4420, data for 44 eV=1.8 MeV.										72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
464	* 92U ²³⁷	Destruct	of Target	I		1-	15			10		LLL	Howerton	DMA	70
					REQ COM: Needed for evaluation, * Radioactive target-6,7 day,										69
					STATUS: LASL McNally have fission data to 1,8 MeV, LA 4420										72
					LASL Barr ⁺ , have critical assembly core and re-										72
					flector integral fission measurements,										72
465	92U ²³⁸	Elastic	$\sigma(\bullet_n)$	I		1-	10		5-	10		ANL	Avery	DRDT	69
												GE	Snyder	DRDT	69
												LMFB	Hennig-A&C	DRDT	69
												ORNL	Perry	DRDT	69
					REQ COM: Accuracy 10 per in energy region 1-300keV, Accuracy 5 per in energy region 300keV to 2MeV, Accuracy 10 per in energy region 2-10MeV, Factors of 2 lower accuracy would be useful on short term,										69
					STATUS: ANL Smith ⁺ , data to 1,7 MeV; extending to 5 MeV. ECMN Ahmed has data to 2,3 MeV,										72
															72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR		
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG			
466	92U ²³⁸	Inelastic	σ(E _{n'})	I		100-	10		5				ANL	Avery	DRDT	69	
													GE	Snyder	DRDT	69	
													LMFB	Hemmig-AEC	DRDT	69	
					REQ COM: Energy resolution should be 5 percent Emission cross sections instead of inelastic and n,2n might be useful Accuracy of 20 per would be useful.												69
					STATUS: ANL Smith ⁺ , data to 1.7 MeV; extending to 5 MeV. BCMNH Ahmed has data to 2.3 MeV.												72
467	92U ²³⁸	Emission	σ(E _{n'})	I			5-15				20	LLL	Howerton	DMA	70		
					REQ COM: Energy range of interest: 0.2MeV ≤ E _{n'} ≤ E _n .												70
					STATUS: No active work.												72
					468	92U ²³⁸	σ _{n,2n}	II			Ths=10			10		GE	Snyder
REQ COM: Needed for control of U-232 in Pu=238 production.												72					
STATUS: No active work.												72					
469	92U ²³⁸	σ _{n,3n}	II							Ths=15				20	LLL	Howerton	DMA
				REQ COM: Needed for evaluation.												69	
				STATUS: No active work.												72	

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
470	92U ²³⁸	Fis Ratio	wrt U ²³⁵	I		500-	15	1-	5				LASL Hansen	DMA	67
					REQ COM: Accuracy 5 per below 1,3 MeV, 1 per above, Energy resolution 3 per, energy calibration 1 per, Intermediate accuracy would be useful,										67 69 69
					STATUS: ANL Meadows ⁺ have data to 5,3 MeV, to be pub- lished, See USNDC-1, ANL Poenitz ⁺ have points at 2, 2.5, 3 MeV, with quoted accuracy ~2 per, USNDC-1, LLL Behrens ⁺ measurements in progress, NCSAC-42,										72 72 72 72 72
471	92U ²³⁸	Fis Ratio	wrt Pu ²³⁹	I		500-	14	2-	4				LMFB Hennig-AEC DRDT		69
					REQ COM: Accuracy 4 per below 1,3 MeV, 2 per 1,3-5 MeV, 3 per > 5 MeV, Energy resolution 3 per, energy calibration 1 per, Intermediate accuracy would be useful,										69 69 69 69
					STATUS: ANL work planned,										72
472	92U ²³⁸	Nu Bar		I			1-10	1					ANL Avery LMFB Hennig-AEC DRDT		69 69
					REQ COM: Confirmation of Soleilhac data requested, need ratio to Cf Nu Bar,										72 72
					STATUS: LLL Howe ⁺ have measurements in progress,										72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
473	92U238	Delayd n Y		II			5=1k		5				LASL Walton	DNMS	70
					REQ COM: Calculation of moderating assemblies for U assay, Data needed for extrapolation to 15MeV,										70
					STATUS: ANL Cox, work in progress, LASL Evans ⁺ have recorrected older work, see USNDC-3, NSE to be published,										72
474	92U238	Delayd n Y	P(E _n)	I	Th	to	5		5				LMFB Hennig-AEC DRDT		72
					REQ COM: Available data discrepant										72
					STATUS: ANL Cox planning work,										72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YP	
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG		
475	92U ²³⁸	σ _{n,γ}		I	500	to	10	2	to	10		AI	Alter	DRDT	69	
												ANL	Avery	DRDT	69	
												GE	Snyder	DRDT	69	
												LMFB	Hennig-AEC	DRDT	69	
					REQ COM: Highest priority need for fast reactor calc,											69
					Accuracy 6 per from 500 eV to 1 keV,											72
					Accuracy 4 per from 1-300 keV,											72
					Accuracy 6 per from 300-500 keV,											72
					Accuracy 10 per from 500 keV to 10 MeV,											69
					Accuracy of 10 per from 1 keV to 10 MeV would be											72
					useful,											72
					STATUS: LLL Czirr ⁺ , USNDC-1,											72
					RPI Block ⁺ , USNDC-1, to 80 keV in progress,											72
					ANL Poenitz, measuring in 400-1500 keV range,											72
476	92U ²³⁸	σ _{n,γ}		I	Th-	to	15			10		LLL	Howerton	DMA	69	
					REQ COM: Needed for evaluation, Disagreements and											69
					gaps in existing data need to be resolved,											69
					STATUS: LLL Czirr ⁺ , USNDC-1,											72
					RPI Block ⁺ , USNDC-1, to 80 keV in progress,											72
					ANL Poenitz, measuring in 400-1500 keV range,											72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
477	$^{92}\text{U}^{238}$	Tot $\bar{\nu}$ Prod	$\sigma(\sigma_{\bar{\nu}}, E_{\bar{\nu}})$	II	.001	to	10	*		10				LMFB Hemmig-AEC DRDT	72
					REQ COM: Accuracy 10 per in spectrum Gamma ray spectrum desired at intervals of 0.5 MeV in gamma energy. Gammas of all energies wanted, For shielding and $\bar{\nu}$ heating calculations.										67
					STATUS: ANL Bollinger, average spectrum results, LASL journey, thermal capture spectrum, NCSAC-42.										72
478	$^{92}\text{U}^{238}$	$\sigma_{n,\bar{\nu}}$ wrt or	$\sigma_{n,f} \text{ Pu}^{239}$ $\sigma_{n,f} \text{ U}^{235}$	I		10-	10	1.5	7					ANL Avery DRDT	69
														GE Snyder DRDT	72
														LMFB Hemmig-AEC DRDT	69
														ORNL Perry DRDT	69
					REQ COM: Needed is ratio of capture cross section of U^{238} to fission cross section of Pu^{239} or U^{235} , Direct ratio needed to supplement separate meas, Accuracy 1.5 per below 300 keV, 7 per above, Intermediate accuracy would be useful on near term Ratio data discrepant with absolute measurements.										69
					STATUS: ORNL de Saussure ⁺ have measurements rel. to ^{235}U and to ^6Li in progress to 100 keV, plan to extend to 800 keV.										72

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REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≥15	>15	LAB	PERSON	ORG	
479	$^{92}\text{U}^{238}$	Delayd $\bar{\gamma}$ Y	$P(E_{\bar{\gamma}}, T^{1/2})$	II			2,14				35	BNL	Kouts	DNMS	69
					REQ COM: Accuracy refers to rel. intensities of delayed gammas from fission, $E_{\bar{\gamma}} > 2\text{MeV}$ and $10\text{ usec} < t < 1\text{hr}$, Absolute gamma yields to a factor of 2 also useful STATUS: No active work,										70 70 70 72
480	$^{92}\text{U}^{238}$	Res Par		I		*					10	AI	Alter	DRDT	69
												ANL	Avery	DRDT	69
												GE	Snyder	DRDT	69
												LMFB	Hemmig-AEC	DRDT	69
					REQ COM: *Needed for Doppler effect on fast reactors, to as high energy as can be measured, Need answers to questions of missing p-wave levels and uncertainty of gamma-widths, Existing data $> 1\text{ keV}$ are discrepant, STATUS: COL Rahn ⁺ , NCSAC-42 and USNDC-1, Trans. and Self indication measurements,										69 69 69 69 72 72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR		
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG			
481	$^{93}\text{Np}^{237}$	$\sigma_{n,2n}$	Act.	II			Ths=15			10		SRL	Dessauer	DPMM	67		
				II			Ths=10			10		GE	Snyder	DRDT	69		
				I			Ths=15		≤5			LLL	Howerton	DMA	70		
				REQ COM: To evaluate contamination of Pu^{238} by Pu^{236} Also needed for control of U-232 production Measurements with lower accuracy not helpful, LLL													67
															69		
STATUS: No active work,															72		
482	$^{93}\text{Np}^{237}$	$\sigma_{n,f}$		II		1=	5			10		SRL	Dessauer	DPMM	67		
				REQ COM: Subthreshold to several MeV, for Pu^{238} production,													67
				STATUS: NBS Bowman ⁺ plan measurements rel. to $^{235}\text{U}(n,f)$ to 2 MeV,													72
483	$^{93}\text{Np}^{237}$	Fis Ratio	wrt U^{235}	III	20=	50				10		LASL	Hansen	DMA	66		
				I		50=	1		5		LASL	Hansen	DMA	66			
				II			1=15	1			LASL	Hansen	DMA	66			
				REQ COM: < 50 keV; $E_n(\text{res}) = 30 \text{ per}$; $E_n(\text{calib}) = 10 \text{ per}$, > 50 keV; $E_n(\text{res}) = 3 \text{ per}$; $E_n(\text{calib}) = 1 \text{ per}$,													69
															69		
STATUS: NBS Bowman ⁺ plan measurements 10 keV=2 MeV,															72		

REQ #	TARGET * Z A	REACTION TYPE QUANTITY VARIABLE	PRI OR,	INCIDENT ENERGY eV keV MeV			PERCENT ACCURACY 1-3 4-9 ≤15 >15				REQUESTER LAB PERSON ORG			YR	
484	93 ND 237	σ _{n,ḡ}	I	.001-	1		3	to	10		BNW	Leonard	DPMM	67	
			I	.001-	1					GE	Snyder	DRDT	67		
			II		1-	5				SRL	Dessauer	DPMM	67		
			REQ COM: Accuracy 3 per interval Th=10 eV Accuracy 5 per in $\bar{g}_n$, Accuracy 10 per in $\bar{g}_g$, from thermal to 1keV, For thermal reactor calc, and Pu-238 prod,												
485	* 93 ND 238	σ _{n,ḡ}	II	Th-	1				10		BNW	Leonard	DPMM	67	

			REQ COM: Needed to evaluate Pu ²³⁸ production, *Radioactive sample - 2,1 days												
			STATUS: No active work,												
486	94 ^{Pu} 238	σ _{n,2n}	I			Ths=15			15		LLL	Howerton	DMA	69	
REQ COM: Needed for evaluation,															
STATUS: No active work,															

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
492	94Pu238	σ _{n,γ}		I		1-300					50	LLL	Howerton	DMA	69
					REQ COM: Needed for evaluation,										69
					STATUS: LASL Silbert ⁺ to be published, to 200keV, USNDC-3,										72
493	94Pu238	σ _{n,p}		II		to	15				50	LLL	Howerton	DMA	69
					REQ COM: Needed for evaluation,										69
					STATUS: No active work,										72
494	94Pu238	Destruct	of Target	I		1-	1		5			LASL	Motz	DMA	66
				I		1-	15			10		LLL	Howerton	DMA	70
					REQ COM: None,										66
					STATUS: LASL Silbert ⁺ capture and fission data to be published, See USNDC-3,										72
															72
495	94Pu239	Elastic	σ(θ _n)	II			1-3			10		ANL	Avery	DRDT	69
				II			1-3			10		LMFB	Hennig-AEC	DRDT	69
				II			1-7			10		LASL	Diven	DMA	67
					REQ COM: Energy resolution 500 keV or better,										69
					STATUS: ANL Smith ⁺ data to 3.0 MeV, extending to 4.0 MeV.										72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
500	^{239}Pu	$\sigma_{n,f}$		I	Th-	1			1			GE	Snyder	DRDT	72
REQ COM: Standard parameter for Pu-fueled reactor															67
Direct measurements disagree															67
Improved precision needed for thermal reactors															67
U and Pu half lives should be confirmed as they															72
affect this measurement,															72
STATUS: LLL Behrens ⁺ measurements in progress, NGSAC-k2.															72
RPI Block ⁺ , plan meas. rel. to ^{235}U , Th at 24 keV,															72
BCM N Theobald ⁺ in progress to 2keV, EANDC(E) 150/u															72
SAC Blons, NSE, to be published,															72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR	
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG		
501	94Pu239	σn,f		I	1	to	10	2=	5				ANL	Avery	DRDT	69
			I	1	to	10	2=	5				GE	Snyder	DRDT	69	
			I	1	to	10	2=	5				LMFB	Hemmig-AEC	DRDT	69	
			I		50=	8	1					NDC	Caswell	DPR	69	
REQ COM: Highest priority for fast reactor calculations, 69																
Accuracy 3 per below 20 keV, 2 per 20 keV to 3 MeV 69																
Accuracy 5 per in energy range 3-6 MeV 69																
Verification of current accuracy or intermediate 69																
improvement would be useful, 69																
Need related accuracy for 5-10 percent energy bins 72																
STATUS: LLL Behrens+ measurements in progress, NCSAC-42. 72																
ORNL Gwin+ to 1,5 in progress, See NCSAC-42. 72																
ANL Poenitz, 0,5-5,0 MeV rel. to 235U, in progress 72																
NBS Bowman+ plan measurements 0,1-2,0 MeV. 72																
RPI Block+ measurements in progress, 1-200 keV. 72																
AERE Gayther+ measurements in progress agree to 5 72																
per with Sowerby+ evaluation, AEREM 2497. 72																
SAC Blons. to 30 keV, NSE, to be published, 72																

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
502	94Pu ²³⁹	Fis Ratio	wrt U ²³⁵	I		10-	1k	2					LMFB Hennig-AEC	DRDT	72
				I		10-	15	1					LASL Hansen	DMA	66
REQ COM: Energy resolution 3 per., energy calibration 1 per															69
Need 2 per for avg over 5-10 per energy intervals,															72
STATUS: NBS Bowman ⁺ plan measurements 0.1-2 MeV, 2-5 per.															72
ANL Poenitz ⁺ in progress 0.15-3 MeV, 1 percent,															72
LLL Behrens ⁺ in progress, expect 2 per, NCSAC-42,															72
ORNL Gwin ⁺ in progress to 1.5 MeV, expect 2 per.															72
See NCSAC-42,															72
RPI Block ⁺ in progress to 200 keV, expect 1 per.															72
CEA Szabo ⁺ have completed new measurements 17 keV															72
to 1 MeV, EANDC(E) 150/U,															72

REQ #	TARGET * 2 A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
503	^{239}Pu	Nu Bar		I	Th	to	10	≤1*				AI	Alter	DRDT	66
												ANL	Avery	DRDT	66
												GE	Snyder	DRDT	66
												LMFB	Hemmig-AEC	DRDT	66
												ORNL	Perry	DRDT	66
												REQ COM: *Requested accuracy 1/2 percent 1 keV to 3 MeV;			69
												otherwise 1 percent, Accuracy of 1.5 percent			69
												would be useful,			69
												Highest priority for fast reactor calculations,			69
												Require resolution of significant structure up			72
												to 500 keV,			72
												STATUS: RPI Reed ⁺ plan measurements, Thr=200 eV,			72
												ORNL Weston ⁺ in progress, Thr=200 eV, plan to			72
												extend to 1.5 MeV,			72
												LLL Howe ⁺ in progress rel, to $\bar{\nu}^{252}\text{Cf}$, NCSAC-42.			72
												SAC Trochon and Ryabor find no evidence for spin			72
												correlation,			72
												AAEC Boldeman and Walsh, data < 2 MeV, to be pub,			72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
504	94Pu^{239}	Delayed n	$P(E_n)$	II	Th	to	5		5				ANL Avery	DMDT	69
													LMFB Hemmig-AEC	DRDT	69
					REQ COM: Needed for analysis of fast criticals and fast reactor calculations, Yield, half life, and energy needed, DRDT										69
					STATUS: No active work,										72
505	94Pu^{239}	Delayed n		II			3-14			10			LASL Walton	DNMS	70
					REQ COM: Calculation of moderating assemblies for Pu assay, Data needed for extrapolation to 15MeV,										70
					STATUS: LASL Evans ⁺ report recorrected older work, NSE, to be published, USNDC-3, ANL Cox, work in progress,										72
															72
															72
506	94Pu^{239}	Eta		I	Th-1			1					GE Snyder	DRDT	67
					REQ COM: For Pu-fueled reactor calculations										67
					Desire accuracy to 0,5 per, Th-1 eV										67
					Standard parameter, want value at 0,025 eV,										67
					STATUS: No active work; however, see alpha and nubar,										72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
507	94Pu^{239}	Alpha		I	100	to	10	4	to	10		ANL	Avery	DRDT	69
												GE	Snyder	DRDT	69
												LMFB	Hennig-AEC	DRDT	69
												ORNL	Maienschein	DRDT	69
					REQ COM: Accuracy 8 per in range 100 eV to 1 keV,										72
					Accuracy 4 per in range 1 keV to 50 keV,										72
					Accuracy 6 per in range 50 to 600 keV,										72
					Accuracy 10 per in range 600 keV-10 MeV,										69
					Energy resol, needed below 20 keV to be determined										69
					Capture cross section would be equally useful,										69
					STATUS: RPI Block ⁺ , plan measurements, 1-200 keV,										72
508	94Pu^{239}	Delayed $\bar{\gamma}$ Y	$P(E_{\bar{\gamma}}, T^{1/2})$	I			2.14				35	BNL	Kouts	DNMS	69
					REQ COM: Accuracy refers to rel. intensities of delayed										70
					gammas from fission, $E_{\bar{\gamma}} > 2\text{MeV}$ and $10\text{ usec} < t < 1\text{hr}$,										70
					Absolute gamma yields to factor of 2 also useful,										70
					STATUS: BNL Chrien ⁺ have some data for ^{235}U and ^{239}Pu ,										70
					Large ⁺ , Phys, Chem, Fission give some data on U,										69

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
509	$^{239}_{94}\text{Pu}$	Fis $\bar{g}$ Y	P($E_{\bar{g}}$)	II	Th						15		LASL Walton	DNMS	70
					REQ COM: For non-destructive assays of ^{239}Pu , Ge(Li) resolution required-2,5 keV at 1,2 MeV, Need spectra 0,25-5 MeV, and yield (photons/fission=MeV-sec) 1ms-12hr, to 15 percent, Associate gammas with fission products if possible										70
					STATUS: Kimhof ⁺ , 4 min-24 hrs, NCSAC-42, p. 142.										70
510	$^{239}_{94}\text{Pu}$	Cap Spect	P($E_{\bar{g}}$)	III	Th-100						20		LASL Walton	DNMS	70
					REQ COM: Development of new Pu assay technique, Ge(Li) resolution (2,5keV, at 1,2MeV) required, Gamma yield per capture required to 20 percent, Need spectra above 1,2MeV gamma energy,										70
					STATUS: No active work,										70

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURAOY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≥15	>15	LAB	PERSON	ORG	
514	94Pu239	Fis Prod Y	of Nd147	II	Th				3				BET Bayard	DNR	67
					REQ COM: For calculation of Fission product poisons,										67
					STATUS: GE Meek and Rider compilation summarizes status, NEDG=12154,										72 72
515	94Pu239	Fis Prod Y	of Sm149	II	Th				3				BET Bayard	DNR	67
					REQ COM: For calculation of Fission product poisons										67
					STATUS: GE Meek and Rider compilation summarizes status, NEDG=12154,										72 72
516	94Pu240	Inelastic		II	*****										
							1,5-10					20	GE Snyder	DRDT	72
													LMFB Hennig-AEC	DRDT	69
					REQ COM: Emission σ's might be equally useful at the higher energies,										69 69
					STATUS: ANL Smith ⁺ , data to 1,5 MeV, work planned to higher energies,										72 72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1=3	4=9	≤15	>15	LAB	PERSON	ORG	
517	94Pu^{240}	$\sigma_{n,f}$		II		500=	10		5				GE Snyder	DRDT	72
				II	500=	100			9				LMFB Hemmig-AEC	DRDT	72
					REQ COM: Important for fast reactor calculations,										69
					STATUS: LLL Behrens ⁺ measurements in progress, NCSAC-k2.										72
					ORNL Weston ⁺ measurements in progress to 250 keV.										72
					AERE Belcher ⁺ measurements in progress rel. to ^{235}U to 1 MeV.										72
															72
518	94Pu^{240}	Fis Ratio	wrt U^{235}	III		1=100			5				ACRP Hannum	DRDT	72
				II		1=	15		2				LASL Hansen	DMA	67
				II		100=	5		3				LMFB Hemmig-AEC	DRDT	72
					REQ COM: < 100 keV; $E_n(\text{res}) = 6$ per; $E_n(\text{calib}) = 2$ per,										67
					> 100 keV; $E_n(\text{res}) = 3$ per; $E_n(\text{calib}) = 2$ per,										67
					Accuracy 5 percent useful.										72
					STATUS: LLL Behrens ⁺ measurements in progress, NCSAC-k2.										72
					AERE Belcher ⁺ measurements in progress to 1 MeV.										72
519	94Pu^{240}	Nu Bar		II		Ths=	10		3				ANL Avery	DRDT	72
													LMFB Hemmig-AEC	DRDT	69
					REQ COM: Accuracy of 5 percent would be useful,										72
					STATUS: SCU Savin ⁺ 70 HELS 2, 157, 3=5 per in energy										72
					region 1=4 MeV, Solielhac ⁺ planning 1=14 MeV.										72

REQ #	TARGET		REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
	* Z	A	QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≥15	>15	LAB	PERSON	ORG	
520	94	Pu ²⁴⁰	Delayd n Y		II		750-	14				20	LASL	Walton	DNMS	70
						REQ COM: Calculation of moderating assemblies for Pu assay Data needed for extrapolation to 15MeV,										70
						STATUS: ANL Cox will try if sample is available,										72
521	94	Pu ²⁴⁰	$\sigma_{n,\bar{e}}$		I	Th=100				3			GE	Snyder	DRDT	67
						REQ COM: Improved precision needed for thermal reactors,										67
						STATUS: Discrepancy between RPI and older measurements has been resolved, see Hockenbury ⁺ NSE 49, 153.										72
																72
522	94	Pu ²⁴⁰	$\sigma_{n,\bar{e}}$		I	500-	150			5			ANL	Avery	DRDT	69
					I		150-	1			10		GE	Snyder	DRDT	72
					I								LMFB	Hennig-AEC	DRDT	69
						REQ COM: Accuracy of 15 per would be useful, High priority for fast reactor calculations										69
						STATUS: Discrepancy between RPI and older measurements has been resolved, see Hockenbury ⁺ NSE 49, 153.										72
						ORNL Weston ⁺ measurements in progress to 250 keV.										72
																72
523	94	Pu ²⁴⁰	Alpha		II		150-	7			10		LLL	Howerton	DMA	62
						REQ COM: None,										62
						STATUS: ORNL Weston ⁺ measurements in progress to 250 keV.										72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
524	94Pu^{240}	Res Par		II	100=	5					10		ANL Avery	DNMT	69
													LMFB Hemmig-AEC	DNMT	69
					REQ COM: Needed for fast reactor calc., incl. Doppler eff. Existing data discrepant.										69 72
					STATUS: RPI Hockenbury ⁺ , NSE(1972); capture, fission and total measurements to 30 keV. Deduced res, par. for 35 resonances below 500 eV.										72 72
525	94Pu^{240}	Delayed $\bar{\gamma}$ Y	$P(E_{\bar{\gamma}}, T^{1/2})$	II			2.14				35		BNL Kouts	DNMS	69
					REQ COM: Accuracy refers to rel. intensities of delayed gammas from fission, $E_{\bar{\gamma}} > 2\text{MeV}$ and $10\text{ usec} < t < 1\text{hr}$. Absolute gamma yield to factor of 2 also useful.										70 70 70
					STATUS: HAR Thomas resonance ($n, \bar{\gamma}$) data from $\text{Pu}=240$ in eV region, shows delayed component, UKNDC, p. 37.										72 72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR		
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≥15	>15	LAB	PERSON	ORG			
526	^{241}Pu	$\sigma_{n,f}$	Fis Ratio wrt U^{235}	I	Th-	30		3	to	10		ANL	Avery	DRDT	69		
												GE-	Snyder	DRDT	69		
				I		1-	10		5			LMFB	Hennig-AEC	DRDT	72		
				REQ COM: Accuracy to 3 per from thermal to 10 eV, 10 per from 10eV to 30keV, Ratio to U^{235} or Pu^{239} would be useful													
					STATUS: ORNL Weston ⁺ , in progress, rel. to $^{10}\text{B}(n,\alpha)$, to 200 keV, LLL Behrens ⁺ in progress, rel. to ^{235}U , UCSAC-42, CEA Szabo ⁺ have completed measurements 17 keV to 1 MeV, RANDC(E) 150/U, SAC Blons report data taken at liq. N temp., to 30 keV, NSE, to be published												
527	^{241}Pu	Fis Ratio	wrt U^{235}	II		10-	15	1				LASL	Hansen	DMA	66		
				REQ COM: Energy resolution 3 per, energy calibration 1 per,													
					STATUS: LLL Behrens ⁺ in progress, NCSAC-42.												
528	^{241}Pu	Nu Bar		II		1-10		6				ANL	Avery	DRDT	72		
					1,	1		4			LMFB	Hennig-AEC	DRDT	69			
				REQ COM: None,													
					STATUS: LLL Howe ⁺ plan measurements > 10 keV. See NCSAC-42 Conde ⁺ ; 5 values from 0.52-15 MeV, JNE 22, p. 53.												

[illegible]

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR	
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG		
532	94Pu241	Res Par		II	Th-	.4			5	to	20	ANL	Avery	DRDT	72	
					REQ COM: Accuracy 5 per from thermal to 100 eV, Accuracy 10 per from 100 eV to 400 eV, 20 per would be useful for thermal and fast reactor calculations,										67 67 67 67	
					STATUS: SAC Blons ⁺ , least squares multilevel analysis in progress, EANDC(E) 150/U,										72 72	
533	94Pu241	Delayed n Y		III	Th	to	14			10		LASL Walton	DNMS	70		
					REQ COM: Calculation of moderating assemblies for Pu assay Data needed for extrapolation to 15MeV,										70 70	
					STATUS: ANL Cox may attempt if sample is available,										72	
534	94Pu242	σ _{n,2n}		I	***** Ths-15										LLL Howerton DMA	69
					REQ COM: Needed for evaluation,										69	
					STATUS: No active work,										72	
535	94Pu242	Nu Bar		II		500-	10		5			LMFB Hennig-AEC	DRDT	69		
					REQ COM: None										69	
					STATUS: No active work,										72	

REQ #	TARGET		REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
	* Z	A	QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
536	94	Pu ²⁴²	Nu Bar	Prompt	II		500-	1k	3				LLL	Howerton	DMA	62
						REQ COM: None,										69
						STATUS: No active work,										72
537	94	Pu ²⁴²	Delayed n Y		III			3.1k				20	LASL Walton		DNMS	70
						REQ COM: Calculation of moderating assemblies for Pu assay										70
						STATUS: LASL Evans ⁺ report recorrected older data, to be published NSR, see USNDC-3,										72
																72
538	94	Pu ²⁴²	σ _{n,γ}		I	Th	to	7	3-			20	BNW Leonard		DPMM	67
					II	Th	to	7	3-			20	GZ Hutchins		DRDT	72
					I		1-	7				<20	LMFB Hemmig-AEC		DRDT	72
						REQ COM: Accuracy: 3 per to 100 eV; 10 per, 100 eV to 1 keV										67
						Accuracy: 15-20 per from 1 keV to 7 MeV,										72
						Accuracy: Res. params. to 10-20 per below 10 keV,										67
						For fast breeder calc., Cm, Cf production,										67
						STATUS: RPI Hockenbury ⁺ , capture measurements up to 30 keV are in progress,										72
																72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
539	94Pu^{242}	$\sigma_{n,\alpha}$	Act	I		1-300					50	LLL	Howerton	DMA	69
					REQ COM: Needed for evaluation,										69
					STATUS: Czirr, foil available, exp. planned,										72
					KFK Beer ⁺ , plan measurements,										72
					RPI Hockenbury ⁺ , capture measurements up to 30 keV are in progress,										72
540	94Pu^{242}	$\sigma_{n,p}$		II			14				20	LASL	Bell	DMA	67
					REQ COM: For interpretation of heavy element production,										67
					STATUS: No active work,										72
541	95Am^{241}	Total		II	Th				2-3			BNW	Leonard	DFMM	69
					REQ COM: Accuracy 2-3 per in thermal energy range										69
					STATUS: No active work,										72
542	95Am^{241}	$\sigma_{n,2n}$		I			Ths-15			15		LLL	Howerton	DMA	69
					REQ COM: Needed for evaluation,										69
					STATUS: No active work,										72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR	
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG		
543	95Am ²⁴¹	σ _{n,γ}		I	Th-	1					10		SRL	Dessauer	DPMM	67
												BNW	Leonard	DPMM	67	
												LLL	Howerton	DMA	70	
				II	Th	to	10			15		GE	Hutchins	DRDT	72	
					REQ COM: Production of both Am ²⁴² and Am ^{242m} wanted,										67	
					PNW needs values at 0.0253 eV, priority 2,										67	
					Needed for Pu ²³⁸ program, and production of Cm ²⁴⁴ ,										67	
					For spent fuel shielding,										72	
					STATUS: ORNL Weston ⁺ in progress, to 250 keV,										72	
544	95Am ²⁴¹	σ _{n,γ}		I		.1-300					50		LLL	Howerton	DMA	69
					REQ COM: Required is cross section for production of both										69	
					Am ²⁴² and Am ^{242m} ,										69	
					STATUS: ORNL Weston ⁺ in progress, to 250 keV,										72	
545	95Am ²⁴²	Total		II	Th-	10					10		SRL	Dessauer	DPMM	67

					REQ COM: Resonance energies needed to determine Cm ²⁴⁴ prod,										67	
					STATUS: No active work,										72	

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
546	$^{95}\text{Am}^{242}$	$\sigma_{n,f}$		II	Th-	10				10-	20	SRL	Dessauer	DPMM	69
					REQ COM: Cross section needed for 150 year isomer, Require accuracy 10 per in thermal value and RI, Needed to determine Cm^{244} production.										69
					STATUS: LLL Browne ⁺ plan measurement, see NC3A0-42.										72
547	$^{95}\text{Am}^{242}$	$\sigma_{n,f}$		II	Th	to	10			15		GE	Hutchins	DRDT	72
				I	Th	to	5			≤10		LLL	Howerton	DMA	69
				II	Th-	10				10-	20	SRL	Dessauer	DPMM	69
					REQ COM: Needed for evaluation, LLL, Cross section wanted for 152 year isomer, Need resonance integral and thermal value to 10 percent, to evaluate Cm^{244} production. SRL.										69
					STATUS: No active work,										72
548	$^{95}\text{Am}^{243}$	Total		I	Th-	10			2			BNW	Leonard	DPMM	67
					REQ COM: Res. int. wanted for Cm^{244} production, Needed for long term reactivity calculations.										67
					STATUS: AND Simpson ⁺ , meas, trans, from 0.5 to 1000 eV, ANOR-1060.										72
															72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≥15	>15	LAB	PERSON	ORG	
552	$^{96}\text{Cm}^{243}$	Total		II	Th-	10				10		SRL	Dessauer	DPMM	67
					REQ COM: Resonance energies wanted to evaluate Cm^{244} prod, Accuracy 10 per in res, integral										67
					STATUS: No active work,										72
553	$^{96}\text{Cm}^{243}$	$\sigma_{n,f}$		II	Th-	10				10		SRL	Dessauer	DPMM	67
				I		10-100				10		LASL	Cowan	DMA	69
					REQ COM: Needed to evaluate Cm^{244} production, Accuracy 10 per in resonance integral										67
					STATUS: LASL Diven, data to be analyzed from Physics 8, LLL Browne ⁺ plan measurements, see NCSAC-42.										72
554	$^{96}\text{Cm}^{243}$	$\sigma_{n,\bar{e}}$		II	Th-	10			5-	10		SRL	Dessauer	DPMM	69
					REQ COM: Require alpha to 10 percent, Accuracy 5-10 per in thermal value and R,I,										69
					STATUS: No active work,										72
555	$^{96}\text{Cm}^{244}$	$\sigma_{n,2n}$		I	*****										69
							Ths=15			15		LLL	Howerton	DMA	69
					REQ COM: Needed for evaluation,										69
					STATUS: No active work,										72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YP
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
556	$^{96}\text{Cm}^{244}$	$\sigma_{n,f}$		I		10-100				10			LASL Cowan	DMA	69
					REQ COM: Needed to evaluate Cf production.										69
					STATUS: No active work in this energy region.										72
557	$^{96}\text{Cm}^{244}$	$\sigma_{n,\bar{g}}$		II		10-	10			10			GE Snyder	DRDT	67
				II		10=	10			10			AI Alter	DRDT	67
					REQ COM: For spent fuel shielding,										72
					Accuracy 5-10 per in resonance integral,										67
					Needed to evaluate Cf production,										69
					STATUS: No active work,										72
558	$^{96}\text{Cm}^{244}$	$\sigma_{n,\bar{g}}$		I		1-300				50			LLL Howerton	DMA	69
					REQ COM: Needed for evaluation,										69
					STATUS: No active work,										72
559	$^{96}\text{Cm}^{245}$	Total		I	Th-	10				10			SRL Dessauer	DPMM	67
					REQ COM: Need 10 per in res, int., to evaluate Cf prod,										67
					STATUS: No active work,										72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
560	$^{96}\text{Cm}^{245}$	$\sigma_{n,f}$		I	Th=	10				10		SRL	Dessauer	DPMM	67
				I		10-100				10		LASL	Cowan	DMA	69
					REQ COM: Need 10 per in σ and res, int., to eval, Cf prod, Need integral alpha to 10 per, thermal and res,										67 69
					STATUS: LLL Browne ⁺ plan measurements, NCSAC-42,										72
561	$^{96}\text{Cm}^{245}$	$\sigma_{n,\bar{f}}$		I	Th=	10				10		SRL	Dessauer	DPMM	69
					REQ COM: Need 10 per in res, int., to evaluate Cf prod, Need integral alpha to 10 per, thermal and res,										69 69
					STATUS: No active work,										72
562	$^{96}\text{Cm}^{246}$	Total		I	Th=	10				10		SRL	Dessauer	DPMM	67

					REQ COM: Resonance structure desired, to evaluate Cf prod, Accuracy 10 per in resonance integral										67 67
					STATUS: No active work,										72
563	$^{96}\text{Cm}^{246}$	$\sigma_{n,f}$		I		10-100				10		LASL	Cowan	DMA	69
					REQ COM: To evaluate Cf ²⁵² production by R-process,										69
					STATUS: No active work in this energy region,										72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≥15	>15	LAB	PERSON	ORG	
564	$^{96}\text{Cm}^{246}$	$\sigma_{n,\bar{g}}$		I	Th-	10				10		SRL	Dessauer	DPMM	69
					REQ COM: Need accuracy 10 per in resonance integral, Resonance structure desired, to evaluate Cf prod,										69
					STATUS: No active work,										72
565	$^{96}\text{Cm}^{247}$	Total		I	Th-	10					20	SRL	Dessauer	DPMM	67
					REQ COM: Need 20 per in res, int, to evaluate Cf prod,										67
					STATUS: No active work,										72
566	$^{96}\text{Cm}^{247}$	$\sigma_{n,f}$		I	Th-	10			5-	10		SRL	Dessauer	DPMM	67
				I		10-100				10		LASL	Cowan	DMA	69
					REQ COM: Need 5-10 per in thermal value and RI, SRL, Need 10 per in σ to evaluate Cf prod, by R-process, LASL,										67
					STATUS: LLL Browne ⁺ plan measurements, NCSAG-42,										72
567	$^{96}\text{Cm}^{247}$	$\sigma_{n,\bar{g}}$		I	Th-	10			5-	10		SRL	Dessauer	DPMM	69
					REQ COM: Need 5-10 per in res, int, and thermal value, to evaluate Cf production,										69
					STATUS: No active work,										72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
568	$^{96}\text{Cm}^{248}$	Total		I	Th=	10					20	SRL	Dessauer	DPMM	67
					REQ COM: Need 50 per accuracy at thermal										67
					Need 20 per in res, int, to evaluate Cf prod,										67
					STATUS: SRL Benjamin ⁺ plan measurements at GRELA.										72
569	$^{96}\text{Cm}^{248}$	$\sigma_{n,f}$		I		10-100				10		LASL	Cowan	DMA	69
					REQ COM: To evaluate Cf production,										69
					STATUS: No active work in this energy region,										72
570	$^{96}\text{Cm}^{248}$	$\sigma_{n,\bar{g}}$		I	Th=	10				10		SRL	Dessauer	DPMM	69
					REQ COM: Need 10 per at thermal and in resonance integral										69
					to evaluate Cf production,										69
					STATUS: SRL Benjamin ⁺ will try to infer from total cross										72
					section measured on GRELA,										72
571	$^{97}\text{Bk}^{249}$	Total		I	Th=	10					20	SRL	Dessauer	DPMM	67
					REQ COM: Res, param, desired to evaluate Cf production,										67
					Need 20 per in resonance integral,										67
					STATUS: No active work,										72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
572	$^{97}\text{Bk}^{249}$	$\sigma_{n,\bar{e}}$		I	Th-	10				10		SRL	Dessauer	DPMM	69
					REQ COM: For Cf production, 10 per thermal and RI.										69
					STATUS: No active work.										72
573	$^{98}\text{Cf}^{249}$	$\sigma_{n,f}$		I		10-100				10		LASL	Cowan	DMA	69
					REQ COM: None.										69
					STATUS: LASL Silbert has data to be published, USNDC-3, LLL Browne ⁺ plan measurements, NCSAC-42.										72

574	$^{98}\text{Cf}^{250}$	Total		I	Th-	10				20		SRL	Dessauer	DPMM	67
					REQ COM: Resonances desired to evaluate Cf production. Need 20 per in res, int, to evaluate Cf ²⁵² prod.										67
					STATUS: No active work.										72
575	$^{98}\text{Cf}^{250}$	$\sigma_{n,f}$		I	Th-	10				10		SRL	Dessauer	DPMM	67
				I		10-100				10		LASL	Cowan	DMA	69
					REQ COM: To evaluate Cf production, Accuracy 10 per in res, integral, SRL.										67
					STATUS: No active work.										72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
576	$^{250}_{98}\text{Cf}$	$\sigma_{n,\bar{g}}$		I	Th-	10				10		SRL	Dessauer	DPMM	69
					REQ COM: Need 10 per in res, int, to eval, Cf^{252} prod,										69
					STATUS: No active work,										72
577	$^{251}_{98}\text{Cf}$	$\sigma_{n,\bar{g}}$		I	Th-	10				10		SRL	Dessauer	DPMM	67
					REQ COM: To evaluate Cf production,										67
					Accuracy 10 per in resonance integral,										67
					STATUS: No active work,										72
578	$^{252}_{98}\text{Cf}$	$\sigma_{n,f}$		I		10-100				10		LASL	Cowan	DMA	69
					REQ COM: None,										69
					STATUS: No active work,										72
579	$^{252}_{98}\text{Cf}$	Nu Bar		I					.25			NDC	Caswell	DPR	69
												BET	Bayard	DNR	72
					REQ COM: Required is nubar for spontaneous fission of Cf^{252}										69
					as primary standard,										69
					STATUS: NPL Axton has work in progress,										70

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
580	$^{98}\text{Cf}^{252}$	Nu Bar		I				<1				AI	Alter	DRDT	72
					REQ COM: Spontaneous fission source; required as standard.										72
					STATUS: No active work.										72
581	$^{98}\text{Cf}^{252}$	Fis Spect	$P(E_{n'})$	I				1				BET	Bayard	DNR	72
				I				5*				NDC	Caswell	DPR	72
					REQ COM: Spontaneous fission source.										72
					One percent in mean energy of spectrum req. DNR.										72
					5 percent in shape; 5 percent in energy. DPR.										72
					Needed for reference standard.										72
					STATUS: No active work.										72
582	$^{98}\text{Cf}^{252}$	$\sigma_{n,\bar{k}}$		I	Th-	10			10			SRL	Dessauer	DPMM	67
					REQ COM: To evaluate Cf production										67
					Accuracy 10 per in resonance integral.										67
					STATUS: No active work.										72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
583	* 98Cf ²⁵³	σ _{n,ḡ}		II	Th-	10					20	SRL	Dessauer	DPMH	67
					REQ COM: To evaluate Cf production										67
					Accuracy 20 per in res, integral										67
					*Target half-life 18d,										67
					Want to confirm that thermal cross sect, < 3b,										67
					STATUS: ORNL Bemis, NSE 41, 146 gives sigma eff, = 17.6 b										72
					for pile neutrons,										72
584	* 99Es ²⁵³	σ _{n,f}		I		10-100					10		LASL Cowan	DMA	69
					REQ COM: *Target half-life 20d,										69
					STATUS: LASL Silbert, USNDC-3, no active work,										72

585	* 99Es ²⁵⁴	Alpha		II	Th-	20					20		LASL Bell	DMA	67
					REQ COM: needed to plan for production of Fm ²⁵⁷										67
					*Target half-life 480d,										67
					STATUS: No active work,										72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR	
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG		
586	* ₁₀₀ Fm ²⁵⁵	$\sigma_{n,f}$		I		10-100					10			LASL Cowan	DMA	69
					REQ COM: Measurement in presence of Es ²⁵⁵ parent,											69
					*Target half-life 40d,											69
					STATUS: No active work,											72
587	* ₁₀₀ Fm ²⁵⁷	$\sigma_{n,f}$		I		10-100					10			LASL Cowan	DMA	69

					REQ COM: *Target half-life 94d,											69
					STATUS: No active work in this energy region,											72

TABLE 2. PHOTONS INCIDENT

<u>Reaction</u>	<u>Variables Allowed</u>	<u>Definition</u>
$\sigma_{g,f}^-$		Photofission cross section
$\bar{g},n$	Total n Y	Total yield of neutrons per incident photon
$\bar{g},n$	Delayd n Y	Delayed neutron yield per incident photon
$\bar{g},f$	Del $\bar{g}$ spec	Spectrum of delayed fission gammas per incident photon
Photoneut	Yield	Photoneutron yield

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REQ #	TARGET # Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≥15	>15	LAB	PERSON	ORG	
590	^4_2Be	$\bar{\gamma}, n$	Total n Y	II			Ths-10				20	IRT	Bramblett	DNMS	72
					REQ COM: Background effect on non-destr, photonuc, assay. Electron energy resol, 1 percent, Total neut, yield produced by bremsstrahlung required, Converter (prefer Ta) thick enough to stop elects, Neutron yield absolute or relative to D($\bar{\gamma}, n$).										70 70 70 70 70
					STATUS: No useful data,										72
591	$^{13}_6\text{C}$	$\bar{\gamma}, n$	Total n Y	II			Ths-10				20	IRT	Bramblett	DNMS	72
					REQ COM: Background effect on non-destr, photonuc, assay. Electron energy resol, 1 percent, Total neut, yield produced by bremsstrahlung required, Converter (prefer Ta) thick enough to stop elects, Neutron yield absolute or relative to D($\bar{\gamma}, n$).										70 70 70 70 70
					STATUS: No useful data,										72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
592	80^{17}	$\bar{\gamma}, n$	Total n Y	II			Ths-10				20	IRT	Bramblett	DNMS	72
					REQ COM: Background effect on non-destr, photonuc, assay. Electron energy resol, 1 percent, Total neut, yield produced by bremsstrahlung required, Converter (prefer Ta) thick enough to stop elects. Neutron yield absolute or relative to D($\bar{\gamma}, n$). STATUS: No useful data.										70 70 70 70 70 72
593	90Th^{232}	$\bar{\gamma}, n$	Total n Y	II			Ths-10			10		IRT	Bramblett	DNMS	72
					REQ COM: For non-destructive photonuc, assay of Th mixtures k* neutron yield (incl, fission) produced by bremsstrahlung required, Converter (prefer Ta) thick enough to stop electrons, Absolute neutron yield or relative to D($\bar{\gamma}, n$). Electron energy resolution 1 percent, STATUS: Relative data of Gozani+, Trans, ANS13, 707(1970). Katz+, Can, J, Phys, 35, 470(1957).										70 70 70 70 70 70 70

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
594	$^{232}_{90}\text{Th}$	$\bar{\nu}, n$	Delayed n Y	I			Ths=10			10		IRT	Bramblett	DNMS	72
					REQ COM: For non-destructive photonuc. assay of Th mixtures Delayed neut. yield produced by bremsstrahlung required. Converter (prefer Ta) thick enough to stop electrons, Absolute neutron yield or relative to $D(\bar{\nu}, n)$. Electron energy resolution 1 percent,										70
					STATUS: Relative data of Gozani+, Trans,ANS13,707(1970), Katz+, Can,J.Phys,35,470(1957).										70
595	$^{232}_{90}\text{Th}$	$\bar{\nu}, f$	Del $\bar{\nu}$ Spec	III			10			10		IRT	Bramblett	DNMS	72
					REQ COM: For non-destructive photonuc. assay of Th mixtures Electron energy resolution 5 percent, Absolute fission product delayed gamma yield (1ms-1hr) produced by bremsstrahlung required, Converter (prefer Ta) thick enough to stop electrons, Emergent gamma energies 0.5-5 MeV, $\Delta E_{\bar{\nu}} = 3 \text{ keV}$,										70
					STATUS: Prelim. data of Rundquist, Trans,ANS13,746(1970),										70

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
600	$^{92}\text{U}^{234}$	$\bar{\gamma}, n$	Delayed n Y	III			Ths-10			30		IRT	Bramblett	DNMS	72
					REQ COM: For non-destructive photonuc. assay of ^{233}U , ^{235}U , Delayed neut. yield produced by bremsstrahlung required, Converter (prefer Ta) thick enough to stop electrons, Absolute neutron yield or relative to D($\bar{\gamma}, n$). Electron energy resolution 1 percent,										70
					STATUS: No data,										72
601	$^{92}\text{U}^{234}$	$\bar{\gamma}, f$	Del $\bar{\gamma}$ Spec	III			10			30		IRT	Bramblett	DNMS	72
					REQ COM: For non-destructive photonuc. assay of ^{233}U , ^{235}U , Electron energy resolution 5 percent, Absolute fission product delayed gamma yield (1ms-1hr) produced by bremsstrahlung required. Converter (prefer Ta) thick enough to stop electrons, Emergent gamma energies 0.5-5 MeV, $\Delta E_{\gamma} = 3$ keV.										70
					STATUS: No data,										72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	10-15	>15	LAB	PERSON	ORG	
604	$^{235}_{92}\text{U}$	$\bar{\gamma}, f$	Del $\bar{\gamma}$ Spec	II			10			10			IRT Bramblett	DNMS	72
					REQ COM: For non-destructive photonuc. assay of ^{235}U , Electron energy resolution 5 percent, Absolute fission product delayed gamma yield (1ms-1hr) produced by bremsstrahlung required, Converter (prefer Ta) thick enough to stop electrons, Emergent gamma energies 0.5-5 MeV, $\Delta E_{\gamma} = 3$ keV,										70
					STATUS: Prelim. data of Rundquist, TRANS,ANS13,746(1970).										70
605	$^{236}_{92}\text{U}$	$\bar{\gamma}, n$	Total n Y	II	***** Ths=10 30 IRT Bramblett DNMS										72
					REQ COM: For non-destructive photonuc. assay of ^{235}U , lx neutron yield (incl. fission) produced by bremsstrahlung required, Converter (prefer Ta) thick enough to stop electrons, Absolute neutron yield or relative to $D(\bar{\gamma}, n)$, Electron energy resolution 1 percent,										70
					STATUS: No data,										72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
606	$^{236}_{92}\text{U}$	$\bar{\gamma}, n$	Delayd n Y	II			Ths=10			30		IRT	Bramblett	DNMS	72
					REQ COM: For non-destructive photonuc. assay of ^{235}U , Delayed neut, yield produced by bremsstrahlung required. Converter (prefer Ta) thick enough to stop electrons, Absolute neutron yield or relative to D($\bar{\gamma}, n$). Electron energy resolution 1 percent,										70
					STATUS: None,										72
607	$^{236}_{92}\text{U}$	$\bar{\gamma}, f$	Del $\bar{\gamma}$ Spec	III			10			30		IRT	Bramblett	DNMS	72
					REQ COM: For non-destructive photonuc. assay of ^{235}U , Electron energy resolution 5 percent, Absolute fission product delayed gamma yield (1ms-1hr) produced by bremsstrahlung required, Converter (prefer Ta) thick enough to stop electrons, Emergent gamma energies 0.5-5 MeV, $\Delta E_{\bar{\gamma}} = 3 \text{ keV}$,										70
					STAT'S: No data,										72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
610	$_{92}\text{U}^{238}$	$\bar{\gamma}, f$	Del $\bar{\gamma}$ Spec	II			10			10			IRT Bramblett	DNMS	72
REQ COM: For non-destructive photonuc, assay of uranium, Electron energy resolution 5 percent, Absolute fission product delayed gamma yield (1ms-1hr) produced by bremsstrahlung required, Converter (prefer Ta) thick enough to stop electrons, Emergent gamma energies 0.5-5 MeV, $\Delta E_{\gamma} = 3$ keV, STATUS: Prelim, data of Rundquist, Trans,ANS13,746(1970).															70 70 70 70 70
611	$_{94}\text{Pu}^{239}$	$\bar{\gamma}, n$	Total n Y	II			Ths-10			10			IRT Bramblett	DNMS	72
REQ COM: For non-destructive photonuc, assay of ^{239}Pu, kg neutron yield (incl, fission) produced by bremsstrahlung required, Converter (prefer Ta) thick enough to stop electrons, Absolute neutron yield or relative to D($\bar{\gamma}, n$), Electron energy resolution 1 percent, STATUS: Relative data of Gozani+, Trans,ANS13,707(1970).															70 70 70 70 70

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR	
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≥15	>15	LAB	PERSON	ORG		
61k	$^{240}_{94}\text{Pu}$	$\bar{\gamma}, n$	Total n Y	II			Ths-10			10			IRT	Bramblett	DNMS	72
					REQ COM: For non-destructive photonuc, assay of ^{239}Pu , k $\times$ neutron yield (incl, fission) produced by bremsstrahlung required, Converter (prefer Ta) thick enough to stop electrons, Absolute neutron yield or relative to D($\bar{\gamma}, n$). Electron energy resolution 1 percent,											70
					STATUS: No data,											72
615	$^{240}_{94}\text{Pu}$	$\bar{\gamma}, n$	Delayed n Y	II			Ths-10			10			IRT	Bramblett	DNMS	72
					REQ COM: For non-destructive photonuc, assay of ^{239}Pu , Delayed neut, yield produced by bremsstrahlung required, Converter (prefer Ta) thick enough to stop electrons, Absolute neutron yield or relative to D($\bar{\gamma}, n$). Electron energy resolution 1 percent,											70
					STATUS: No data,											72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
616	94Pu^{240}	$\bar{\gamma}, f$	Del $\bar{\gamma}$ Spec	II			10			10		IRT	Bramblett	DNMS	72
					REQ COM: For non-destructive photonuc, assay of Pu^{239} , Electron energy resolution 5 percent, Absolute fission product delayed gamma yield (1ms-1hr) produced by bremsstrahlung required, Converter (prefer Ta) thick enough to stop electrons, Emergent gamma energies 0.5-5 MeV, $\Delta E_{\gamma} = 3 \text{ keV}$.										70
					STATUS: No data,										72
617	94Pu^{241}	$\bar{\gamma}, n$	Total n Y	III	***** Ths=10 30 IRT Bramblett DNMS										72
					REQ COM: For non-destructive photonuc, assay of Pu, 1μ neutron yield (incl, fission) produced by bremsstrahlung required, Converter (prefer Ta) thick enough to stop electrons, Absolute neutron yield or relative to $D(\bar{\gamma}, n)$. Electron energy resolution 1 percent,										70
					STATUS: None,										72

REQ #	TARGET * Z A	REACTION TYPE		PRI OK,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≥15	>15	LAB	PERSON	ORG	
618	${}_{94}^{241}\text{Pu}$	$\bar{\gamma}, n$	Delayed n Y	III			Ths-10			30		IRT	Bramblett	DNMS	72
					REQ COM: For non-destructive photonuc, assay of Pu, Delayed neut, yield produced by bremsstrahlung required, Converter (prefer Ta) thick enough to stop electrons, Absolute neutron yield or relative to D($\bar{\gamma}, n$). Electron energy resolution 1 percent,										70
					STATUS: None,										72
619	${}_{94}^{241}\text{Pu}$	$\bar{\gamma}, f$	Del $\bar{\gamma}$ Spec	III			10			30		IRT	Bramblett	DNMS	72
					REQ COM: For non-destructive photonuc, assay of Pu, Electron energy resolution 5 percent, Absolute fission product delayed gamma yield (1ms-1hr) produced by bremsstrahlung required, Converter (prefer Ta) thick enough to stop electrons, Emergent gamma energies 0.5-5 MeV, $\Delta E_{\gamma} = 3$ keV.										70
					STATUS: No data,										70

TABLE 3. MEDIUM ENERGY REQUESTS

<u>Reaction</u>	<u>Variables Allowed</u>	<u>Definition</u>
Tot p Reac		Total reaction cross section for incident protons
$\sigma_{p,x}$	$\sigma(E_x)$	Cross section for the emission of a charged-particle, x, where x is one of many charged particles allowed
σ_{p,Li^6}		Cross section for Li^6 production due to incident protons
$\sigma_{p,A=19}$		Cross section for the production of mass 19 particles
$\sigma_{p,kny}$	$\sigma(\theta_n, E_n)$	Angle and energy dependence of the neutrons produced by protons incident, k is the neutron multiplicity, and y is the remaining particle or particles
$\sigma_{p,kpy}$	$\sigma(\theta_p, E_p)$	Angle and energy dependence of the protons produced by protons incident, k is the proton multiplicity, and y is the remaining particle or particles
$\sigma_{a,kny}^-$	$\sigma(\theta_n, E_n)$	Angle and energy dependence of the neutrons produced by α 's incident, k is the neutron multiplicity, and y is the remaining particle or particles
$\sigma_{a,k\pi^\pm y}^-$	$\sigma(\theta_\pi, E_\pi)$	Angle and energy dependence of the pions produced by α 's incident, k is the pion multiplicity, and y is the remaining particle or particles
$\sigma_{a,x}^-$	$\sigma(E_x)$	Cross section for the emission of a charged particle, x, where x is one of many charged particles allowed

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REQ #	TARGET # Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		keV	MeV	Gev	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
620	${}^4_2\text{He}$	$\sigma_{p,x}$	$\sigma(E_x)$	II		25-100					10*		GSFC Reames	NASA	67
					REQ COM: x = each of the nuclides: D, T, and He^3 ,										67
					(*) : requested accuracy 10 percent or a few mb,										69
					STATUS: None,										72
621	${}^4_2\text{He}$	$\sigma_{p,x}$	$\sigma(E_x)$	II		300-	.6				10*		GSFC Reames	NASA	67
					REQ COM: x = each of the nuclides: D, T, and He^3 ,										67
					(*) : requested accuracy 10 percent or a few mb,										69
					STATUS: None,										72
622	${}^4_2\text{He}$	$\sigma_{\alpha,x}$	$\sigma(E_x)$	II		25-600					10*		GSFC Reames	NASA	67
					REQ COM: x = each of the nuclides: D, T, and He^3 ,										67
					(*) : requested accuracy 10 percent or a few mb,										69
					STATUS: None,										72
623	${}^6_3\text{Li}$	Tot p Reac		III		25-600					10*		GSFC Reames	NASA	67
					REQ COM: (*) : requested accuracy 10 percent or a few mb,										69
					STATUS: None,										72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		keV	MeV	GeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
624	${}^7_3\text{Li}$	Tot p Reac		III		25-600					10*		GSFC Reames	NASA	67
					REQ COM: (*): requested accuracy 10 percent or a few mb,										69
					STATUS: None,										72
625	${}^7_3\text{Li}$	$\sigma_{p,x}$		II		25-600					10*		GSFC Reames	NASA	67
					REQ COM: x = each of the nuclides Li^6 and Be^7 ,										67
					(*) : requested accuracy 10 percent or a few mb,										69
					STATUS: None,										72
626	${}^7_4\text{Be}$	σ_{p,Li^6}		II		25-600						est,*	GSFC Reames	NASA	67
					REQ COM: (*): need an estimate of the amount of Li^6 formed,										67
					STATUS: None,										72
627	${}^9_4\text{Be}$	Tot p Reac		III		25-600					10*		GSFC Reames	NASA	67

					REQ COM: (*): requested accuracy 10 percent or a few mb,										69
					STATUS: None,										72

[illegible]

REQ #	TARGET * Z A	REACTION TYPE QUANTITY VARIABLE	PRI OR,	INCIDENT ENERGY keV Mev Gev	PERCENT ACCURACY 1-3 4-9 ≤15 >15	REQUESTER LAB PERSON ORG	YR
631	${}^6_6\text{C}$	$\sigma_{p,kny}$	$\sigma(E_n, E_n')$	II	600- 2	25 HASL O'Brien DBER NASA Reetz NASA ORNL Alsmiller DPR	66 66 66
					REQ COM: One energy in interval, Measurements at a few angles, one near 0° , Measurements should include 1-MeV neutron.		66 66 66
					STATUS: None.		72
632	${}^6_6\text{C}^{12}$	n.x	II	***** 25- 1	10*	GSFC Reames NASA	67
					REQ COM: x = each of the nuclides: Li^6 , Li^7 , Be^7 , Be^9 , Be^{10} , Be^{11} , B^{10} , B^{11} , C^{10} , C^{11} . (*): requested accuracy 10 percent or a few mb.		67 67 69
					STATUS: None.		72
633	${}^6_6\text{C}^{12}$	$\sigma_{\alpha,x}$	I	25- 1.2	10*	GSFC Reames NASA	69
					REQ COM: x = each of the stable and particle-stable iso- topes with $3 \leq Z \leq 6$, (*): requested accuracy 10 percent or a few mb.		69 69 69
					STATUS: None.		72

REQ #	TARGET * Z A	REACTION TYPE QUANTITY VARIABLE	PRI OR.	INCIDENT ENERGY keV MeV GeV	PERCENT ACCURACY 1-3 4-9 ≤15 >15	REQUESTER LAB PERSON ORG	YR
634	${}^6\text{C}^{13}$	$\sigma_{p,x}$	I	25-600	10*	GSFC Reames NASA	67
				REQ COM: x = each of the nuclides Li^6 , Li^7 , Be^7 , Be^{10} , Be^{11} , B^{10} , B^{11} , B^{12} , C^{10} , C^{11} , C^{12} (*): requested accuracy 10 percent or a few mb. STATUS: None.			67 67 67 72
635	${}^7\text{N}^{14}$	$\sigma_{p,x}$	II	25-600	10*	GSFC Reames NASA	67
				REQ COM: x = each of the stable and particle-stable iso- topes with $3 \leq Z \leq 6$, For Li^6 and Be^7 isotopes, below 100 MeV, only. (*): requested accuracy 10 percent or a few mb. STATUS: None.			67 67 67 69 72
636	${}^7\text{N}^{15}$	$\sigma_{p,x}$	II	***** 25-600	10*	GSFC Reames NASA	67
				REQ COM: x = each of the stable and particle-stable iso- topes with $3 \leq Z \leq 7$. (*): requested accuracy 10 percent or a few mb. STATUS: None.			67 67 67 72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		keV	MeV	GeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
637	8_0	$\sigma_{p,kny}$	$\sigma(\theta_n, E_n)$	I		~50					25	HASL O'Brien	DBER	66	
												NASA Reetz	NASA	66	
												ORNL Alsmiller	DPR	66	
					REQ COM: Measurements at a few angles, one near 0° .									66	
					Measurements should include 1-MeV neutrons,									66	
					STATUS: None,									72	
638	8_0	$\sigma_{p,kny}$	$\sigma(\theta_n, E_n)$	II		600-	2				25	HASL O'Brien	DBER	66	
												NASA Reetz	NASA	66	
												ORNL Alsmiller	DPR	66	
					REQ COM: One energy in interval,									66	
					Measurements at a few angles, one near 0° ,									66	
					Include very low (~1 MeV) neutrons,									66	
					STATUS: None,									72	
639	8_0	$\sigma_{\pi^+,k\pi^+y}$	$\sigma(\theta_\pi, E_\pi)$	II			1-2				25	HASL O'Brien	DBER	66	
												NASA Reetz	NASA	66	
												ORNL Alsmiller	DPR	66	
					REQ COM: Cross section for π^+ at one energy in interval,									66	
					Measurements at a few angles, one near 0° ,									66	
					Low-energy (~50 MeV) pions should be included,									66	
					STATUS: None,									72	

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		keV	MeV	GeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
640	8^{16}	$\sigma_{p,x}$		I		25-600					10*		GSFC Reames	NASA	67
					REQ COM: x = each of the nuclides: Li^6 , Li^7 , Be^9 , Be^{10} , B^{10} , B^{11} , C^{10} , C^{11} .										67
					(*) : requested accuracy 10 percent or a few mb.										69
					STATUS: None.										72
641	8^{16}	$\sigma_{p,x}$		I		25-600					10*		GSFC Reames	NASA	67
					REQ COM: x = each of the nuclides: C^{12} , C^{13} , C^{14} , N^{13} , N^{14} , N^{15} , O^{15} .										67
					(*) : requested accuracy 10 percent or a few mb.										69
					STATUS: None.										72
642	8^{16}	$\sigma_{\alpha,x}$		I		25-	1,2				10*		GSFC Reames	NASA	69
					REQ COM: x = each of the stable and particle-stable isotopes with $3 \leq Z \leq 7$.										69
					(*) : requested accuracy 10 percent or a few mb.										69
					STATUS: None.										72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		keV	MeV	Gev	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
643	8O^{18}	$\sigma_{p,x}$		I		25-600					10*		GSFC Reames	NASA	67
					REQ COM: x = each of the nuclides: $\text{Li}^{6,7}$, Be^{7-10} , $\text{B}^{10,11}$, C^{10-14} , N^{13-16} , $\text{O}^{16,17}$, (*): requested accuracy 10 percent or a few mb, STATUS: None,										67 67 69 72
644	10Ne^{20}	$\sigma_{p,A=19}$		I		25-600					10		GSFC Reames	NASA	67
					REQ COM: Production of O^{19} , F^{19} , and Ne^{19} ; Upper limits useful, STATUS: None,										67 67 72
645	12Mg^{24}	$\sigma_{p,x}$		II		25-600					10*		GSFC Reames	NASA	67
					REQ COM: x = each of the stable and particle-stable iso- topes with $3 \leq Z \leq 11$, (*): requested accuracy 10 percent or a few mb, STATUS: None,										67 67 69 72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		keV	MeV	GeV	1-3	4-9	≥15	>15	LAB	PERSON	ORG	
646	^{13}Al	$\sigma_{p,kny}$	$\sigma(\theta_n, E_n)$	I		600-	2					25	HASL O'Brien NASA Reetz ORNL Alsmiller	DBER NASA DPR	66 66 66
REQ COM: Measurements at a few angles, one near 0° , Measurements should include 1-MeV neutrons, Data on an adjacent element would suffice,															66 66 66
STATUS: None,															72
647	^{13}Al	$\sigma_{p,kny}$	$\sigma(\theta_n, E_n)$	I			~10,30					25	HASL O'Brien NASA Reetz ORNL Alsmiller	DBER NASA DPR	66 66 66
REQ COM: Measurements at a few angles, one near 0° , Measurements should include 1-MeV neutrons, Data on an adjacent element would suffice,															66 66 66
STATUS: None,															72
648	^{13}Al	$\sigma_{p,kpy}$	$\sigma(\theta_p, E_p)$	II		~2000,	~10,30					25	HASL O'Brien NASA Reetz ORNL Alsmiller	DBER NASA DPR	66 66 66
REQ COM: Measurements at a few angles, one near 0° , Include low-energy (~50 MeV) protons, Data on an adjacent element would suffice,															66 66 66
STATUS: None,															72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		keV	MeV	GeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
649	¹³ Al	$\sigma_{\alpha, \text{kny}}$	$\sigma(\theta_n, E_n)$	II		100-	1					25	HASL O'Brien NASA Reetz ORNL Alsmiller	DBER NASA DPR	66 66 66
					REQ COM: Measurements at a few angles, one near 0°, include very low-energy (~1 MeV) neutrons,										66 66
					STATUS: None,										72
650	²⁰ Ca ⁴⁰	$\sigma_{p, x}$		III		25-600					10*		GSFC Reames NASA		67
					REQ COM: x = each of the stable and particle-stable isotopes with $3 \leq Z \leq 11$,										67
					(*) : requested accuracy 10 percent or a few mb,										67
					STATUS: None,										72
651	²⁶ Fe ⁵⁶	$\sigma_{p, x}$		II		25-600					10*		GSFC Reames NASA		67
					REQ COM: x = each of the stable and particle stable isotopes with $3 \leq Z \leq 11$,										67
					(*) : requested accuracy 10 percent or a few mb,										67
					STATUS: None,										72

REQ #	T/ *	ST A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
			QUANTITY	VARIABLE		keV	MeV	GeV	1-3	4-9	≥15	>15	LAB	PERSON	ORG	
655	2'		$\sigma_{p,kpy}$	$\sigma(\theta_p, E_p)$	II		~2000,	~10,30				25	HASL O'Brien NASA Reetz ORNL Alsmiller	DBER NASA DPR	66 66 66	
REQ COM: Measurements at a few angles, one near 0°, Include low-energy (~50 MeV) protons, Data on an adjacent element would suffice, STATUS: None.															66 66 66 72	
656	^{83}Bi		$\sigma_{p,kny}$	$\sigma(\theta_n, E_n)$	I		600-	2				25	HASL O'Brien NASA Reetz ORNL Alsmiller	DBER NASA DPR	66 66 66	
REQ COM: One energy (only) within energy range, Measurements at a few angles, one near 0°. Measurements should include 1-MeV neutrons, Data on an adjacent element would suffice, STATUS: None,															66 66 66 66 72	

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		keV	MeV	GeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
657	83^{Bi}	$\sigma_{p,kny}$	$\sigma(\theta_n, E_n)$	II			~10,30				25	HASL O'Brien	DBER	66	
												NASA Reetz	NASA	66	
												ORNL Alsmiller	DPR	66	
					REQ COM: Measurements at a few angles, one near 0°, Measurements should include 1-MeV neutron, Data on an adjacent element would suffice,									66	
					STATUS: None,									72	
658	83^{Bi}	$\sigma_{p,kpy}$	$\sigma(\theta_p, E_p)$	II		~2000,	~10,30				25	HASL O'Brien	DBER	66	
												NASA Reetz	NASA	66	
												ORNL Alsmiller	DPR	66	
					REQ COM: Measurements at a few angles, one near 0°, Include low-energy (~50 MeV) protons, Data on an adjacent element would suffice,									66	
					STATUS: None,									72	

TABLE 4
REQUESTS DELETED FROM NCSAS 35

NCSAC-35 Number	Target	Reaction	Variable	Priority	NCSAC-35 Number	Target	Reaction	Variable	Priority
	1H^1	Total		I	149	39Y^{87}	$\sigma_{n,2n}$	Act	I
3	1H^1	$\sigma_{n,\bar{g}}$		II	150	39Y^{87}	$\sigma_{n,p}$		II
6	2He^3	Total		I	151	39Y^{88}	$\sigma_{n,2m}$	Act	I
7	2He^3	Elastic	$\sigma(\theta_n)$	III	152	39Y^{88}	$\sigma_{n,p}$		II
10	3Li^6	Total		I	159	40Zr^{88}	$\sigma_{n,2n}$	Act	I
15	3Li^6	$\sigma_{n,\alpha}$ Ratio	wrt B^{10}	I	161	$*40\text{Zr}^{88}$	$\sigma_{n,p}$		II
17	3Li^7	Total		I	162	40Zr^{89}	$n,2n$	Act	I
47	8O^{17}	$(n,p)\text{N}^{17}$	$\beta \rightarrow \text{O}^{17*} \rightarrow n$	I	169	40Zr^{90}	$n,\bar{g}$		I
69	16S^{36}	$\sigma_{n,2n}$	Act	I	173	40Zr^{91}	Total		I
74	20Ca^{40}	$\sigma_{n,\alpha}$	Act	III	176	40Zr^{91}	$\sigma_{n,\bar{g}}$		I
76	20Ca^{46}	$\sigma_{n,2n}$	Act	I	179	40Zr^{91}	Res. Par.		I
104	26Fe	Tot $\bar{g}$ Prod	$\sigma(\theta_{\bar{g}}, E_{\bar{g}})$	I	182	40Zr^{92}	Total		I
148	$*37\text{Rb}^{84}$	$\sigma_{n,p}$		II	185	40Zr^{92}	$\sigma_{n,\bar{g}}$		I

TABLE 4 (cont.)

NCSAC-35 Number	Target	Reaction	Variable	Priority	NCSAC-35 Number	Target	Reaction	Variable	Priority
189	$_{40}\text{Zr}^{94}$	Total		I	242	$_{60}\text{Nd}^{146}$	$\sigma_{n,\bar{g}}$		II
192	$_{40}\text{Zr}^{94}$	$\sigma_{n,\bar{g}}$			249	$_{62}\text{Sm}^{147}$	$\sigma_{n,\bar{g}}$		II
193	$_{40}\text{Zr}^{94}$	Res Int	Capture	II	252	* $_{62}\text{Sm}^{151}$	Total		I
197	$_{40}\text{Zr}^{96}$	Total		I	257	* $_{63}\text{Eu}^{148}$	$\sigma_{n,2n}$	Act.	II
198	$_{40}\text{Zr}^{96}$	$\sigma_{n,\bar{g}}$		I	261	* $_{63}\text{Eu}^{150}$	$\sigma_{n,2n}$	Act	II
201	$_{40}\text{Zr}^{96}$	Res In	Capture	I	268	* $_{63}\text{Eu}^{154}$	Total		II
202	$_{40}\text{Zr}^{96}$	$\bar{G}_n$ and $\bar{G}_{\bar{g}}$		I	271	* $_{63}\text{Eu}^{155}$	Total		II
203	$_{41}\text{Nb}$	Elastic	$\sigma(\theta_n)$	II	278	$_{64}\text{Gd}^{154}$	$\bar{G}_n$ and $\bar{G}_{\bar{g}}$		
210	$_{41}\text{Nb}^{91}$	n,2n	Act	I	288	$_{64}\text{Gd}^{158}$	$\sigma_{n,\bar{g}}$		I
212	* $_{41}\text{Nb}^{91}$	$\sigma_{n,p}$		II	289	$_{64}\text{Gd}^{158}$	Res Int	Capture	I
213	* $_{41}\text{Nb}^{92}$	$\sigma_{n,2n}$	Act	I	290	$_{64}\text{Gd}^{158}$	$\bar{G}_n$ and $\bar{G}_{\bar{g}}$		I
215	* $_{41}\text{Nb}^{92}$	$\sigma_{n,p}$		II	291	$_{64}\text{Gd}^{160}$	Res Int	Capture	I
217	* $_{41}\text{Nb}^{94}$	$\sigma_{n,\bar{g}}$		I	292	$_{64}\text{Gd}^{160}$	$\bar{G}_n$ and $\bar{G}_{\bar{g}}$		I
219	* $_{41}\text{Nb}^{95}$	Res Int	Capture	I	295	$_{68}\text{Er}^{166}$	$\sigma_{n,\bar{g}}$		I II

Table 4 (cont.)

NCSAC-35 Number	Target	Reaction	Variable	Priority	NCSAC-35 Number	Target	Reaction	Variable	Priority
296	$^{167}_{68}\text{Er}$	$\sigma_{n,\bar{g}}$		I	426	$^{238}_{92}\text{U}$	Delayd f Y		II
297	$*^{167}_{69}\text{Tm}$	$\sigma_{n,2n}$	Act	II	437	$^{238}_{94}\text{U}$	Nu Bar		II
299	$*^{168}_{69}\text{Tm}$	$\sigma_{n,2n}$	Act	II	440	$^{238}_{94}\text{U}$	$\sigma_{n,\bar{g}}$		II
305	$*^{173}_{71}\text{Lu}$	$\sigma_{n,2n}$	Act	II	462	$^{239}_{94}\text{U}$	Delayd f Y		II
307	$*^{174}_{71}\text{Lu}$	$\sigma_{n,2n}$	Act	II	467	$^{240}_{94}\text{Pu}$	Delayd n Y $P(E_n,)$		II II II
342	$^{206}_{82}\text{Pb}$	$\sigma_{n,\alpha}$	Act	I	473	$^{240}_{94}\text{Pu}$	Delayd f Y		III
351	^{90}Th	Delayd n Y $P(E_n,)$		II II	482	$^{241}_{94}\text{Pu}$	Delayd $\bar{g}$ Y $P(E_{\bar{g}}, T^{\frac{1}{2}})$		II
366	$^{233}_{92}\text{U}$	Delayd n Y $P(E_n,)$		II II	483	$^{241}_{94}\text{Pu}$	Delayd f Y		III
374	$^{233}_{92}\text{U}$	Delayd f Y		III	485	$^{242}_{94}\text{Pu}$	$\sigma_{n,f}$		I
375	$^{234}_{92}\text{U}$	Total		II	491	$^{242}_{94}\text{Pu}$	Delayd $\bar{g}$ Y $P(E_{\bar{g}}, T^{\frac{1}{2}})$		II
379	$^{234}_{92}\text{U}$	Nu Bar		II	492	$^{242}_{94}\text{Pu}$	$\sigma_{n,p}$		II
405	$^{235}_{92}\text{U}$	Delayd f Y		II	493	$^{242}_{94}\text{Pu}$	Delayd f Y		III
406	$^{236}_{92}\text{U}$	Total		I	508	$^{244}_{96}\text{Cm}$	Total		II
408	$^{236}_{92}\text{U}$	Res Int		II	511	$^{244}_{96}\text{Cm}$	Nu Bar		II

SECTION V.

TABLE 5.A

DBER

Division of Biomedical and Environmental Research, James L. Liverman, Director

Phone: 301-973-3208

USAEC, Washington, D. C. 20545

Contact: Keran O'Brien (HASL)

Phone: 212-620-3632

Health and Safety Laboratory
Radiation Physics Division
USAEC
376 Hudson Street
New York, New York 10014

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		keV	MeV	GeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
630	⁶ C	$\sigma_{p,kny}$	$\sigma(\theta_n, E_n)$	I		~50					25	HASL	O'Brien	DBER	67
631	⁶ C	$\sigma_{p,kny}$	$\sigma(\theta_n, E_n)$	II		600-	2				25	HASL	O'Brien	DBER	66
637	⁸ O	$\sigma_{p,kny}$	$\sigma(\theta_n, E_n)$	I		~50					25	HASL	O'Brien	DBER	66
638	⁸ O	$\sigma_{p,kny}$	$\sigma(\theta_n, E_n)$	II		600-	2				25	HASL	O'Brien	DBER	66
639	⁸ O	$\sigma_{\alpha,k\pi+y}$	$\sigma(\theta_{\pi}, E_{\pi})$	II			1=2				25	HASL	O'Brien	DBER	66
646	¹³ Al	$\sigma_{p,kny}$	$\sigma(\theta_n, E_n)$	I		600-	2				25	HASL	O'Brien	DBER	66
647	¹³ Al	$\sigma_{p,kny}$	$\sigma(\theta_n, E_n)$	I			~10,30				25	HASL	O'Brien	DBER	66
648	¹³ Al	$\sigma_{p,kpy}$	$\sigma(\theta_p, E_p)$	II		~2000,	~10,30				25	HASL	O'Brien	DBER	66
649	¹³ Al	$\sigma_{\alpha,kny}$	$\sigma(\theta_n, E_n)$	II		100-	1				25	HASL	O'Brien	DBER	66
653	²⁷ Co	$\sigma_{p,kny}$	$\sigma(\theta_n, E_n)$	I		600-	2				25	HASL	O'Brien	DBER	66
654	²⁷ Co	$\sigma_{p,kny}$	$\sigma(\theta_n, E_n)$	I			~10,30				25	HASL	O'Brien	DBER	66
655	²⁷ Co	$\sigma_{p,kpy}$	$\sigma(\theta_p, E_p)$	II		~2000,	~10,30				25	HASL	O'Brien	DBER	66
656	⁸³ Bi	$\sigma_{p,kny}$	$\sigma(\theta_n, E_n)$	I		600-	2				25	HASL	O'Brien	DBER	66
657	⁸³ Bi	$\sigma_{p,kny}$	$\sigma(\theta_n, E_n)$	II			~10,30				25	HASL	O'Brien	DBER	66
658	⁸³ Bi	$\sigma_{p,kpy}$	$\sigma(\theta_p, E_p)$	II		~2000,	~10,30				25	HASL	O'Brien	DBER	66

SECTION V.

TABLE 5.B

DCTR

Division of Controlled Thermonuclear Research, Robert L. Hirsch, Director

Phone: 301-973-4558

USAEC, Washington, D. C. 20545

Contact: William C. Gough

Phone: 301-973-3155

REQ #	TARGET * Z A	REACTION TYPE QUANTITY VARIABLE	PRI OR _i	INCIDENT ENERGY eV keV MeV			PERCENT ACCURACY 1-3 4-9 ≤15 >15				REQUESTER LAB PERSON ORG			YR
3	${}^1_1\text{H}^2$	$\sigma_{p,n}^{\text{p}}$				3.3-15				<25	ORNL McNally	DCTR	72	
6	${}^1_1\text{H}^3$	$\sigma_{p,n}^{\text{p}}$		*****	*****	*****	***	***	***	*****	ORNL McNally	DCTR	72	
7	${}^1_1\text{H}^3$	$\sigma_{t,2n}^{\text{p}}$			10-	10				<25	ORNL McNally	DCTR	72	
9	${}^2_2\text{He}^3$	$\sigma_{t,d}^{\text{p}}$			100-	10				<25	ORNL McNally	DCTR	72	
10	${}^2_2\text{He}^4$	$\sigma_{d,n}^{\text{p}}$		*****	*****	*****	***	***	***	*****	ORNL McNally	DCTR	72	
13	${}^3_3\text{Li}^6$	Elastic				~14			15		AEC Gough	DCTR	71	
16	${}^3_3\text{Li}^6$	$\sigma_{n,n}^{\text{p}}$				Ths=14			10		AEC Gough	DCTR	71	
17	${}^3_3\text{Li}^6$	$\sigma_{n,t}^{\text{p}}$				3-14			<10		AEC Gough	DCTR	71	
20	${}^3_3\text{Li}^6$	$(n,p')\text{Li}^6$		$d + \bar{a}$		3-15				<25	ORNL McNally	DCTR	72	
21	${}^3_3\text{Li}^6$	$\sigma_{p,\bar{a}}^{\text{p}}$			100-	15				<25	ORNL McNally	DCTR	72	
22	${}^3_3\text{Li}^6$	$\sigma_{d,n}^{\text{p}}$			100-	5				<25	ORNL McNally	DCTR	72	
23	${}^3_3\text{Li}^6$	$\sigma_{d,n}^{\text{p}}$		$\text{He}^3 + \bar{a}$	100-	5				<25	ORNL McNally	DCTR	72	
24	${}^3_3\text{Li}^6$	$\sigma_{d,p}^{\text{p}}$			100-	5				<25	ORNL McNally	DCTR	72	
25	${}^3_3\text{Li}^6$	$\sigma_{d,p}^{\text{p}}$		$t + \bar{a}$	100-	5				<25	ORNL McNally	DCTR	72	
26	${}^3_3\text{Li}^6$	$(d,d')\text{Li}^6$		$d + \bar{a}$		3-6				<25	ORNL McNally	DCTR	72	
27	${}^3_3\text{Li}^6$	$\sigma_{d,\bar{a}}^{\text{p}}$			100-	5				<25	ORNL McNally	DCTR	72	
28	${}^3_3\text{Li}^6$	$(t,n)\text{Be}^8$		$2\bar{a}$ decay	10-	2				<25	ORNL McNally	DCTR	72	
29	${}^3_3\text{Li}^6$	$(t,p)\text{Li}^8$		$\bar{b}^- + 2\bar{a}$	10-	2				<25	ORNL McNally	DCTR	72	
30	${}^3_3\text{Li}^6$	$\sigma_{t,d}^{\text{p}}$			10-	2				<25	ORNL McNally	DCTR	72	
31	${}^3_3\text{Li}^6$	$({}^3\text{He},n)\text{B}^8$		$\bar{b}^+ + 2\bar{a}$		2-8				<25	ORNL McNally	DCTR	72	
32	${}^3_3\text{Li}^6$	$({}^3\text{He},p)$		$2\bar{a}$ decay	100-	8				<25	ORNL McNally	DCTR	72	
33	${}^3_3\text{Li}^6$	$({}^3\text{He},d)$			100-	8				<25	ORNL McNally	DCTR	72	
34	${}^3_3\text{Li}^6$	$\sigma_{\bar{a},p}^{\text{p}}$				3-12				<25	ORNL McNally	DCTR	72	

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
35	${}^6_3\text{Li}$	$(\bar{a}, \bar{a}')\text{Li}^{6*}$	$d + \bar{a}$				3-12				<25	ORNL	McNally	DCTR	72
36	${}^6_3\text{Li}$	${}^6\text{Li} + {}^6\text{Li} \rightarrow {}^7\text{Be} + {}^4\text{He} + n$				*	*				*	AEC	Gough	DCTR	71
					*****	*****	*****	***	***	***	*****				
37	${}^7_3\text{Li}$	Elastic	$\sigma(E_n)$				~1k			15		AEC	Gough	DCTR	71
38	${}^7_3\text{Li}$	Inelastic	$\sigma(E_{n'})$			Ths-	1k			15		AEC	Gough	DCTR	71
41	${}^7_3\text{Li}$	$\sigma_{n,n't}$					3-1k		<10			AEC	Gough	DCTR	71
42	${}^7_3\text{Li}$	$\sigma_{n,n't}$	$\sigma(E_{n'})$				~1k			15		AEC	Gough	DCTR	71
49	${}^9_4\text{Be}$	$\sigma_{p,\bar{a}}$				10-	15				<25	ORNL	McNally	DCTR	72
50	${}^9_4\text{Be}$	$(p,d)\text{Be}^A$	$2\bar{a}$ decay			10-	15				<25	ORNL	McNally	DCTR	72
61	${}^{12}_6\text{C}$	$\sigma_{n,n'} \text{ 1st}$					4.8-1k			10		AEC	Gough	DCTR	71
62	${}^{12}_6\text{C}$	$\sigma_{n,n'} 3\bar{a}$					1k			10		AEC	Gough	DCTR	71
76	${}^9_9\text{F}$	Inelastic					10-1k			10		AEC	Gough	DCTR	71
78	${}^9_9\text{F}$	$\sigma_{n,\bar{g}}$				1-	1			10		ORNL	Perry	DRDT	66
79	${}^9_9\text{F}$	Absorption			Th-	to	1k			10		AEC	Gough	DCTR	71
89	${}^{13}_{13}\text{Al}$	$\sigma_{n,2n}$					1k			10		AEC	Gough	DCTR	71
90	${}^{13}_{13}\text{Al}$	$\sigma_{n,2n}$	$\sigma(E_{n'}, E_{n'})$				1k			15		AEC	Gough	DCTR	71
91	${}^{13}_{13}\text{Al}$	Inelastic	$\sigma(E_{n'})$			Ths-	1k			15		AEC	Gough	DCTR	72
93	${}^{13}_{13}\text{Al}$	$\sigma_{n,\bar{g}}$					1k				20	AEC	Gough	DCTR	71
94	${}^{13}_{13}\text{Al}$	$\sigma_{n,p}$					1k				20	AEC	Gough	DCTR	71
95	${}^{13}_{13}\text{Al}$	$\sigma_{n,\bar{a}}$					1k				20	AEC	Gough	DCTR	71
96	${}^{13}_{13}\text{Al}$	$\sigma_{n,n'} (E'S)$				Ths-	1k			15		AEC	Gough	DCTR	72
97	${}^{13}_{13}\text{Al}$	Cap Spect	$P(E_{\bar{g}})$	I	Th					10		SNPO	Fleishman	DSNS	69
117	${}^{23}_{23}\text{V}$	$\sigma_{n,2n}$					1k			10		AEC	Gough	DCTR	71

REQ #	TARGET # Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
118	23 ^V	$\sigma_{n,2n}$	$\sigma(\theta_{n,2n}, E_{n,1})$				1k			15		AEC	Gough	DCTR	71
120	23 ^V	Inelastic	$\sigma(E_{n,1})$			Ths-	1k			15		AEC	Gough	DCTR	72
121	23 ^V	$\sigma_{n,\bar{e}}$					1k				20	AEC	Gough	DCTR	71
123	23 ^V	$\sigma_{n,p}$					1k				20	AEC	Gough	DCTR	71
124	23 ^V	$\sigma_{n,\bar{a}}$					1k				20	AEC	Gough	DCTR	71
126	23 ^V	$\sigma_{n,n'}(g's)$				Ths-	1k			15		AEC	Gough	DCTR	72
127	23 ^V	Cap Spect	$P(E_g)$		Th-	res.				15		AEC	Gough	DCTR	71
131	24 ^{Cr}	Inelastic	$\sigma(E_{n,1})$			Ths-	1k			15		AEC	Gough	DCTR	72
132	24 ^{Cr}	$\sigma_{n,2n}$					1k			10		AEC	Gough	DCTR	71
133	24 ^{Cr}	$\sigma_{n,2n}$	$\sigma(\theta_{n,2n}, E_{n,1})$				1k			15		AEC	Gough	DCTR	71
135	24 ^{Cr}	$\sigma_{n,\bar{e}}$					1k				20	AEC	Gough	DCTR	71
136	24 ^{Cr}	$\sigma_{n,p}$					1k				20	AEC	Gough	DCTR	71
137	24 ^{Cr}	$\sigma_{n,\bar{a}}$					1k				20	AEC	Gough	DCTR	71
138	24 ^{Cr}	$\sigma_{n,n'}(g's)$					1k				20	AEC	Gough	DCTR	71
139	24 ^{Cr}	Cap Spect	$P(E_g)$		Th-	res.				15		AEC	Gough	DCTR	71
150	26 ^{Fe}	Inelastic	$\sigma(E_{n,1})$			Ths-	1k			15		AEC	Gough	DCTR	72
151	26 ^{Fe}	$\sigma_{n,2n}$					1k			10		AEC	Gough	DCTR	71
152	26 ^{Fe}	$\sigma_{n,2n}$	$\sigma(\theta_{n,2n}, E_{n,1})$				1k			15		AEC	Gough	DCTR	71
156	26 ^{Fe}	$\sigma_{n,\bar{e}}$					1k				20	AEC	Gough	DCTR	71
157	26 ^{Fe}	$\sigma_{n,p}$					1k				20	AEC	Gough	DCTR	71
159	26 ^{Fe}	$\sigma_{n,\bar{a}}$					1k				20	AEC	Gough	DCTR	71
160	26 ^{Fe}	$\sigma_{n,n'}(g's)$				Ths-	1k			15		AEC	Gough	DCTR	72
161	26 ^{Fe}	Cap Spect	$P(E_g)$		Th-	res.				15		AEC	Gough	DCTR	71
184	28 ^{Ni}	Inelastic	$\sigma(E_{n,1})$			Ths-	1k			15		AEC	Gough	DCTR	72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
185	²⁸ Ni	$\sigma_{n,2n}$	$\sigma(\theta_{n1}, E_{n1})$				1k			10		AEC	Gough	DCTR	71
186	²⁸ Ni	$\sigma_{n,2n}$					1k			15		AEC	Gough	DCTR	71
188	²⁸ Ni	$\sigma_{n,\bar{e}}$					1k				20	AEC	Gough	DCTR	71
189	²⁸ Ni	$\sigma_{n,p}$					1k				20	AEC	Gough	DCTR	71
191	²⁸ Ni	$\sigma_{n,\bar{a}}$					1k				20	AEC	Gough	DCTR	71
192	²⁸ Ni	$\sigma_{n,n'}(g's)$	$P(E_{\bar{e}})$			Ths-	1k			15		AEC	Gough	DCTR	72
193	²⁸ Ni	Cap Spect			Th-	res.				15		AEC	Gough	DCTR	71
201	²⁹ Cu	Inelastic	$\sigma(E_{n1})$			Ths-	1k			15		AEC	Gough	DCTR	72
202	²⁹ Cu	$\sigma_{n,2n}$	$\sigma(\theta_{n1}, E_{n1})$				1k			10		AEC	Gough	DCTR	71
203	²⁹ Cu	$\sigma_{n,2n}$					1k			15		AEC	Gough	DCTR	71
204	²⁹ Cu	$\sigma_{n,\bar{e}}$					1k				20	AEC	Gough	DCTR	71
205	²⁹ Cu	$\sigma_{n,p}$					1k				20	AEC	Gough	DCTR	71
206	²⁹ Cu	$\sigma_{n,\bar{a}}$					1k				20	AEC	Gough	DCTR	71
207	²⁹ Cu	$\sigma_{n,n'}(g's)$	$P(E_{\bar{e}})$			Ths-	1k			15		AEC	Gough	DCTR	72
208	²⁹ Cu	Cap Spect			Th-	res.				15		AEC	Gough	DCTR	71
228	⁴⁰ Zr	Inelastic	$\sigma(E_{n1})$			Ths-	1k			15		AEC	Gough	DCTR	72
229	⁴⁰ Zr	$\sigma_{n,2n}$	$\sigma(\theta_{n1}, E_{n1})$				1k			10		AEC	Gough	DCTR	71
230	⁴⁰ Zr	$\sigma_{n,2n}$					1k			15		AEC	Gough	DCTR	71
233	⁴⁰ Zr	$\sigma_{n,\bar{e}}$					1k				20	AEC	Gough	DCTR	71
235	⁴⁰ Zr	$\sigma_{n,p}$					1k				20	AEC	Gough	DCTR	71
236	⁴⁰ Zr	$\sigma_{n,\bar{a}}$					1k				20	AEC	Gough	DCTR	71
238	⁴⁰ Zr	$\sigma_{n,n'}(g's)$	$P(E_{\bar{e}})$			Ths-	1k			15		AEC	Gough	DCTR	72
239	⁴⁰ Zr	Cap Spect			Th-	res.				15		AEC	Gough	DCTR	71
270	⁴¹ Nb	Inelastic	$\sigma(E_{n1})$			Ths-	1k			15		AEC	Gough	DCTR	72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
273	$^{41}_{41}\text{Nb}$	$\sigma_{n,2n}$	$\sigma(\theta_{n'}, E_{n'})$				1k			10		AEC	Gough	DCTR	71
274	$^{41}_{41}\text{Nb}$	$\sigma_{n,2n}$					1k			15		AEC	Gough	DCTR	71
277	$^{41}_{41}\text{Nb}$	$\sigma_{n,\bar{e}}$					1k				20	AEC	Gough	DCTR	71
278	$^{41}_{41}\text{Nb}$	$\sigma_{n,p}$					1k				20	AEC	Gough	DCTR	71
279	$^{41}_{41}\text{Nb}$	$\sigma_{n,\bar{e}}$					1k				20	AEC	Gough	DCTR	71
281	$^{41}_{41}\text{Nb}$	$\sigma_{n,n'}(\bar{e}'\text{'S})$			Th-	Ths-	1k			15		AEC	Gough	DCTR	72
282	$^{41}_{41}\text{Nb}$	Cap Spect	$P(E_{\bar{e}})$		Th-	res,				15		AEC	Gough	DCTR	71
284	$^{41}_{41}\text{Nb}$	Tot $\bar{e}$ Prod	$\sigma(E_{\bar{e}})$		Th-	to	1k			15		AEC	Gough	DCTR	71
290	$^{42}_{42}\text{Mo}$	Inelastic	$\sigma(E_{n'})$			Ths-	1k			15		AEC	Gough	DCTR	72
291	$^{42}_{42}\text{Mo}$	$\sigma_{n,2n}$	$\sigma(\theta_{n'}, E_{n'})$				1k			10		AEC	Gough	DCTR	71
292	$^{42}_{42}\text{Mo}$	$\sigma_{n,2n}$					1k			15		AEC	Gough	DCTR	71
295	$^{42}_{42}\text{Mo}$	$\sigma_{n,\bar{e}}$					1k				20	AEC	Gough	DCTR	71
296	$^{42}_{42}\text{Mo}$	$\sigma_{n,p}$					1k				20	AEC	Gough	DCTR	71
297	$^{42}_{42}\text{Mo}$	$\sigma_{n,\bar{e}}$					1k				20	AEC	Gough	DCTR	71
299	$^{42}_{42}\text{Mo}$	$\sigma_{n,n'}(\bar{e}'\text{'S})$			Th-	Thr-	1k			15		AEC	Gough	DCTR	71
300	$^{42}_{42}\text{Mo}$	Cap Spect	$P(E_{\bar{e}})$		Th-	res,				15		AEC	Gough	DCTR	71
301	$^{42}_{42}\text{Mo}$	Tot $\bar{e}$ Prod	$\sigma(E_{\bar{e}})$		Th-	to	1k			15		AEC	Gough	DCTR	71

SECTION V.

TABLE 5.C

DMA

Division of Military Application, Maj. Gen. Frank A. Camm, Asst. Gen Man. for Military Application

Phone: 301-973-4221

USAEC, Washington, D. C. 20545

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
4	${}^1_1\text{H}^3$	Elastic	$\sigma(\theta_n)$	II			14			10		LASL	Motz	DNA	65
5	${}^1_1\text{H}^3$	$\sigma_{n,2n}$		III			12,5			10		LASL	Motz	DNA	65
8	${}^2_2\text{He}^3$	$\sigma_{n,p}$		II		10-	3	1				GGA	Nordheim	DRDT	69
14	${}^3_3\text{Li}^6$	Emission	$\sigma(\theta_{n_1}, E_{n_1})$	I			8-14			≤10		LASL	Motz	DNA	65
15	${}^3_3\text{Li}^6$	$\sigma_{n,2n}$		I			8-16		5			LASL	Motz	DNA	66
18	${}^3_3\text{Li}^6$	$\sigma_{n,\bar{a}}$		I		1-	3	1				ANL	Avery	DRDT	69
					*****	*****	*****	***	***	***	***				
39	${}^3_3\text{Li}^7$	Emission	$\sigma(\theta_{n_1}, E_{n_1})$	I			5-16			10		LASL	Motz	DNA	63
40	${}^3_3\text{Li}^7$	$\sigma_{n,2n}$		I			8-16		5			LASL	Motz	DNA	65
44	${}^4_4\text{Be}$	Elastic	$\sigma(\theta_n)$	I			7-20			10		LLL	Howerton	DNA	62
					*****	*****	*****	***	***	***	***				
48	* ${}^4_4\text{Be}^7$	$\sigma_{n,p}$		II	Th-	to	15				50	LLL	Howerton	DNA	69
53	${}^5_5\text{B}^{10}$	$\sigma_{n,\bar{a}}$		I		1-	10	1-	5			ANL	Avery	DRDT	69
56	${}^6_6\text{C}$	Elastic	$\sigma(\theta_n)$	II			6-15		5			AFWL	Enz	DNA	69
58	${}^6_6\text{C}$	Emission	$\sigma(\theta_{n_1}, E_{n_1})$	II			8-15			10		AFWL	Enz	DNA	69
59	${}^6_6\text{C}$	Tot $\bar{E}$ Prod	$\sigma(\theta_{\bar{E}}, E_{\bar{E}})$	III			6-16			≤10		LASL	Biggers	DNA	65
64	${}^7_7\text{N}$	Elastic	$\sigma(\theta_n)$	I			7-15		5			AC	Greenhow	DNA	69
66	${}^7_7\text{N}$	Emission	$\sigma(\theta_{n_1}, E_{n_1})$	I			7-15			10		AC	Greenhow	DNA	69
67	${}^7_7\text{N}$	Absorption		I			1-15		5			AC	Greenhow	DNA	66
68	${}^7_7\text{N}$	Tot $\bar{E}$ Prod	$\sigma(\theta_{\bar{E}}, E_{\bar{E}})$	I			8-15			10		AC	Greenhow	DNA	69
69	${}^8_8\text{O}$	Elastic	$\sigma(\theta_n)$	II		10-	1		5			IRT	Preskitt	DRDT	69

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
71	^8_0O	Absorption		I			10-15		5			AFWL Enz	DNA		66
72	^8_0O	Tot $\bar{g}$ Prod	$\sigma(\theta_{\bar{g}}, E_{\bar{g}})$	I			10-15			10		LASL Biggers	DMA		62
75	^9_9F	Elastic	$\sigma(\theta_n)$	I			3-20			10		LLL Howerton	DMA		69
77	^9_9F	Emission	$\sigma(E_{n'})$	I		500-	20			10		LLL Howerton	DMA		69
80	^9_9F	$\sigma_{n,\bar{g}}$		I			9-14			10		LLL Howerton	DMA		69
88	$^{13}_{13}\text{Al}$	Elastic	$\sigma(\theta_n)$	I			8-16		5			LASL Biggers	DMA		66
102	$^{30}_{14}\text{Si}$	$\sigma_{n,\bar{g}}$	Act	III	.025	to	15				30	LLL Howerton	DMA		69
103	$^{34}_{16}\text{S}$	$\sigma_{n,\bar{g}}$	Act	I	.025	to	15				30	LLL Howerton	DMA		69
104	$^{41}_{19}\text{K}$	$\sigma_{n,\bar{g}}$	Act	II	.025	to	15				30	LLL Howerton	DMA		69
108	$^{44}_{20}\text{Ca}$	$\sigma_{n,\bar{g}}$	Act	I	.025	to	15				30	LLL Howerton	DMA		69
144	$^{55}_{25}\text{Mn}$	$\sigma_{n,\bar{g}}$		II	Th-	1				10		LLL Howerton	DMA		66
148	$^{54}_{26}\text{Fe}$	Elastic	$\sigma(\theta_n)$	I			8-16		5			LASL Biggers	DMA		66
153	$^{54}_{26}\text{Fe}$	Emission	$\sigma(E_{n'})$	I			5-15				20	LLL Howerton	DMA		70
154	$^{54}_{26}\text{Fe}$	Emission	$\sigma(\theta_{n'}, E_{n'})$	I			7-15			10		AFWL Enz	DNA		69
165	$^{56}_{26}\text{Fe}$	Tot $\bar{g}$ Prod	$\sigma(\theta_{\bar{g}}, E_{\bar{g}})$	II			8-15			10		GDFW Western	DNA		69
					*****	*****	*****	***	***	***	*****				
169	$^{54}_{26}\text{Fe}$	$\sigma_{n,\bar{g}}$	Act	II	.025-	to	15				30	LLL Howerton	DMA		69
					*****	*****	*****	***	***	***	*****				
171	$^{56}_{26}\text{Fe}$	$\sigma_{n,2n}$	Act.	II			Ths-15				30	LLL Howerton	DMA		69

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
173	$^{58}_{26}\text{Fe}$	$\sigma_{n,\bar{g}}$	Act	II	.025	to	15				30	LLL	Howerton	DMA	69
176	$^{60}_{27}\text{Co}$	$\sigma_{n,\bar{g}}$	Act	I	.025	to	15				30	LLL	Howerton	DMA	69
211	$^{63}_{29}\text{Cu}$	$\sigma_{n,\bar{g}}$	Act	III	.025	to	15				30	LLL	Howerton	DMA	69
213	$^{65}_{29}\text{Cu}$	$\sigma_{n,2n}$	Act.	III			Ths=15				30	LLL	Howerton	DMA	69
217	$^{64}_{30}\text{Zn}$	$\sigma_{n,\bar{g}}$	Act	I	.025	to	15				30	LLL	Howerton	DMA	69
218	$^{66}_{30}\text{Zn}$	$\sigma_{n,2n}$	Act.	I			Ths=15				30	LLL	Howerton	DMA	72
225	* $^{83}_{37}\text{Rb}$	$\sigma_{n,\bar{g}}$		I		.1-300					50	LLL	Howerton	DMA	69
226	* $^{84}_{37}\text{Rb}$	$\sigma_{n,\bar{g}}$		I		.1-300					50	LLL	Howerton	DMA	69
241	* $^{88}_{40}\text{Zr}$	$\sigma_{n,\bar{g}}$		I		.1-300					50	LLL	Howerton	DMA	69
242	* $^{89}_{40}\text{Zr}$	$\sigma_{n,\bar{g}}$		I		.1-300					50	LLL	Howerton	DMA	69
271	$^{91}_{41}\text{Nb}$	$\sigma_{n,n'}$	Isom State	I		Ths=	15				20	LLL	Howerton	DMA	69
275	$^{91}_{41}\text{Nb}$	$\sigma_{n,2n}$	Act.	I			Ths=15		≤5			LLL	Howerton	DMA	70
285	* $^{91}_{41}\text{Nb}$	$\sigma_{n,\bar{g}}$		I		.1-300					50	LLL	Howerton	DMA	69
286	* $^{92}_{41}\text{Nb}$	$\sigma_{n,\bar{g}}$		I		.1-300					50	LLL	Howerton	DMA	69
287	* $^{93}_{41}\text{Nb}$	$\sigma_{n,\bar{g}}$		I		.1-300					50	LLL	Howerton	DMA	69

REQ #	TARGET * Z A	REACTION TYPE QUANTITY	TYPE VARIABLE	PRI OR,	INCIDENT ENERGY eV keV MeV			PERCENT ACCURACY 1-3 4-9 ≤15 >15				REQUESTER LAB PERSON ORG			YR
330	⁶³ Eu	$\sigma_{n,\bar{g}}$	$\sigma(E_{\bar{g}})$	II	100-	200				10		LASL Motz	DMA	66	
331	⁶³ Eu	Tot $\bar{g}$ Prod		III		1-	15			*		LASL Motz	DMA	66	
						*****	*****	*****	***	***	***	*****			
332	* ⁶³ Eu ¹⁴⁸	$\sigma_{n,\bar{g}}$	Act.	I		.1-300				50		LLL Howerton	DMA	69	
						*****	*****	*****	***	***	***	*****			
							.1-300				50		LLL Howerton	DMA	69
333	* ⁶³ Eu ¹⁴⁹	$\sigma_{n,\bar{g}}$	Act.	I		.1-300				50		LLL Howerton	DMA	69	
						*****	*****	*****	***	***	***	*****			
							.1-300				50		LLL Howerton	DMA	69
334	* ⁶³ Eu ¹⁵⁰	$\sigma_{n,\bar{g}}$	Act.	I		.1-300				50		LLL Howerton	DMA	69	
						*****	*****	*****	***	***	***	*****			
							.1-300				50		LLL Howerton	DMA	69
335	⁶³ Eu ¹⁵¹	$\sigma_{n,2n}$	$\sigma(E_{\bar{g}})$	I			14			15		LLL Howerton	DMA	69	
337	⁶³ Eu ¹⁵¹	$\sigma_{n,\bar{g}}$		I		.1-300					20		LLL Howerton	DMA	69
						*****	*****	*****	***	***	***	*****			
338	* ⁶³ Eu ¹⁵²	$\sigma_{n,\bar{g}}$	Act.	I		.1-300				30		LASL Bell	DMA	70	
						*****	*****	*****	***	***	***	*****			
							.1-300				30		LASL Bell	DMA	70
341	* ⁶³ Eu ¹⁵⁴	$\sigma_{n,\bar{g}}$	Act.	I		.1-300				30		LASL Bell	DMA	70	
						*****	*****	*****	***	***	***	*****			
							.1-300				30		LASL Bell	DMA	70
345	⁶⁴ Gd	$\sigma_{n,\bar{g}}$	$\sigma(E_{\bar{g}})$	II	100-	200				10		LASL Motz	DMA	66	
346	⁶⁴ Gd	Tot $\bar{g}$ Prod		III		1-	15			*		LASL Motz	DMA	66	
						*****	*****	*****	***	***	***	*****			
357	⁶⁶ Dy	$\sigma_{n,\bar{g}}$	$\sigma(E_{\bar{g}})$	II	100-	200				10		LASL Motz	DMA	66	
358	⁶⁶ Dy	Tot $\bar{g}$ Prod		III		1-	15			*		LASL Motz	DMA	66	
						*****	*****	*****	***	***	***	*****			
359	* ⁶⁹ Tm ¹⁶⁷	$\sigma_{n,\bar{g}}$	Act.	I		.1-300				50		LLL Howerton	DMA	69	
						*****	*****	*****	***	***	***	*****			
							.1-300				50		LLL Howerton	DMA	69
360	* ⁶⁹ Tm ¹⁶⁸	$\sigma_{n,\bar{g}}$	Act.	I		.1-300				50		LLL Howerton	DMA	69	
						*****	*****	*****	***	***	***	*****			
							.1-300				50		LLL Howerton	DMA	69
361	⁶⁹ Tm	$\sigma_{n,2n}$	Act.	I			Ths=15		≤5			LLL Howerton	DMA	70	

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
365	* $^{173}_{71}\text{Lu}$	$\sigma_{n,\bar{g}}$		I		.1-300					50	LLL	Howerton	DMA	69
					*****	*****	*****	***	***	***	*****				
366	* $^{174}_{71}\text{Lu}$	$\sigma_{n,\bar{g}}$		I		.1-300					50	LLL	Howerton	DMA	69
					*****	*****	*****	***	***	***	*****				
367	$^{175}_{71}\text{Lu}$	$\sigma_{n,2n}$	Act.	I			Ths=15		≤5			LLL	Howerton	DMA	70
368	$^{175}_{71}\text{Lu}$	$\sigma_{n,\bar{g}}$		I		.1-300					20	LLL	Howerton	DMA	69
384	$^{180}_{74}\text{W}$	$\sigma_{n,\bar{g}}$	Act	I	.025-	to	15				30	LLL	Howerton	DMA	69
					*****	*****	*****	***	***	***	*****				
385	$^{182}_{74}\text{W}$	$\sigma_{n,2n}$	Act.	I			Ths=15				30	LLL	Howerton	DMA	69
					*****	*****	*****	***	***	***	*****				
389	$^{184}_{74}\text{W}$	$\sigma_{n,\bar{g}}$	Act	I	.025-	100					30	LLL	Howerton	DMA	69
					*****	*****	*****	***	***	***	*****				
390	$^{186}_{74}\text{W}$	$\sigma_{n,2n}$	Act.	I			Ths=15				30	LLL	Howerton	DMA	69
394	$^{197}_{79}\text{Au}$	$\sigma_{n,\bar{g}}$		II	.5	1*		1				BET	Bayard	DNR	67
399	$^{204}_{82}\text{Pb}$	$\sigma_{n,n'}$	Isom State	I			Ths=15				30	LLL	Howerton	DMA	69
					*****	*****	*****	***	***	***	*****				
400	$^{208}_{82}\text{Pb}$	$\sigma_{n,\bar{g}}$	Act	II	.025	to	15				30	LLL	Howerton	DMA	69
412	$^{233}_{92}\text{U}$	Emission	$\sigma(E_{n'})$	I			5-15				20	LLL	Howerton	DMA	70
413	$^{233}_{92}\text{U}$	$\sigma_{n,2n}$		II			Ths=15			10		LASL	Barr	DMA	67
416	$^{233}_{92}\text{U}$	Fis Ratio	wrt ^{235}U	I		10-	15	1				LASL	Hansen	DMA	67
421	$^{233}_{92}\text{U}$	Nu Bar	Prompt	I			7-20	3				LLL	Howerton	DMA	62
					*****	*****	*****	***	***	***	*****				
429	$^{234}_{92}\text{U}$	$\sigma_{n,2n}$	Act.	I			Ths=15		≤5			LLL	Howerton	DMA	70

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REQ #	TARGET * Z A	REACTION TYPE		PRI OK	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
430	$^{92}\text{U}^{234}$	$\sigma_{n,3n}$		II			Ths-15				20	LASL Barr		DMA	67
432	$^{92}\text{U}^{234}$	Nu Bar	Prompt	I		500-	20	3				LLL Howerton		DMA	62
					*****	*****	*****	***	***	***	*****				
433	$^{92}\text{U}^{235}$	Elastic	$\sigma(E_n)$	II			1-5				20	ANL Avery		DRDT	69
434	$^{92}\text{U}^{235}$	Inelastic	$\sigma(E_{n'})$	II		50-	6			10		ANL Avery		DRDT	69
435	$^{92}\text{U}^{235}$	Emission	$\sigma(E_{n'})$	I			5-15				20	LLL Howerton		DMA	70
436	$^{92}\text{U}^{235}$	Emission	$\sigma(E_{n'}, E_{n'})$	I			6-20		5			LLL Howerton		DMA	62
437	$^{92}\text{U}^{235}$	$\sigma_{n,2n}$	Act.	I			Ths-15		≤5			LLL Howerton		DMA	70
438	$^{92}\text{U}^{235}$	$\sigma_{n,3n}$		II			Ths-16			10		LASL Barr		DMA	67
442	$^{92}\text{U}^{235}$	$\sigma_{n,f}$		I		10-	15	1				LASL Hansen		DMA	66
					*****	*****	*****	***	***	***	*****				
459	$^{92}\text{U}^{236}$	Nu Bar	Prompt	I		500-	14	3				LLL Howerton		DMA	62
					*****	*****	*****	***	***	***	*****				
463	* $^{92}\text{U}^{237}$	$\sigma_{n,f}$		II	100-		16			10		LASL Barr		DMA	67
464	* $^{92}\text{U}^{237}$	Destruct	of Target	I		1-	15			10		LLL Howerton		DMA	70
					*****	*****	*****	***	***	***	*****				
467	$^{92}\text{U}^{238}$	Emission	$\sigma(E_{n'})$	I			5-15				20	LLL Howerton		DMA	70
469	$^{92}\text{U}^{238}$	$\sigma_{n,3n}$		II			Ths-15				20	LLL Howerton		DMA	69
470	$^{92}\text{U}^{238}$	Fis Ratio	wrt ^{235}U	I		500-	15	1-	5			LASL Hansen		DMA	67
476	$^{92}\text{U}^{238}$	$\sigma_{n,g}$		I	Th-	to	15			10		LLL Howerton		DMA	69
481	$^{93}\text{Np}^{237}$	$\sigma_{n,2n}$		II			Ths-15			10		SRL Dessauer		DPHM	67
483	$^{93}\text{Np}^{237}$	Fis Ratio	wrt ^{235}U	III	20-	50				10		LASL Hansen		-DMA	66
486	$^{94}\text{Pu}^{238}$	$\sigma_{n,2n}$		I			Ths-15			15		LLL Howerton		DMA	69
487	$^{94}\text{Pu}^{238}$	$\sigma_{n,3n}$		I			14				50	LLL Howerton		DMA	69
489	$^{94}\text{Pu}^{238}$	Fis Ratio	wrt ^{235}U	I		10-	5	3				LASL Hansen		DMA	66

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
490	94Pu ²³⁸	Nu Bar	Prompt	I		10-	15	3				LLL	Howerton	DMA	62
492	94Pu ²³⁸	$\sigma_{n,\bar{e}}$		I		.1-300					50	LLL	Howerton	DMA	69
493	94Pu ²³⁸	$\sigma_{n,p}$		II		to	15				50	LLL	Howerton	DMA	69
494	94Pu ²³⁸	Destruct	of Target	I		1-	1		5			LASL	Motz	DMA	66
					*****	*****	*****	***	***	***	*****				
495	94Pu ²³⁹	Elastic	$\sigma(E_n)$	II			1-3			10		ANL	Avery	DRDT	69
497	94Pu ²³⁹	Emission	$\sigma(E_{n'})$	I			5-15				20	LLL	Howerton	DMA	70
498	94Pu ²³⁹	$\sigma_{n,2n}$		I			Ths=15			10		LASL	Barr	DMA	67
499	94Pu ²³⁹	$\sigma_{n,3n}$		II			Ths=15				20	LASL	Barr	DMA	67
502	94Pu ²³⁹	Fis Ratio	wrt U ²³⁵	I		10-	14	2				LMFH	Hemmig-AEC	DRDT	72
					*****	*****	*****	***	***	***	*****				
518	94Pu ²⁴⁰	Fis Ratio	wrt U ²³⁵	III		1=100			5			ACKP	Hannum	DRDT	72
523	94Pu ²⁴⁰	Alpha		II		150-	7			10		LLL	Howerton	DMA	62
					*****	*****	*****	***	***	***	*****				
527	94Pu ²⁴¹	Fis Ratio	wrt U ²³⁵	II		10-	15	1				LASL	Hansen	DMA	66
529	94Pu ²⁴¹	Nu Bar	Prompt	II		500-	14	3				LLL	Howerton	DMA	62
					*****	*****	*****	***	***	***	*****				
534	94Pu ²⁴²	$\sigma_{n,2n}$		I			Ths=15			15		LLL	Howerton	DMA	69
536	94Pu ²⁴²	Nu Bar	Prompt	II		500-	14	3				LLL	Howerton	DMA	62
539	94Pu ²⁴²	$\sigma_{n,\bar{e}}$	Act	I		.1-300					50	LLL	Howerton	DMA	69
540	94Pu ²⁴²	$\sigma_{n,p}$		II			14				20	LASL	Bell	DMA	67
					*****	*****	*****	***	***	***	*****				
542	95Am ²⁴¹	$\sigma_{n,2n}$		I			Ths=15			15		LLL	Howerton	DMA	69
543	95Am ²⁴¹	$\sigma_{n,\bar{e}}$		I	Th-	1				10		SRL	Dessauer	DPMM	67
544	95Am ²⁴¹	$\sigma_{n,\bar{e}}$		I		.1-300					50	LLL	Howerton	DMA	69
					*****	*****	*****	***	***	***	*****				
547	95Am ²⁴²	$\sigma_{n,\bar{e}}$		II	Th	to	10			15		GE	Hutchins	DRDT	72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
553	$^{96}\text{Cm}^{243}$	$\sigma_{n,f}$		II	Th-	10				10		SRL	Dessauer	DPHM	67
					*****	*****	*****	***	***	***	*****				
555	$^{96}\text{Cm}^{244}$	$\sigma_{n,2n}$		I			Ths-15			15		LLL	Howerton	DMA	69
556	$^{96}\text{Cm}^{244}$	$\sigma_{n,f}$		I		10-100				10		LASL	Cowan	DMA	69
558	$^{96}\text{Cm}^{244}$	$\sigma_{n,\bar{e}}$		I		1-300					50	LLL	Howerton	DMA	69
					*****	*****	*****	***	***	***	*****				
560	$^{96}\text{Cm}^{245}$	$\sigma_{n,f}$		I	Th-	10				10		SRL	Dessauer	DPHM	67
					*****	*****	*****	***	***	***	*****				
563	$^{96}\text{Cm}^{246}$	$\sigma_{n,f}$		I		10-100				10		LASL	Cowan	DMA	69
					*****	*****	*****	***	***	***	*****				
566	$^{96}\text{Cm}^{247}$	$\sigma_{n,f}$		I	Th-	10			5-	10		SRL	Dessauer	DPHM	67
					*****	*****	*****	***	***	***	*****				
569	$^{96}\text{Cm}^{248}$	$\sigma_{n,f}$		I		10-100				10		LASL	Cowan	DMA	69
					*****	*****	*****	***	***	***	*****				
573	$^{98}\text{Cf}^{249}$	$\sigma_{n,f}$		I		10-100				10		LASL	Cowan	DMA	69
					*****	*****	*****	***	***	***	*****				
575	$^{98}\text{Cf}^{250}$	$\sigma_{n,f}$		I	Th-	10				10		SRL	Dessauer	DPHM	67
					*****	*****	*****	***	***	***	*****				
578	$^{98}\text{Cf}^{252}$	$\sigma_{n,f}$		I		10-100				10		LASL	Cowan	DMA	69
					*****	*****	*****	***	***	***	*****				
584	* $^{99}\text{Es}^{253}$	$\sigma_{n,f}$		I		10-100				10		LASL	Cowan	DMA	69
					*****	*****	*****	***	***	***	*****				
585	* $^{99}\text{Es}^{254}$	Alpha		II	Th-	20					20	LASL	Bell	DMA	67
					*****	*****	*****	***	***	***	*****				
586	* $^{100}\text{Fm}^{255}$	$\sigma_{n,f}$		I		10-100				10		LASL	Cowan	DMA	69
					*****	*****	*****	***	***	***	*****				
587	* $^{100}\text{Fm}^{257}$	$\sigma_{n,f}$		I		10-100				10		LASL	Cowan	DMA	69
					*****	*****	*****	***	***	***	*****				

SECTION V.

TABLE 5.D

DNA

Department of Defense DOD

Jack W. Rosengren

Phone: 202-694-5044

Defense Nuclear Agency

(Capt. Dean Kaul) Radiation Transport Project Officer

Phone: 202-694-5395

REQ #	TARGET			REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
	*	Z	A	QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
56		6	C	Elastic	$\sigma(\theta_n)$	II			6-15		5			AFWL	Enz	DNA	69
58		6	C	Emission	$\sigma(\theta_{n'}, E_{n'})$	II			8-15			10		AFWL	Enz	DNA	69
59		6	C	Tot $\bar{E}$ Prod	$\sigma(\theta_{\bar{E}}, E_{\bar{E}})$	III			6-16			<10		LASL	Biggers	DNA	65
60		6	C	Absorption		II			10-15		5			AFWL	Enz	DNA	69
64		7	N	Elastic	$\sigma(\theta_n)$	I			7-15		5			AC	Greenhow	DNA	69
65		7	N	Elastic	$\sigma(\theta_n)$	I			7-15		5			NEL	Eccleshall	DNA	69
66		7	N	Emission	$\sigma(\theta_{n'}, E_{n'})$	I			7-15			10		AC	Greenhow	DNA	69
67		7	N	Absorption		I			1-15		5			AC	Greenhow	DNA	66
68		7	N	Tot $\bar{E}$ Prod	$\sigma(\theta_{\bar{E}}, E_{\bar{E}})$	I			8-15			10		AC	Greenhow	DNA	69
69		8	O	Elastic	$\sigma(\theta_n)$	II		10-	1		5			IRT	Preskitt	DRDT	69
70		8	O	Emission	$\sigma(\theta_{n'}, E_{n'})$	I			8-15			10		AFWL	Enz	DNA	69
71		8	O	Absorption		I			10-15		5			AFWL	Enz	DNA	66
72		8	O	Tot $\bar{E}$ Prod	$\sigma(\theta_{\bar{E}}, E_{\bar{E}})$	I			10-15			10		LASL	Biggers	DNA	62
82		11	Na	Elastic	$\sigma(\theta_n)$	II			8-15		5			NEL	Eccleshall	DNA	69
84		11	Na	Emission	$\sigma(\theta_{n'}, E_{n'})$	II			4-15			10		NEL	Eccleshall	DNA	69
88		13	Al	Elastic	$\sigma(\theta_n)$	I			8-16		5			LASL	Biggers	DNA	66
92		13	Al	Emission	$\sigma(\theta_{n'}, E_{n'})$	I			8-15			10		AFWL	Enz	DNA	69
99		13	Al	$\sigma_{n,p}$	Act	III			5-11.9			10		NEL	Eccleshall	DNA	69
100		14	Si	Elastic	$\sigma(\theta_n)$	II			8-15			10		NEL	Eccleshall	DNA	69
101		14	Si	Emission	$\sigma(\theta_{n'}, E_{n'})$	II			8-15			10		NEL	Eccleshall	DNA	69
105		20	Ca	Elastic	$\sigma(\theta_n)$	II			8-15			10		NEL	Eccleshall	DNA	69

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
106	²⁰ Ca	Emission	$\sigma(\theta_{n1}, E_{n1})$	II			8-15			10		NEL	Eccleshall	DNA	69
107	²⁰ Ca	Tot $\bar{\sigma}$ Prod	$\sigma(\theta_{\bar{\sigma}}, E_{\bar{\sigma}})$	II			5-15			10		NEL	Eccleshall	DNA	69
112	²² Ti	Tot $\bar{\sigma}$ Prod	$\sigma(\theta_{\bar{\sigma}}, E_{\bar{\sigma}})$	III			4-14				20	GDFW	Western	DNA	63
113	²² Ti ⁴⁶	$\sigma_{n,p}$	Act	II			1-18			10		HEDL	McElroy	DRDT	69
114	²² Ti ⁴⁷	$\sigma_{n,p}$	Act	II			>1			10		HEDL	McElroy	DRDT	69
115	²² Ti ⁴⁸	$\sigma_{n,p}$	Act	II			>1			10		HEDL	McElroy	DRDT	69
122	²³ V	$\sigma_{n,\bar{\sigma}}$	Act	II	Th				5			AFIT	Dooley	DNA	62
141	²⁴ Cr	Tot $\bar{\sigma}$ Prod	$\sigma(E_{\bar{\sigma}})$	I	500=	20				15*		SNPO	Fleishman	DSNS	69
145	²⁵ Mn	Tot $\bar{\sigma}$ Prod	$\sigma(E_{\bar{\sigma}})$	I	300=	120				15*		SNPO	Fleishman	DSNS	69
154	²⁶ Fe	Emission	$\sigma(\theta_{n1}, E_{n1})$	I			7-15			10		AFWL	Enz	DNA	69
165	²⁶ Fe	Tot $\bar{\sigma}$ Prod	$\sigma(\theta_{\bar{\sigma}}, E_{\bar{\sigma}})$	II			8-15			10		GDFW	Western	DNA	69
170	²⁶ Fe ⁵⁴	$\sigma_{n,p}$	Act	III			1-18			15		BET	Bayard	DNR	72
177	²⁷ Co	Tot $\bar{\sigma}$ Prod	$\sigma(E_{\bar{\sigma}})$	I	100=	100				15*		SNPO	Fleishman	DSNS	69
196	²⁸ Ni	Tot $\bar{\sigma}$ Prod	$\sigma(E_{\bar{\sigma}})$	II		12-340				15*		SNPO	Fleishman	DSNS	69
198	²⁸ Ni ⁵⁸	$\sigma_{n,p}$	Act	III			9.4-14			10		NEL	Eccleshall	DNA	69

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	15	>15	LAB	PERSON	ORG	
199	28 ⁶⁰ Ni	$\sigma_{n,p}$	Act	III			2=12.5			10		NEL	Eccleshall	DNA	69
209	29 ^{Cu}	Tot $\bar{e}$ Prod	$\sigma(E_{\bar{e}})$	II	200-	50				15*		SNPO	Fleishman	DSNS	69
216	30 ^{Zn}	Tot $\bar{e}$ Prod	$\sigma(E_{\bar{e}})$	I	200-	25				15*		SNPO	Fleishman	DSNS	69
219	32 ^{Ge}	Emission	$\sigma(\theta_{n'}, E_{n'})$	II			1=15			10		NEL	Eccleshall	DNA	69
220	32 ^{Ge}	Tot $\bar{e}$ Prod	$\sigma(\theta_{\bar{e}}, E_{\bar{e}})$	II			1=15			10		NEL	Eccleshall	DNA	69
221	33 ^{As}	Elastic	$\sigma(\theta_n)$	II	Th	to	14			15		IRT	Russell	DNA	69
222	33 ^{As}	Emission	$\sigma(\theta_{n'})$	II		Th=	14			15		IRT	Russell	DNA	69
240	40 ^{Zr}	Tot $\bar{e}$ Prod	$\sigma(E_{\bar{e}})$	II	100-	20				15*		SNPO	Fleishman	DSNS	69
283	41 ^{Nb}	Tot $\bar{e}$ Prod	$\sigma(E_{\bar{e}})$	II	30-	75				15*		SNPO	Fleishman	DSNS	69
302	42 ^{Mo}	Tot $\bar{e}$ Prod	$\sigma(E_{\bar{e}})$	I	10-	9				15*		SNPO	Fleishman	DSNS	69
381	74 ^W	Emission	$\sigma(\theta_{n'}, E_{n'})$	I			4=14			10		AEWL	Enz	DNA	69
382	74 ^W	Tot $\bar{e}$ Prod	$\sigma(E_{\bar{e}})$	I	2-	2.5				15*		SNPO	Fleishman	DSNS	69
396	82 ^{Pb}	Emission	$\sigma(\theta_{n'}, E_{n'})$	II			3=15			10		NEL	Eccleshall	DNA	69
397	82 ^{Pb}	Tot $\bar{e}$ Prod	$\sigma(E_{\bar{e}})$	II			8=15			10		NEL	Eccleshall	DNA	69
406	90 Th	Tot $\bar{e}$ Prod	$\sigma(E_{\bar{e}})$	II		500	=15			10		AEWL	Enz	DNA	69

SECTION V.

TABLE 5.E

DNMS

Division of Nuclear Materials Security, Delmar L. Crowson, Director

Phone: 301-973-3671

USAEC, Washington, D. C. 20545

Contacts have been set up by Nuclear Materials Security at ANC, BNL, IRT, and LASL

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	15	>15	LAB	PERSON	ORG	
47	4 Be	(n,p) Li ⁹	$\bar{E} = \text{Be}^{9*} \rightarrow n$	II			14			10		LASL	Walton	DNMS	70
408	90 Th	Delayed $\bar{E}$ Y	$P(E_{\bar{E}}, T^{1/2})$	II			2.14				35	BNL	Kouts	DNMS	69
424	92 U ²³³	Delayed $\bar{E}$ Y	$P(E_{\bar{E}}, T^{1/2})$	I			2.14				35	BNL	Kouts	DNMS	69
449	92 U ²³⁵	Fis $\bar{E}$ Y	$P(E_{\bar{E}})$	II	Th					15		LASL	Walton	DNMS	70
451	92 U ²³⁵	Delayed n Y		II			5.14		5			LASL	Walton	DNMS	70
453	92 U ²³⁵	Delayed $\bar{E}$ Y	$P(E_{\bar{E}}, T^{1/2})$	I			2.14				35	BNL	Kouts	DNMS	69
460	92 U ²³⁶	Fis Spect	$P(E_{n'})$	II			*			10		LASL	Walton	DNMS	70
461	92 U ²³⁶	Delayed n Y		I			3.14			10		LASL	Walton	DNMS	70
473	92 U ²³⁸	Delayed n Y		II			5.14		5			LASL	Walton	DNMS	70
479	92 U ²³⁸	Delayed $\bar{E}$ Y	$P(E_{\bar{E}}, T^{1/2})$	II			2.14				35	BNL	Kouts	DNMS	69
505	94 Pu ²³⁹	Delayed n Y		II			3.14			10		LASL	Walton	DNMS	70
508	94 Pu ²³⁹	Delayed $\bar{E}$ Y	$P(E_{\bar{E}}, T^{1/2})$	I			2.14				35	BNL	Kouts	DNMS	69
509	94 Pu ²³⁹	Fis $\bar{E}$ Y	$P(E_{\bar{E}})$	II	Th					15		LASL	Walton	DNMS	70
510	94 Pu ²³⁹	Cap Spect	$P(E_{\bar{E}})$	III	Th-100						20	LASL	Walton	DNMS	70
520	94 Pu ²⁴⁰	Delayed n Y		II		750e	14				20	LASL	Walton	DNMS	70
525	94 Pu ²⁴⁰	Delayed $\bar{E}$ Y	$P(E_{\bar{E}}, T^{1/2})$	II			2.14				35	BNL	Kouts	DNMS	69
533	94 Pu ²⁴¹	Delayed n Y		III	Th	to	14			10		LASL	Walton	DNMS	70
537	94 Pu ²⁴²	Delayed n Y		III			3.14				20	LASL	Walton	DNMS	70

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
588	$^1_1\text{H}^2$	$\bar{E},n$	Total n Y	I			Ths-10			10		IRT	Bramblett	DNMS	70
589	^6_3Li	$\bar{E},n$	Total n Y	III			Ths-10				20	IRT	Bramblett	DNMS	72
590	^9_4Be	$\bar{E},n$	Total n Y	II			Ths-10				20	IRT	Bramblett	DNMS	72
591	$^{13}_6\text{C}$	$\bar{E},n$	Total n Y	II			Ths-10				20	IRT	Bramblett	DNMS	72
592	$^{17}_8\text{O}$	$\bar{E},n$	Total n Y	II			Ths-10				20	IRT	Bramblett	DNMS	72
593	$^{232}_{90}\text{Th}$	$\bar{E},n$	Total n Y	II			Ths-10			10		IRT	Bramblett	DNMS	72
594	$^{232}_{90}\text{Th}$	$\bar{E},n$	Delayd n Y	I			Ths-10			10		IRT	Bramblett	DNMS	72
595	$^{232}_{90}\text{Th}$	$\bar{E},f$	Del $\bar{E}$ Spec	III			10			10		IRT	Bramblett	DNMS	72
596	$^{233}_{92}\text{U}$	$\bar{E},n$	Total n Y	I			Ths-10			10		IRT	Bramblett	DNMS	72
597	$^{233}_{92}\text{U}$	$\bar{E},n$	Delayd n Y	I			Ths-10			10		IRT	Bramblett	DNMS	72
598	$^{233}_{92}\text{U}$	$\bar{E},f$	Del $\bar{E}$ Spec	II			10			10		IRT	Bramblett	DNMS	72
					*****	*****	*****	***	***	***	*****				
599	$^{234}_{92}\text{U}$	$\bar{E},n$	Total n Y	II			Ths-10			30		IRT	Bramblett	DNMS	72
600	$^{234}_{92}\text{U}$	$\bar{E},n$	Delayd n Y	III			Ths-10			30		IRT	Bramblett	DNMS	72
601	$^{234}_{92}\text{U}$	$\bar{E},f$	Del $\bar{E}$ Spec	III			10			30		IRT	Bramblett	DNMS	72
					*****	*****	*****	***	***	***	*****				
602	$^{235}_{92}\text{U}$	$\bar{E},n$	Total n Y	II			Ths-10			10		IRT	Bramblett	DNMS	72
603	$^{235}_{92}\text{U}$	$\bar{E},n$	Delayd n Y	II			Ths-10			10		IRT	Bramblett	DNMS	72
604	$^{235}_{92}\text{U}$	$\bar{E},f$	Del $\bar{E}$ Spec	II			10			10		IRT	Bramblett	DNMS	72
					*****	*****	*****	***	***	***	*****				
605	$^{236}_{92}\text{U}$	$\bar{E},n$	Total n Y	II			Ths-10			30		IRT	Bramblett	DNMS	72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
606	$^{92}_{236}\text{U}$	$\bar{g},n$	Delayd n Y	II			Ths-10			30		IRT	Bramblett	DNMS	72
607	$^{92}_{236}\text{U}$	$\bar{g},f$	Del $\bar{g}$ Spec	III			10			30		IRT	Bramblett	DNMS	72
					*****	*****	*****	***	***	***	*****				
608	$^{92}_{238}\text{U}$	$\bar{g},n$	Total n Y	II			Ths-10			10		IRT	Bramblett	DNMS	72
609	$^{92}_{238}\text{U}$	$\bar{g},n$	Delayd n Y	II			Ths-10			10		IRT	Bramblett	DNMS	72
610	$^{92}_{238}\text{U}$	$\bar{g},f$	Del $\bar{g}$ Spec	II			10			10		IRT	Bramblett	DNMS	72
611	$^{94}_{239}\text{Pu}$	$\bar{g},n$	Total n Y	II			Ths-10			10		IRT	Bramblett	DNMS	72
612	$^{94}_{239}\text{Pu}$	$\bar{g},n$	Delayd n Y	II			Ths-10			10		IRT	Bramblett	DNMS	72
613	$^{94}_{239}\text{Pu}$	$\bar{g},f$	Del $\bar{g}$ Spec	II			10			10		IRT	Bramblett	DNMS	72
					*****	*****	*****	***	***	***	*****				
614	$^{94}_{240}\text{Pu}$	$\bar{g},n$	Total n Y	II			Ths-10			10		IRT	Bramblett	DNMS	72
615	$^{94}_{240}\text{Pu}$	$\bar{g},n$	Delayd n Y	II			Ths-10			10		IRT	Bramblett	DNMS	72
616	$^{94}_{240}\text{Pu}$	$\bar{g},f$	Del $\bar{g}$ Spec	II			10			10		IRT	Bramblett	DNMS	72
					*****	*****	*****	***	***	***	*****				
617	$^{94}_{241}\text{Pu}$	$\bar{g},n$	Total n Y	III			Ths-10			30		IRT	Bramblett	DNMS	72
618	$^{94}_{241}\text{Pu}$	$\bar{g},n$	Delayd n Y	III			Ths-10			30		IRT	Bramblett	DNMS	72
619	$^{94}_{241}\text{Pu}$	$\bar{g},f$	Del $\bar{g}$ Spec	III			10			30		IRT	Bramblett	DNMS	72

SECTION V.

TABLE 5.F

DNR

Division of Naval Reactors, H. G. Rickover, Vice Admiral (USN), Director

Phone: 301-973-5771

USAEC, Washington, D. C. 20545

Contacts at BETTIS and KAPL

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
73	8^{17}	$\sigma_{a,n}$		II			Ths=7				20	KAPL	Ehrlich	DNR	72
74	8^{18}	$\sigma_{a,n}$		III	*****	*****	Ths=7	***	***	***	*****	BET	Bayard	DNR	66
182	28^{N1}	Elastic	$\sigma(\theta_n)$	II			1.5-3		5-	10		ANL	Avery	DRDT	72
195	28^{N1}	Tot $\bar{\sigma}$ Prod	$\sigma(E_n)$	II	Th	to	10			10		BET	Bayard	DNR	66
200	$28^{N1^{61}}$	$\bar{\sigma}_n$		I	*****	*****	*****	***	***	***	*****	KAPL	Ehrlich	DNR	69
303	* $42^{Mo^{99}}$	$\sigma_{n,\bar{g}}$		II	.001=	1					20	BET	Bayard	DNR	67
304	* $44^{Ru^{103}}$	$\sigma_{n,\bar{g}}$		II	.001=	1					20	BET	Bayard	DNR	67
305	45^{Rh}	$\sigma_{n,\bar{g}}$		II	.5=	1				10		KAPL	Ehrlich	DNR	67
320	* $60^{Nd^{147}}$	$\sigma_{n,\bar{g}}$		I	.001=	1			5	to	20	KAPL	Ehrlich	DNR	67
321	* $61^{Pm^{147}}$	$\sigma_{n,\bar{g}}$		I	.001=	1				10		BET	Bayard	DNR	67
324	* $61^{Pm^{149}}$	$\sigma_{n,\bar{g}}$		I	.001=	1					20	BET	Bayard	DNR	67
369	72^{Hf}	Elastic	$\sigma(\theta_n)$	II			1.5=10			10		BET	Bayard	DNR	66
370	72^{Hf}	Emission	$\sigma(E_{n'})$	II			1.5=10			15		BET	Bayard	DNR	66
371	72^{Hf}	$\sigma_{n,\bar{g}}$		II	200-	50					20	BET	Bayard	DNR	62
374	$72^{Hf^{177}}$	$\sigma_{n,\bar{g}}$		I	.001=	5			4	to	20	BET	Bayard	DNR	62
376	$72^{Hf^{179}}$	$\sigma_{n,\bar{g}}$		I	.001=	5			5	to	20	BET	Bayard	DNR	62

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
377	$^{180}_{72}\text{Hf}$	$\sigma_{n,\bar{g}}$		I	,001-	5			4	to	20	BET	Bayard	DNR	67
379	$^{73}_{73}\text{Ta}$	$\sigma_{n,\bar{g}}$		I		1-	10		5-	10		AI	Alter	DNDT	69
394	$^{79}_{79}\text{Au}$	$\sigma_{n,\bar{g}}$		II	,5	1*		1				BET	Bayard	DNR	67
405	$^{90}_{90}\text{Th}$	Absorption		II	100	to	1	3-	5			BET	Bayard	DNR	69
407	$^{90}_{90}\text{Th}$	Tot $\bar{K}$ Prod	$\sigma(E_{\bar{K}}, E_{\bar{g}})$	II	,5	to	10			10		BET	Bayard	DNR	67
450	$^{235}_{92}\text{U}$	Delayed n Y	$P(E_{n,})$	II	Th					15		KAPL	Ehrlich	DNR	69
452	$^{235}_{92}\text{U}$	Cap Spect	$P(E_{\bar{g}})$	II	Th-15					10		BET	Bayard	DNR	67
454	$^{235}_{92}\text{U}$	Res Par		I	Th-200					10		ANL	Avery	DNDT	69
496	$^{239}_{94}\text{Pu}$	Inelastic	$\sigma(E_{n,})$	I		10-	10				20	KAPL	Ehrlich	DNK	72
514	$^{239}_{94}\text{Pu}$	Fis Prod Y	of Nd^{147}	II	Th			3				BET	Bayard	DNR	67

SECTION V.

TABLE 5.G

DPMM

Division of Production and Materials Management, F. P. Baranowski, Director

Phone: 301-973-4413

USAEC, Washington, D. C. 20545

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YF
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
232	$_{40}\text{Zr}$	$\sigma_{n,\bar{g}}$		II	Th-	1			5			BNW	Leonard	DPMM	67
336	$_{63}\text{Eu}^{151}$	$\sigma_{n,\bar{g}}$		II	.001-	1		2-	5			SRL	Dessauer	DPMM	67
					*****	*****	*****	***	***	***	*****				
339	$_{63}\text{Eu}^{153}$	$\sigma_{n,\bar{g}}$		II	.001-	1		2-	5			GE	Snyder	DRDT	67
362	$_{69}\text{Tm}$	$\sigma_{n,\bar{g}}$		I	Th-	1			5			BNW	Leonard	DPMM	67
					*****	*****	*****	***	***	***	*****				
363	* $_{69}\text{Tm}^{170}$	$\sigma_{n,\bar{g}}$		I	Th-	1				10		BNW	Leonard	DPMM	67
					*****	*****	*****	***	***	***	*****				
364	* $_{69}\text{Tm}^{171}$	$\sigma_{n,\bar{g}}$		I	Th-	1				10		BNW	Leonard	DPMM	67
395	* $_{81}\text{Tl}^{204}$	$\sigma_{n,\bar{g}}$		II	Th					10		BNW	Leonard	DPMM	65
481	$_{93}\text{Np}^{237}$	$\sigma_{n,2n}$		II			Ths-15			10		SRL	Dessauer	DPMM	67
482	$_{93}\text{Np}^{237}$	$\sigma_{n,f}$		II		1-	5			10		SRL	Dessauer	DPMM	67
484	$_{93}\text{Np}^{237}$	$\sigma_{n,\bar{g}}$		I	.001-	1		3	to	10		BNW	Leonard	DPMM	67
					*****	*****	*****	***	***	***	*****				
485	* $_{93}\text{Np}^{238}$	$\sigma_{n,\bar{g}}$		II	Th-	1				10		BNW	Leonard	DPMM	67
491	$_{94}\text{Pu}^{238}$	$\sigma_{n,\bar{g}}$		III		1-	10			10		AI	Alter	DRDT	69
					*****	*****	*****	***	***	***	*****				
513	$_{94}\text{Pu}^{239}$	Fis Prod Y	of Cs^{137}	II	Th			1				BET	Bayard	DNR	67
					*****	*****	*****	***	***	***	*****				
538	$_{94}\text{Pu}^{242}$	$\sigma_{n,\bar{g}}$		I	Th	to	7	3-			20	BNW	Leonard	DPMM	67
541	$_{95}\text{Am}^{241}$	Total		II	Th			2-3				BNW	Leonard	DPMM	69

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
570	$^{96}\text{Gm}^{248}$	$\sigma_{n,\bar{f}}$		I	Th-	10				10		SRL	Dessauer	DPMM	69
571	$^{97}\text{Bk}^{249}$	Total		I	Th-	10					20	SRL	Dessauer	DPMM	67
572	$^{97}\text{Bk}^{249}$	$\sigma_{n,\bar{g}}$		I	Th-	10				10		SRL	Dessauer	DPMM	69
574	$^{98}\text{Cf}^{250}$	Total		I	Th-	10					20	SRL	Dessauer	DPMM	67
575	$^{98}\text{Cf}^{250}$	$\sigma_{n,f}$		I	Th-	10				10		SRL	Dessauer	DPMM	67
576	$^{98}\text{Cf}^{250}$	$\sigma_{n,\bar{g}}$		I	Th-	10				10		SRL	Dessauer	DPMM	69
					*****	*****	*****	***	***	***	*****				
577	$^{98}\text{Cf}^{251}$	$\sigma_{n,\bar{g}}$		I	Th-	10				10		SRL	Dessauer	DPMM	67
					*****	*****	*****	***	***	***	*****				
582	$^{98}\text{Cf}^{252}$	$\sigma_{n,\bar{g}}$		I	Th-	10				10		SRL	Dessauer	DPMM	67
					*****	*****	*****	***	***	***	*****				
583	* $^{98}\text{Cf}^{253}$	$\sigma_{n,\bar{g}}$		II	Th-	10					20	SRL	Dessauer	DPMM	67

SECTION V.

TABLE 5.H

DPR

Division of Physical Research, John M. Teem, Director

Phone: 301-973-5565

USAEC, Washington, D. C. 20545

Contact: George A. Kolstad, Assistant Director for Physics and Mathematics Programs

Phone: 301-973-3613

W. A. Wallenmeyer, Assistant Director, High-Energy Physics Programs

Phone: 301-973-3624



REQ #	TARGET # Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	OPG	
1	^1_1H	Elastic	$\sigma(\theta_n)$	I			*	2				NDC	Caswell	DPR	72
8	^3_2He	$\sigma_{n,p}$		II		10-	3	1				GGA	Nordheim	DRDT	69
12	^6_3Li	Elastic	$\sigma(\theta_n)$	I		1-100		1-	5			NDC	Caswell	DPR	69
18	^6_3Li	$\sigma_{n,\alpha}$		I		1-	3	1				ANL	Avery	DRDT	69
43	^7_3Li	$\sigma_{\alpha,n}$		II			4-6	2				NDC	Caswell	DPR	69
51	$^{10}_5\text{B}$	Total		II		10-	1	1				NDC	Caswell	DPR	69
52	$^{10}_5\text{B}$	Elastic	$\sigma(\theta_n)$	II		1-100		1-	5			NDC	Caswell	DPR	69
53	$^{10}_5\text{B}$	$\sigma_{n,\alpha}$		I		1-	10	1-	5			ANL	Avery	DRDT	69
54	$^{10}_5\text{B}$	$\sigma_{n,\alpha}(\theta_n)$	$E_n = 480 \text{ keV}$	I		1-	10	1-	5			ANL	Avery	DRDT	69
392	$^{186}_{76}\text{Os}$	$\sigma_{n,\alpha}$		III		1-100			4-9			ORNL	Macklin	DPR	70
393	$^{187}_{76}\text{Os}$	$\sigma_{n,\alpha}$		III		1-100			4-9			ORNL	Macklin	DPR	70
394	$^{197}_{79}\text{Au}$	$\sigma_{n,\alpha}$		II	.5	1*		1				BET	Bayard	DNR	67
442	$^{235}_{92}\text{U}$	$\sigma_{n,f}$		I		10-	15	1				LASL	Hansen	DMA	66
501	$^{239}_{94}\text{Pu}$	$\sigma_{n,f}$		I	1	to	10	2-	5			ANL	Avery	DRDT	69
579	$^{252}_{98}\text{Cf}$	Ther		I				.25				NDC	Caswell	DPR	69
581	$^{252}_{98}\text{Cf}$	Fis Spect	$P(E_n)$	I				1				BET	Bayard	DNK	72

REQ #	TARGET			REACTION TYPE QUANTITY : VARIABLE	PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
	*	Z	A			keV	MeV	GeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
630		6	C	$\sigma_{p,kny}$	$\sigma(\theta_n, E_n)$	I	~50					25	ORNL	Alsmiller	DPR	66
631		6	C	$\sigma_{p,kny}$	$\sigma(\theta_n, E_n)$	II	600-	2				25	ORNL	Alsmiller	DPR	66
637		8	O	$\sigma_{p,kny}$	$\sigma(\theta_n, E_n)$	I	~50					25	ORNL	Alsmiller	DPR	66
638		8	O	$\sigma_{p,kny}$	$\sigma(\theta_n, E_n)$	II	600-	2				25	ORNL	Alsmiller	DPR	66
639		8	O	$\sigma_{\alpha, k\pi^{\pm}y}$	$\sigma(\theta_{\pi}, E_{\pi})$	II		1-2				25	ORNL	Alsmiller	DPR	66
646		13	Al	$\sigma_{p,kny}$	$\sigma(\theta_n, E_n)$	I	600-	2				25	ORNL	Alsmiller	DPR	66
647		13	Al	$\sigma_{p,kny}$	$\sigma(\theta_n, E_n)$	I		~10, 30				25	ORNL	Alsmiller	DPR	66
648		13	Al	$\sigma_{p,kpy}$	$\sigma(\theta_p, E_p)$	II	~2000,	~10, 30				25	ORNL	Alsmiller	DPR	66
649		13	Al	$\sigma_{\alpha,kny}$	$\sigma(\theta_n, E_n)$	II	100-	1				25	ORNL	Alsmiller	DPR	66
653		27	Co	$\sigma_{p,kny}$	$\sigma(\theta_n, E_n)$	I	600-	2				25	ORNL	Alsmiller	DPR	66
654		27	Co	$\sigma_{p,kny}$	$\sigma(\theta_n, E_n)$	I		~10, 30				25	ORNL	Alsmiller	DPR	66
655		27	Co	$\sigma_{p,kpy}$	$\sigma(\theta_p, E_p)$	II	~2000,	~10, 30				25	ORNL	Alsmiller	DPR	66
656		83	Bi	$\sigma_{p,kny}$	$\sigma(\theta_n, E_n)$	I	600-	2				25	ORNL	Alsmiller	DPR	66
657		83	Bi	$\sigma_{p,kny}$	$\sigma(\theta_n, E_n)$	II		~10, 30				25	ORNL	Alsmiller	DPR	66
658		83	Bi	$\sigma_{p,kpy}$	$\sigma(\theta_p, E_p)$	II	~2000,	~10, 30				25	ORNL	Alsmiller	DPR	66

SECTION V.

TABLE 5.I

DRDT

Division of Reactor Development and Technology, Milton Shaw, Director

Phone: 301-973-5203

USAEC, Washington, D. C. 20545

Contacts: William H. Hannum

Phillip B. Hemmig

Reactor Physics Branch

Phone: 301-973-4181

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
2	${}^1_1\text{H}^2$	Elastic		I	1-	1		<2				BET	Bayard	DNR	72
8	${}^3_2\text{He}^3$	$\sigma_{n,p}$		II		10-	3	1				GGA	Nordheim	DRDT	69
18	${}^6_3\text{Li}^6$	$\sigma_{n,\alpha}$		I		1-	3	1				ANL	Avery	DRDT	69
19	${}^6_3\text{Li}^6$	Tot & Prod		II		1-	18			10		HEDL	McElroy	DRDT	69
45	${}^9_4\text{Be}$	Emission	$\sigma(\theta_{n'}, E_{n'})$	II			1.8-5			15		LMFB	Hemmig-AEC	DRDT	62
46	${}^9_4\text{Be}$	$\sigma_{n,\bar{g}}$		II	1-	100				10		IRT	Preskitt	DRDT	69
53	${}^{10}_5\text{B}^{10}$	$\sigma_{n,\alpha}$		I		1-	10	1-	5			ANL	Avery	DRDT	69
54	${}^{10}_5\text{B}^{10}$	$\sigma_{n,\alpha}(\bar{g}_1)$	$E_{\bar{g}} = 180 \text{ keV}$	I		1-	10	1-	5			ANL	Avery	DRDT	69
55	${}^{10}_5\text{B}^{10}$	Tot & Prod		I		1-	18			10		HEDL	McElroy	DRDT	69
57	${}^{12}_6\text{C}$	Elastic	$\sigma(\theta_n)$	III			2-14			10		KAPL	Ehrlich	DNR	62
63	${}^{12}_6\text{C}^{12}$	Polariz.	$P(\theta_n)$	II	*****	*****	*****	***	***	***	*****	KAPL	Ehrlich	DNR	69
69	${}^{16}_8\text{O}$	Elastic	$\sigma(\theta_n)$	II		10-	1		5			IRT	Preskitt	DRDT	69
70	${}^{16}_8\text{O}$	Emission	$\sigma(\theta_{n'}, E_{n'})$	I			8-15			10		AFWL	Enz	DNA	69
78	${}^{19}_9\text{F}$	$\sigma_{n,\bar{g}}$		II		1-	1			10		ORNL	Perry	DRDT	66
81	${}^{23}_{11}\text{Na}$	Total		I		10-	5	3-	5			ORNL	Clifford	DRDT	69
83	${}^{23}_{11}\text{Na}$	Inelastic	$\sigma(E_{n'})$	II			2-10			10		AI	Alter	DRDT	62
85	${}^{23}_{11}\text{Na}$	Absorption		II		1-100					20	GE	Snyder	DRDT	69
86	${}^{23}_{11}\text{Na}$	$\bar{g}_n$ and $\bar{g}_{\bar{g}}$		I		3				10		ANL	Avery	DRDT	62

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
87	$_{11}\text{Na}$	Cap Spect	$P(E_{\bar{e}})$	I		3				10		ANL	Avery	DRDT	72
109	$_{21}\text{Sc}$	$\sigma_{n,\bar{e}}$	Act	II		1=	18			10		HEDL	McElroy	DRDT	69
111	$_{22}\text{Ti}$	Tot $\bar{e}$ Prod	$\sigma(E_{\bar{e}}, E_{\bar{e}})$	I		10=	16				20	ORNL	Clifford	DRDT	69
113	$_{22}\text{Ti}^{k6}$	$\sigma_{n,p}$	Act	II	*****	*****	*****	***	***	***	*****	HEDL	McElroy	DRDT	69
114	$_{22}\text{Ti}^{k7}$	$\sigma_{n,p}$	Act	II	*****	*****	*****	***	***	***	*****	HEDL	McElroy	DRDT	69
115	$_{22}\text{Ti}^{k8}$	$\sigma_{n,p}$	Act	II	*****	*****	*****	***	***	***	*****	HEDL	McElroy	DRDT	69
116	$_{23}\text{V}$	Elastic	$\sigma(E_n)$	III			1,4=10			10		ANL	Avery	DRDT	62
119	$_{23}\text{V}$	Inelastic	$\sigma(E_{n1})$	III			1,5=10				15	ANL	Avery	DRDT	62
125	$_{23}\text{V}$	Absorption		III		1=150				10		ANL	Avery	DRDT	62
128	$_{24}\text{Cr}$	Total		II		1=	20	3				LMFB	Hennig-AEC	DRDT	72
129	$_{24}\text{Cr}$	Elastic	$\sigma(E_n)$	II			2=14		4=9			KAPL	Ehrlich	DNR	69
130	$_{24}\text{Cr}$	Inelastic	$\sigma(E_{n1})$	II		500	=10			10		GE	Snyder	DRDT	66
134	$_{24}\text{Cr}$	$\sigma_{n,\bar{e}}$		II		1=	1			15		GE	Snyder	DRDT	72
140	$_{24}\text{Cr}$	Res Int	Capture	I	,5-	up				10=	15	KAPL	Ehrlich	DNR	69
142	$_{24}\text{Cr}$	Tot $\bar{e}$ Prod	$\sigma(E_{\bar{e}})$	II	*****	*****	*****	***	***	***	*****	BET	Bayard	DNR	69
143	$_{24}\text{Cr}^{53}$	$\bar{G}_{\bar{e}}$		II		1=600			4=9			KAPL	Ehrlich	DNR	69
146	$_{26}\text{Fe}$	Total		I	,001	to	1		5			KAPL	Ehrlich	DNR	72
147	$_{26}\text{Fe}$	Elastic	$\sigma(E_n)$	I			7=14		4=9			KAPL	Ehrlich	DNR	69

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
149	^{26}Fe	Inelastic	$\sigma(E_n)$	I		850-	2		5			GE	Snyder	DRDT	66
155	^{26}Fe	$\sigma_{n,\bar{g}}$		II	.001	to	1			10		KAPL	Ehrlich	DNR	72
					*****	*****	*****	***	***	***	*****				
158	$^{26}\text{Fe}^{56}$	$\sigma_{n,\bar{a}}$		II	Th	to	10			15		GE	Hutchins	DRDT	72
					*****	*****	*****	***	***	***	*****				
162	^{26}Fe	Absorption		I		1-	1.5		5	to	20	ANL	Avery	DRDT	69
164	^{26}Fe	Tot $\bar{g}$ Prod	$\sigma(E_g)$	I	Th	to	10				<15	LMFB	Hemmig=AEC	DRDT	66
166	^{26}Fe	Res Int	Capture	I	.5-	up				10-	15	KAPL	Ehrlich	DNR	69
167	^{26}Fe	$\bar{g}_n$ and $\bar{g}_g$		II		to	1			10		KAPL	Ehrlich	DNR	72
168	^{26}Fe	J, π		III		to	1					KAPL	Ehrlich	DNR	72
					*****	*****	*****	***	***	***	*****				
170	$^{26}\text{Fe}^{54}$	$\sigma_{n,p}$	Act	III			1-18			15		BET	Bayard	DNR	72
					*****	*****	*****	***	***	***	*****				
172	$^{26}\text{Fe}^{57}$	$\bar{g}_n$		I		1-600			4-9			KAPL	Ehrlich	DNR	69
					*****	*****	*****	***	***	***	*****				
173	$^{26}\text{Fe}^{58}$	$\sigma_{n,\bar{g}}$	Act	II	.025	to	15				30	LLL	Howerton	DMA	69
					*****	*****	*****	***	***	***	*****				
174	^{27}Co	Res Par		II	132			1				ANC	Brugger	DRDT	62
175	^{27}Co	$\sigma_{n,\bar{g}}$		II	132			1				ANC	Brugger	DRDT	62
176	^{27}Co	$\sigma_{n,\bar{g}}$	Act	I	.025	to	15				30	LLL	Howerton	DMA	69
					*****	*****	*****	***	***	***	*****				
178	* $^{27}\text{Co}^{58}$	$\sigma_{n,\bar{g}}$		II	Th	to	10			10		BET	Bayard	DNR	72
179	* $^{27}\text{Co}^{58}$	$\sigma_{n,\bar{g}}$		II	Th	to	10			10		BET	Bayard	DNR	72
180	* $^{27}\text{Co}^{58}$	J, π		III		25-	3					KAPL	Ehrlich	DNR	66
					*****	*****	*****	***	***	***	*****				
181	^{28}Ni	Total		II		1-	20	3				ORNL	Clifford	DRDT	72
182	^{28}Ni	Elastic	$\sigma(\theta_n)$	II			1.5-3		5-	10		ANL	Avery	DRDT	72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
183	²⁸ Ni	Inelastic	$\sigma(E_{n'})$	II			1=10			10		GE	Snyder	DRDT	66
187	²⁸ Ni	Absorption		II		1=	1			10		ANL	Avery	DRDT	72
190	²⁸ Ni	$\sigma_{n,\alpha}$		II	Th	to	10			15		GE	Hutchins	DRDT	72
194	²⁸ Ni	Res Int	Capture	I	.5=	up				10=	15	KAPL	Ehrlich	DNR	69
195	²⁸ Ni	Tot $\bar{\sigma}$ Prod	$\sigma(E_{\bar{\sigma}})$	II	Th	to	10			10		BET	Bayard	DNR	66
					*****	*****	*****	***	***	***	*****				
197	²⁸ Ni ⁵⁸	$\sigma_{n,p}$		II			<10		5			BET	Bayard	DNR	72
210	²⁹ Cu ⁶³	$\sigma_{n,\bar{\sigma}}$		II	Th=	1		2=	5			ACRP	Hannum	DRDT	67
211	²⁹ Cu ⁶³	$\sigma_{n,\bar{\sigma}}$	Act	III	.025	to	15				30	LLL	Howerton	DMA	69
212	²⁹ Cu ⁶³	$\sigma_{n,\bar{\sigma}}$	Act	II			>6			10		HEDL	McElroy	DRDT	69
					*****	*****	*****	***	***	***	*****				
214	²⁹ Cu ⁶⁵	$\sigma_{n,\bar{\sigma}}$		II	Th=	1		2=	5			ACRP	Hannum	DRDT	67
223	³⁶ Kr ⁸³	Total		II	.001=	1				10		BET	Bayard	DNR	67
224	³⁶ Kr ⁸³	$\sigma_{n,\bar{\sigma}}$		II	.001=	1				10		BET	Bayard	DNR	67
227	⁴⁰ Zr	Elastic	$\sigma(\theta_n)$	II		200=	1,5			10		KAPL	Ehrlich	DNR	69
231	⁴⁰ Zr	Emission	$\sigma(\theta_{n'}, E_{n'})$	I			2=14			10		KAPL	Ehrlich	DNR	67
232	⁴⁰ Zr	$\sigma_{n,\bar{\sigma}}$		II	Th=	1			5			BNW	Leonard	DPMM	67
234	⁴⁰ Zr	Res Int	Capture	I	.5=	up			5			KAPL	Ehrlich	DNR	69
					*****	*****	*****	***	***	***	*****				
243	⁴⁰ Zr ⁹⁰	Total		I			2=10	3				GE	Snyder	DRDT	72
244	⁴⁰ Zr ⁹⁰	Elastic	$\sigma(\theta_n)$	I		100=	10			10		BET	Bayard	DNR	72
245	⁴⁰ Zr ⁹⁰	Inelastic	$\sigma(\theta_{n'})$	II			14				15	KAPL	Ehrlich	DNR	69
246	⁴⁰ Zr ⁹⁰	Inelastic	$\sigma(E_{n'})$	I			5=15			10		BET	Bayard	DNR	72
247	⁴⁰ Zr ⁹⁰	Emission	$\sigma(\theta_{n'}, E_{n'})$	I			1=15			10		BET	Bayard	DNR	67

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
248	$^{90}_{40}\text{Zr}$	Res Int	Capture	II	.5-	up					20	KAPL	Ehrlich	DNR	69
249	$^{90}_{40}\text{Zr}$	$\bar{G}_n$ and $\bar{G}_g$		II	*	-15				10		KAPL	Ehrlich	DNR	69
250	$^{90}_{40}\text{Zr}$	J, π		II			1.8-5					KAPL	Ehrlich	DNR	69
					*****	*****	*****	***	***	***	*****				
251	$^{91}_{40}\text{Zr}$	Elastic	$\sigma(e_n)$	I		100-	10			10		BET	Bayard	DNR	72
252	$^{91}_{40}\text{Zr}$	Inelastic	$\sigma(e_{n'})$	II			2.5-10			10		BET	Bayard	DNR	72
253	$^{91}_{40}\text{Zr}$	$\sigma_{n,\alpha}$		III			14				30	KAPL	Ehrlich	DNR	69
254	$^{91}_{40}\text{Zr}$	Res Int	Capture	I	.5	up			5			KAPL	Ehrlich	DNR	69
255	$^{91}_{40}\text{Zr}$	$\bar{G}_n$ and $\bar{G}_g$		I	*	-10				10		KAPL	Ehrlich	DNR	69
256	$^{91}_{40}\text{Zr}$	J, π		II			1-4					KAPL	Ehrlich	DNR	69
					*****	*****	*****	***	***	***	*****				
257	$^{92}_{40}\text{Zr}$	Elastic	$\sigma(e_n)$	I		100-	10			10		BET	Bayard	DNR	72
258	$^{92}_{40}\text{Zr}$	Inelastic	$\sigma(e_{n'})$	II			14				15	KAPL	Ehrlich	DNR	69
259	$^{92}_{40}\text{Zr}$	Inelastic	$\sigma(E_{n'})$	I			2.5-10			10		BET	Bayard	DNR	72
260	$^{92}_{40}\text{Zr}$	Res Int	Capture	II	.5-	up					20	KAPL	Ehrlich	DNR	69
261	$^{92}_{40}\text{Zr}$	$\bar{G}_n$ and $\bar{G}_g$		I	*	15				10		KAPL	Ehrlich	DNR	69
262	$^{92}_{40}\text{Zr}$	J, π		II			1-4					KAPL	Ehrlich	DNR	69
					*****	*****	*****	***	***	***	*****				
263	$^{94}_{40}\text{Zr}$	Elastic	$\sigma(e_n)$	I	.5	to	10			10		BET	Bayard	DNR	67
264	$^{94}_{40}\text{Zr}$	Inelastic	$\sigma(e_{n'})$	II			14			15		KAPL	Ehrlich	DNR	67
265	$^{94}_{40}\text{Zr}$	$\bar{G}_n$ and $\bar{G}_g$		II	*	-15				10		KAPL	Ehrlich	DNR	69
266	$^{94}_{40}\text{Zr}$	J, π		II		950-	4					KAPL	Ehrlich	DNR	69
					*****	*****	*****	***	***	***	*****				
267	* $^{95}_{40}\text{Zr}$	$\sigma_{n,\bar{g}}$		II	.5-	10				10-	20	BET	Bayard	DNR	67
					*****	*****	*****	***	***	***	*****				
268	$^{96}_{40}\text{Zr}$	Elastic	$\sigma(e_n)$	I		100-	10			10		BET	Bayard	DNR	72
269	$^{96}_{40}\text{Zr}$	$\sigma_{n,\bar{g}}$		II	Th				5			KAPL	Ehrlich	DNR	69

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
276	$_{41}\text{Nb}$	$\sigma_{n,\bar{g}}$		II		1-100				10		AI	Alter	DRDT	62
288	* $_{41}\text{Nb}^{95}$	$\sigma_{n,\bar{g}}$		I	Th						20	KAPL	Ehrlich	DNR	67
289	$_{42}\text{Mo}$	Inelastic	$\sigma(E_{n1})$	III			1.5-3				20	ANL	Avery	DRDT	72
294	$_{42}\text{Mo}$	$\sigma_{n,\bar{g}}$		III		1=	1			10		ACRP	Hannum	DRDT	72
305	$_{45}\text{Rh}$	$\sigma_{n,\bar{g}}$		II	.5=	1				10		KAPL	Ehrlich	DNR	67
306	* $_{45}\text{Rh}^{105}$	$\sigma_{n,\bar{g}}$		II	.001-1					10		GE	Snyder	DRDT	67
307	* $_{46}\text{Pd}^{107}$	$\sigma_{n,\bar{g}}$		II	.001-	10				10		BET	Bayard	DNR	67
308	$_{47}\text{Ag}^{109}$	$\sigma_{n,\bar{g}}$		II	.001-1					10		GE	Snyder	DRDT	67
309	* $_{52}\text{Te}^{127}$	$\sigma_{n,\bar{g}}$		II	.001-1						20	KAPL	Ehrlich	DNR	67
310	* $_{52}\text{Te}^{132}$	$\sigma_{n,\bar{g}}$		II	.001-1						20	BET	Bayard	DNR	67
311	* $_{53}\text{I}^{133}$	$\sigma_{n,\bar{g}}$		II	.001-	1					20	BET	Bayard	DNR	67
312	$_{54}\text{Xe}^{131}$	$\sigma_{n,\bar{g}}$		II	.001-	1				10		BET	Bayard	DNR	67
313	* $_{54}\text{Xe}^{133}$	$\sigma_{n,\bar{g}}$		II	Th					10		GE	Snyder	DRDT	67
314	* $_{54}\text{Xe}^{135}$	$\sigma_{n,\bar{g}}$		II	.001-2					5		GGA	Nordheim	DRDT	67
315	* $_{54}\text{Xe}^{135}$	Tot $\bar{g}$ Prod	$\sigma(E_{\bar{g}})$	II	Th					10=	20	KAPL	Ehrlich	DNR	67

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
316	55Cs	$\sigma_{n,\bar{g}}$		I	.001-1					10		GE	Snyder	DRDT	67
317	55Cs	$\sigma_{n,\bar{g}}$		I	.5-	1				10		GE	Snyder	DRDT	67
318	60Nd ¹⁴³	$\sigma_{n,\bar{g}}$		I	.001-	1				10		BET	Bayard	DNR	67
					*****	*****	*****	***	***	***	*****				
319	60Nd ¹⁴⁵	$\sigma_{n,\bar{g}}$		I	.001-	1				10		BET	Bayard	DNR	67
					*****	*****	*****	***	***	***	*****				
320	* 60Nd ¹⁴⁷	$\sigma_{n,\bar{g}}$		I	.001-	1			5	to	20	KAPL	Ehrlich	DNR	67
321	* 61Pm ¹⁴⁷	$\sigma_{n,\bar{g}}$		I	.001-	1				10		BET	Bayard	DNR	67
					*****	*****	*****	***	***	***	*****				
322	* 61Pm ¹⁴⁸	$\sigma_{n,\bar{g}}$		I	.001-	1				10		BET	Bayard	DNR	67
323	* 61Pm ¹⁴⁸	$\sigma_{n,\bar{g}}$		I	.001-1					10		BET	Bayard	DNR	67
					*****	*****	*****	***	***	***	*****				
324	* 61Pm ¹⁴⁹	$\sigma_{n,\bar{g}}$		I	.001-	1					20	BET	Bayard	DNR	67
					*****	*****	*****	***	***	***	*****				
325	* 61Pm ¹⁵¹	$\sigma_{n,\bar{g}}$		II	.001-	1				10		BET	Bayard	DNR	67
326	62Sm ¹⁵⁰	$\sigma_{n,\bar{g}}$		I	.001-	1		2-	5			BET	Bayard	DNR	67
					*****	*****	*****	***	***	***	*****				
327	* 62Sm ¹⁵¹	$\sigma_{n,\bar{g}}$		I	.001-	1			5			BET	Bayard	DNR	67
					*****	*****	*****	***	***	***	*****				
328	62Sm ¹⁵²	$\sigma_{n,\bar{g}}$		II	.001-	1				10		BET	Bayard	DNR	67
					*****	*****	*****	***	***	***	*****				
329	* 62Sm ¹⁵³	$\sigma_{n,\bar{g}}$		II	.001-	1					20	BET	Bayard	DNR	67
339	63Eu ¹⁵³	$\sigma_{n,\bar{g}}$		II	.001-	1		2-	5			GE	Snyder	DRDT	67

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
340	* ${}^{63}\text{Eu}^{154}$	$\sigma_{n,\bar{g}}$		II	.001-	1				10		BET	Bayard	DNR	67
					*****	*****	*****	***	***	***	*****				
342	* ${}^{63}\text{Eu}^{155}$	$\sigma_{n,\bar{g}}$		II	.001-	1				10		BET	Bayard	DNR	67
343	${}^{64}\text{Gd}$	Elastic	$\sigma(\theta_n)$	I			1.5-10			10		GE	Snyder	DRDT	67
344	${}^{64}\text{Gd}$	Emission	$\sigma(\theta_n, E_n)$	I			1.5-10			15		GE	Snyder	DRDT	67
347	${}^{64}\text{Gd}$	Res Int	Capture	I	.5-	up			5			GE	Snyder	DRDT	69
					*****	*****	*****	***	***	***	*****				
348	${}^{64}\text{Gd}^{155}$	$\sigma_{n,\bar{g}}$		I	.5-	1			5			GE	Snyder	DRDT	67
349	${}^{64}\text{Gd}^{155}$	Res Int	Capture	I	.5-	up			5			GE	Snyder	DRDT	69
350	${}^{64}\text{Gd}^{155}$	$\bar{G}_n$ and $\bar{G}_K$		I	*-	.5				10		GE	Snyder	DRDT	69
					*****	*****	*****	***	***	***	*****				
351	${}^{64}\text{Gd}^{156}$	$\sigma_{n,\bar{g}}$		I	.001-	1			5			GE	Snyder	DRDT	67
352	${}^{64}\text{Gd}^{156}$	Res Int	Capture	I	.5-	up			5			GE	Snyder	DRDT	69
353	${}^{64}\text{Gd}^{156}$	$\bar{G}_n$ and $\bar{G}_K$		I	*-	2			5			GE	Snyder	DRDT	69
					*****	*****	*****	***	***	***	*****				
354	${}^{64}\text{Gd}^{157}$	$\sigma_{n,\bar{g}}$		I	.5-	1			5			GE	Snyder	DRDT	67
355	${}^{64}\text{Gd}^{157}$	Res Int	Capture	I	.5-	up			5			GE	Snyder	DRDT	69
356	${}^{64}\text{Gd}^{157}$	$\bar{G}_n$ and $\bar{G}_K$		I	*-	1				10		GE	Snyder	DRDT	69
					*****	*****	*****	***	***	***	*****				
371	${}^{72}\text{Hf}$	$\sigma_{n,\bar{g}}$		II	200-	50					20	BET	Bayard	DNR	62
					*****	*****	*****	***	***	***	*****				
372	${}^{72}\text{Hf}^{174}$	$\sigma_{n,\bar{g}}$		I	.001-	5				10-	20	KAPL	Ehrlich	DNR	66
					*****	*****	*****	***	***	***	*****				
373	${}^{72}\text{Hf}^{176}$	$\sigma_{n,\bar{g}}$		I	.001-	5				10-	40	BET	Bayard	DNR	62
					*****	*****	*****	***	***	***	*****				
374	${}^{72}\text{Hf}^{177}$	$\sigma_{n,\bar{g}}$		I	.001-	5			4	to	20	BET	Bayard	DNR	62

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	Lab	PERSON	ORG	
375	^{178}Hf	$\sigma_{n,\bar{g}}$		I	.001-	5		3-	-	to	20	BET	Hayard	DNR	62
					*****	*****	*****	***	***	***	*****				
376	^{179}Hf	$\sigma_{n,\bar{g}}$		I	.001-	5			5	to	20	BET	Hayard	DNR	62
					*****	*****	*****	***	***	***	*****				
377	^{180}Hf	$\sigma_{n,\bar{g}}$		I	.001-	5			4	to	20	BET	Hayard	DNR	67
379	^{182}Ta	$\sigma_{n,\bar{g}}$		I		1-	10		5-	10		AI	Alter	DRDT	69
381	^{182}W	Emission	$\sigma(\theta_{n_1}, E_{n_1})$	I			4-14			10		AFWL	Enz	DNA	69
383	^{183}W	Tot $\bar{g}$ Prod	$\sigma(\theta_{\bar{g}}, E_{\bar{g}})$	I		100-	16				20	ORNL	Clifford	DRDT	63
					*****	*****	*****	***	***	***	*****				
386	^{182}W	$\sigma_{n,\bar{g}}$		I		1-	10			10		AI	Alter	DRDT	69
					*****	*****	*****	***	***	***	*****				
387	^{183}W	$\sigma_{n,\bar{g}}$		I		1-	10			10		AI	Alter	DRDT	69
					*****	*****	*****	***	***	***	*****				
388	^{184}W	$\sigma_{n,\bar{g}}$		I		10-	10			10		AI	Alter	DRDT	69
					*****	*****	*****	***	***	***	*****				
391	^{186}W	$\sigma_{n,\bar{g}}$		I		10-	10			10		AI	Alter	DRDT	69
396	^{208}Pb	Emission	$\sigma(\theta_{n_1}, E_{n_1})$	II			3-15			10		NEL	Eccleshall	DNA	69
401	^{90}Th	Elastic	$\sigma(\theta_n)$	III			1-5			10		ANL	Avery	DRDT	72
402	^{90}Th	Inelastic	$\sigma(E_{n_1})$	III			1-4		5			ANL	Avery	DRDT	72
403	^{90}Th	$\sigma_{n,2n}$		I			Ths=10			10		GE	Snyder	DRDT	67
404	^{90}Th	$\sigma_{n,\bar{g}}$		I	.5-	2			5-	10		BET	Hayard	DNR	62
409	^{231}Pa	$\sigma_{n,\bar{g}}$		II	Th	to	10			10		GE	Snyder	DRDT	69

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
410	* 91 Pa ²³³	$\sigma_{n,\bar{g}}$		II	.001-2				5			IRT	Preskitt	DRDT	67
411	92 U ²³³	Inelastic	$\sigma(E_{n'})$	III		40-	7			10-	20	ANL	Avery	DRDT	67
413	92 U ²³³	$\sigma_{n,2n}$		II			Ths=15			10		LASL	Barr	DMA	67
414	92 U ²³³	$\sigma_{n,f}$		I	.001-	1		.5-	5			BET	Bayard	DNR	62
415	92 U ²³³	$\sigma_{n,f}$		III		1-30			5			ANL	Avery	DRDT	62
416	92 U ²³³	Fis Ratio	wrt U ²³⁵	I		10-	15	1				LASL	Hansen	DMA	67
417	92 U ²³³	Nu Bar		I	.001-	30		.25-	2			BET	Bayard	DNR	69
418	92 U ²³³	Nu Bar		II		30-	3	1-3				BET	Bayard	DNR	69
419	92 U ²³³	Alpha		I	.001-	1		2-	8			BET	Bayard	DNR	62
420	92 U ²³³	Alpha		II		1-	3			10-	20	ANL	Avery	DRDT	62
422	92 U ²³³	Res Par		II	Th-	5				10-	30	ANL	Avery	DRDT	67
423	92 U ²³³	Cap Spect	P(E _n)	II	.01-15						15	BET	Bayard	DNR	67
425	92 U ²³³	Fis Prod Y	of Xe ¹³⁵	II	Th			3				BET	Bayard	DNR	67
426	92 U ²³³	Fis Prod Y	of Cs ¹³⁷	II	Th			1				BET	Bayard	DNR	67
427	92 U ²³³	Fis Prod Y	of Nd ¹⁴⁷	II	Th			3				BET	Bayard	DNR	67
428	92 U ²³³	Fis Prod Y	of Sm ¹⁴⁹	II	Th			3				BET	Bayard	DNR	67

431	92 U ²³⁴	$\sigma_{n,\bar{g}}$		II	.001	to	10	3	to	10		AI	Alter	DRDT	69

433	92 U ²³⁵	Elastic	$\sigma(E_n)$	II			1-5				20	ANL	Avery	DRDT	69
434	92 U ²³⁵	Inelastic	$\sigma(E_{n'})$	II		50-	6			10		ANL	Avery	DRDT	69
439	92 U ²³⁵	$\sigma_{n,f}$		II	1-	1		3				GE	Snyder	DRDT	69
440	92 U ²³⁵	$\sigma_{n,f}$		II	1,10	1,10	1,10	3				KAPL	Ehrlich	DNR	69
441	92 U ²³⁵	$\sigma_{n,f}$		I		1-	14	1-2				GE	Snyder	DRDT	69
443	92 U ²³⁵	$\sigma_{n,f}$ Ratio	wrt H, B ¹⁰	I		1-	14	1				ANL	Avery	DRDT	69
444	92 U ²³⁵	Eta		II	Th-	50		.5-	2			ANL	Avery	DRDT	67

REQ #	TARGET # Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
445	92U ²³⁵	Alpha		II	.001	to	7		5-	10		ANL	Avery	DRDT	69
447	92U ²³⁵	Nu Bar		I	Th=	to	3	1				ANL	Avery	DRDT	69
448	92U ²³⁵	Fis n Y	P(E _{n'})	II	Th	to	3		5			ANL	Avery	DRDT	69
450	92U ²³⁵	Delayd n Y	P(E _{n'})	II	Th					15		KAPL	Ehrlich	DNR	69
454	92U ²³⁵	Res Par		I	Th=200					10		ANL	Avery	DRDT	69
455	92U ²³⁵	Fis Prod Y	of Xe ¹³⁵	II	Th			3				BET	Bayard	DNR	67
456	92U ²³⁵	Fis Prod Y	of Cs ¹³⁷	II	Th			1				BET	Bayard	DNR	67
457	92U ²³⁵	Fis Prod Y	of Sm ¹⁴⁹	II	Th			3				BET	Bayard	DNR	67
458	92U ²³⁵	Fis Prod Y	of Nd ¹⁴⁷	II	Th			3				BET	Bayard	DNR	67
					*****	*****	*****	***	***	***	*****				
462	92U ²³⁶	σ _{n,γ}		I	Th=	1				10		GE	Snyder	DRDT	69
					*****	*****	*****	***	***	***	*****				
465	92U ²³⁸	Elastic	σ(E _{n'})	I		1-	10		5-	10		ANL	Avery	DRDT	69
466	92U ²³⁸	Inelastic	σ(E _{n'})	I		100-	10		5			ANL	Avery	DRDT	69
468	92U ²³⁸	σ _{n,2n}		II			Ths=10			10		GE	Snyder	DRDT	72
471	92U ²³⁸	Fis Ratio	wrt Pu ²³⁹	I		500-	14	2-	4			LMFB	Hemmig-AEC	DRDT	69
472	92U ²³⁸	Nu Bar		I			1=10	1				ANL	Avery		69
474	92U ²³⁸	Delayd n Y	P(E _{n'})	I	Th	to	5		5			LMFB	Hemmig-AEC	DRDT	72
475	92U ²³⁸	σ _{n,γ}		I	500	to	10	2	to	10		AI	Alter	DRDT	69
477	92U ²³⁸	Tot σ Prod	σ(E _{n'} , E _{n'})	II	.001	to	10			10		LMFB	Hemmig-AEC	DRDT	72
478	92U ²³⁸	σ _{n,γ} wrt σ _{n,f}	Pu ²³⁹	I		10-	10	1.5	-7			ANL	Avery	DRDT	69
480	92U ²³⁸	Res Par		I		*				10		AI	Alter	DRDT	69
															--
481	93Np ²³⁷	σ _{n,2n}		II			Ths=15			10		SRL	Dessauer	DPMM	67
484	93Np ²³⁷	σ _{n,γ}		I	.001-	1		3	to	10		BNW	Leonard	DPMM	67
															--
488	94Pu ²³⁸	σ _{n,f}		III			1-10			10		AI	Alter	DRDT	72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACOURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
491	94Pu^{238}	$\sigma_{n,\bar{e}}$		III		1-	10			10		AI	Alter	DRDT	69
					*****	*****	*****	***	***	***	*****				
495	94Pu^{239}	Elastic	$\sigma(E_n)$	II			1=3			10		ANL	Avery	DRDT	69
496	94Pu^{239}	Inelastic	$\sigma(E_{n'})$	I		10-	10				20	KAPL	Ehrlich	DNR	72
498	94Pu^{239}	$\sigma_{n,2n}$		I			Th=15			10		LASL	Barr	DMA	67
500	94Pu^{239}	$\sigma_{n,f}$		I	Th-	1			1			GE	Snyder	DRDT	72
501	94Pu^{239}	$\sigma_{n,f}$		I	1	to	10	2=	5			ANL	Avery	DRDT	69
502	94Pu^{239}	Fis Ratio	wrt U^{235}	I		10-	14	2				LMFB	Hennig=AFC	DRDT	72
503	94Pu^{239}	Nu Bar		I	Th	to	10	41*				AI	Alter	DRDT	66
504	94Pu^{239}	Delayd n Y	$P(E_{n'})$	II	Th	to	5		5			ANL	Avery	DRDT	69
506	94Pu^{239}	Eta		I	Th=1			1				GE	Snyder	DRDT	67
507	94Pu^{239}	Alpha		I	100	to	10	4	to	10		ANL	Avery	DRDT	69
511	94Pu^{239}	Res Par		II	Th=50					10		ANL	Avery	DRDT	69
512	94Pu^{239}	Fis Prod Y	of Xe^{135}	II	Th			3				BET	Bayard	DNR	67
513	94Pu^{239}	Fis Prod Y	of Cs^{137}	II	Th			1				BET	Bayard	DNR	67
515	94Pu^{239}	Fis Prod Y	of Sm^{149}	II	Th			3				BET	Bayard	DNR	67
					*****	*****	*****	***	***	***	*****				
516	94Pu^{240}	Inelastic		II			1.5-10				20	GE	Snyder	DRDT	72
517	94Pu^{240}	$\sigma_{n,f}$		II		500-	10		5			GE	Snyder	DRDT	72
518	94Pu^{240}	Fis Ratio	wrt U^{235}	III		1-100			5			ACRP	Hannum	DRDT	72
519	94Pu^{240}	Nu Bar		II		Th=	10	3				ANL	Avery	DRDT	72
521	94Pu^{240}	$\sigma_{n,\bar{e}}$		I	Th=100			3				GE	Snyder	DRDT	67
522	94Pu^{240}	$\sigma_{n,\bar{e}}$		I	500-	150			5			ANL	Avery	DRDT	69
524	94Pu^{240}	Res Par		II	100-	5				10		ANL	Avery	DRDT	69
					*****	*****	*****	***	***	***	*****				
526	94Pu^{241}	$\sigma_{n,f}$		I	Th=	30		3	to	10		ANL	Avery	DRDT	69
528	94Pu^{241}	Nu Bar		II			1-10		6			ANL	Avery	DRDT	72

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
530	94Pu^{241}	$\sigma_{n,\bar{g}}$		I	Th=	30		3				GE	Snyder	DRDT	67
531	94Pu^{241}	Alpha		II		1=	2				20	GE	Snyder	DRDT	69
532	94Pu^{241}	Res Par		II	Thr=	.4			5	to	20	ANL	Avery	DRDT	72
					*****	*****	*****	***	***	***	*****				
535	94Pu^{242}	Nu Bar		II		500=	10		5			LMfB	Hemmig-AEC	DRDT	69
538	94Pu^{242}	$\sigma_{n,\bar{g}}$		I	Th	to	7	3=			20	BNW	Leonard	DPMM	67
543	95Am^{241}	$\sigma_{n,\bar{g}}$		I	Th=	1				10		SRL	Dessauer	DPMM	67
					*****	*****	*****	***	***	***	*****				
547	95Am^{242}	$\sigma_{n,\bar{g}}$		II	Th	to	10			15		GE	Hutchins	DRDT	72
					*****	*****	*****	***	***	***	*****				
549	95Am^{243}	$\sigma_{n,\bar{g}}$		II	Thr	to	10			15		GE	Snyder	DRDT	72
557	96Cm^{244}	$\sigma_{n,\bar{g}}$		II		10=	10			10		GE	Snyder	DRDT	67
579	98Cf^{252}	Nu Bar		I				.25				NDC	Caswell	DPR	69
580	98Cf^{252}	Nu Bar		I				<1				AI	Alter	DRDT	72
581	98Cf^{252}	Fis Spect	$P(E_{n'})$	I				1				BET	Bayard	DNR	72

SECTION V.

TABLE 5.J

DSNS

Division of Space Nuclear Systems, David S. Gabriel, Director

Phone: 301-973-3027

USAEC, Washington, D. C. 20545

Contacts set up at AGC and at WAL along with the following in the DSNS Division

Charles P. MaCallum

Donald S. Beard

} Phone: 301-973-4558

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
11	${}^3_3\text{Li}$	Tot $\bar{g}$ Prod	$\sigma(E_{\bar{g}})$	II		258±10				15*	1	SNPO	Fleishman	DSNS	69
97	${}^{13}_{13}\text{Al}$	Cap Spect	$P(E_{\bar{g}})$	I	Th					10		SNPO	Fleishman	DSNS	69
98	${}^{13}_{13}\text{Al}$	Tot $\bar{g}$ Prod	$\sigma(E_{\bar{g}})$	II		5±200				15*		SNPO	Fleishman	DSNS	69
110	${}^{22}_{22}\text{Ti}$	Tot $\bar{g}$ Prod	$\sigma(E_{\bar{g}})$	II		1±100				15*		SNPO	Fleishman	DSNS	69
141	${}^{24}_{24}\text{Cr}$	Tot $\bar{g}$ Prod	$\sigma(E_{\bar{g}})$	I	500-	20				15*		SNPO	Fleishman	DSNS	69
145	${}^{25}_{25}\text{Mn}$	Tot $\bar{g}$ Prod	$\sigma(E_{\bar{g}})$	I	300-	120				15*		SNPO	Fleishman	DSNS	69
163	${}^{26}_{26}\text{Fe}$	Tot $\bar{g}$ Prod	$\sigma(E_{\bar{g}})$	II		1-650				15*		SNPO	Fleishman	DSNS	69
177	${}^{27}_{27}\text{Co}$	Tot $\bar{g}$ Prod	$\sigma(E_{\bar{g}})$	I	100-	100				15*		SNPO	Fleishman	DSNS	69
196	${}^{28}_{28}\text{Ni}$	Tot $\bar{g}$ Prod	$\sigma(E_{\bar{g}})$	II		12-340				15*		SNPO	Fleishman	DSNS	69
209	${}^{29}_{29}\text{Cu}$	Tot $\bar{g}$ Prod	$\sigma(E_{\bar{g}})$	II	200-	50				15*		SNPO	Fleishman	DSNS	69
215	${}^{30}_{30}\text{Zn}$	Cap Spect	$P(E_{\bar{g}})$	I	Th					10		SNPO	Fleishman	DSNS	69
216	${}^{30}_{30}\text{Zn}$	Tot $\bar{g}$ Prod	$\sigma(E_{\bar{g}})$	I	200-	25				15*		SNPO	Fleishman	DSNS	69
231	${}^{40}_{40}\text{Zr}$	Emission	$\sigma(\theta_{n_1}, E_{n_1})$	I			2±14			10		KAPL	Ehrlich	DNR	67
237	${}^{40}_{40}\text{Zr}$	Cap Spect	$P(E_{\bar{g}})$	I	Th					10		SNPO	Fleishman	DSNS	69
240	${}^{40}_{40}\text{Zr}$	Tot $\bar{g}$ Prod	$\sigma(E_{\bar{g}})$	II	100-	20				15*		SNPO	Fleishman	DSNS	69
272	${}^{41}_{41}\text{Nb}$	Emission	$\sigma(\theta_{n_1}, E_{n_1})$	I			1.5-15			10		LASL	Streetman	DSNS	69

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DSNS

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REQ #	TARGET			REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
	*	Z	A	QUANTITY	VARIABLE		eV	keV	MeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
280		41	Nb	Cap Spect	$P(E_{\gamma})$	I	Th					10		SNPO	Fleishman	DSNS	69
283		41	Nb	Tot $\bar{\epsilon}$ Prod	$\sigma(E_{\gamma})$	II	30-	75				15*		SNPO	Fleishman	DSNS	69
293		42	Mo	Emission	$\sigma(\theta_{n_1}, E_{n_1})$	II			1.5-15			10		LASL	Streetman	DSNS	69
298		42	Mo	Cap Spect	$P(E_{\gamma})$	I	Th					10		SNPO	Fleishman	DSNS	69
302		42	Mo	Tot $\bar{\epsilon}$ Prod	$\sigma(E_{\gamma})$	I	10-	9				15*		SNPO	Fleishman	DSNS	69
378		73	Ta	Emission	$\sigma(\theta_{n_1}, E_{n_1})$	III			1.5-15			10		LASL	Streetman	DSNS	69
380		73	Ta	Tot $\bar{\epsilon}$ Prod	$\sigma(E_{\gamma})$	I	4-	1.4				15*		SNPO	Fleishman	DSNS	69
381		74	W	Emission	$\sigma(\theta_{n_1}, E_{n_1})$	I			4-14			10		AFWL	Enz	DNA	69
382		74	W	Tot $\bar{\epsilon}$ Prod	$\sigma(E_{\gamma})$	I	2-	2.5				15*		SNPO	Fleishman	DSNS	69
398		82	Pb	Tot $\bar{\epsilon}$ Prod	$\sigma(E_{\gamma})$	II	80-	800				15*		SNPO	Fleishman	DSNS	69
446		92	U^{235}	$\sigma_{n,f} + \sigma_{n,\bar{\epsilon}}$	at 77°K	II	Th-	1		3-	5			SNPO	Fleishman	DSNS	69

SECTION V.

TABLE 5.K

NASA

National Aeronautics and Space Administration

REQ #	TARGET * Z A	REACTION TYPE		PRI OR.	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		keV	MeV	GeV	1-3	4-9	≥15	>15	LAB	PERSON	ORG	
620	${}^4_2\text{He}$	$\sigma_{p,x}$	$\sigma(E_x)$	II		25-100				10*		GSFC	Reames	NASA	67
621	${}^4_2\text{He}$	$\sigma_{p,x}$	$\sigma(E_x)$	II		300=	.6			10*		GSFC	Reames	NASA	67
622	${}^4_2\text{He}$	$\sigma_{\alpha,x}$	$\sigma(E_x)$	II		25-600				10*		GSFC	Reames	NASA	67
623	${}^{6-}_3\text{Li}$	Tot p Reac		III		25-600				10*		GSFC	Reames	NASA	67
					*****	*****	*****	***	***	***	*****				
624	${}^7_3\text{Li}$	Tot p Reac		III		25-600				10*		GSFC	Reames	NASA	67
625	${}^7_3\text{Li}$	$\sigma_{p,x}$		II		25-600				10*		GSFC	Reames	NASA	67
626	${}^7_4\text{Be}$	σ_{p,Li^6}		II		25-600					est,*	GSFC	Reames	NASA	67
					*****	*****	*****	***	***	***	*****				
627	${}^9_4\text{Be}$	Tot p Reac		III		25-600				10*		GSFC	Reames	NASA	67
628	${}^{10}_5\text{B}$	$\sigma_{p,x}$		II		25-600				10*		GSFC	Reames	NASA	67
					*****	*****	*****	***	***	***	*****				
629	${}^{11}_5\text{B}$	$\sigma_{p,x}$		II		25-600				10*		GSFC	Reames	NASA	67
630	${}^{12}_6\text{C}$	$\sigma_{p,kny}$	$\sigma(\theta_{n'}, E_{n'})$	I		~50					25	HASL	O'Brien	DHER	67
631	${}^{12}_6\text{C}$	$\sigma_{p,kny}$	$\sigma(\theta_{n'}, E_{n'})$	II		600=	2				25	HASL	O'Brien	DBER	66
					*****	*****	*****	***	***	***	*****				
632	${}^{12}_6\text{C}$	$\sigma_{p,x}$		II		25=	1			10*		GSFC	Reames	NASA	67
633	${}^{12}_6\text{C}$	$\sigma_{\alpha,x}$		I		25=	1,2			10*		GSFC	Reames	NASA	69
					*****	*****	*****	***	***	***	*****				
634	${}^{13}_6\text{C}$	$\sigma_{p,x}$		I		25-600				10*		GSFC	Reames	NASA	67
635	${}^{14}_7\text{N}$	$\sigma_{p,x}$		II		25-600				10*		GSFC	Reames	NASA	67
					*****	*****	*****	***	***	***	*****				
636	${}^{15}_7\text{N}$	$\sigma_{p,x}$		II		25-600				10*		GSFC	Reames	NASA	67

REQ #	TARGET * Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		keV	MeV	GeV	1-3	4-9	15	>15	LAB	PERSON	ORG	
637	8_0	$\sigma_{p,kny}$	$\sigma(\theta_{n'}, E_{n'})$	I		~50					25	HASL	O'Brien	DBER	66
638	8_0	$\sigma_{p,kny}$	$\sigma(\theta_{n'}, E_{n'})$	II		600-	2				25	HASL	O'Brien	DBER	66
639	8_0	$\sigma_{\alpha, k\pi^+y}$	$\sigma(\theta_{\pi}, E_{\pi})$	II			1-2				25	HASL	O'Brien	DBER	66
					*****	*****	*****	***	***	***	*****				
640	$^{16}_8$	$\sigma_{p,x}$		I		25-600					10*	GSFC	Reames	NASA	67
641	$^{16}_8$	$\sigma_{p,x}$		I		25-600					10*	GSFC	Reames	NASA	67
642	$^{16}_8$	$\sigma_{\alpha, x}$		I		25-	1, 2				10*	GSFC	Reames	NASA	69
					*****	*****	*****	***	***	***	*****				
643	$^{18}_8$	$\sigma_{p,x}$		I		25-600					10*	GSFC	Reames	NASA	67
644	$^{20}_{10}Ne$	$\sigma_{p, A=19}$		I		25-600					10	GSFC	Reames	NASA	67
645	$^{24}_{12}Mg$	$\sigma_{p,x}$		II		25-600					10*	GSFC	Reames	NASA	67
646	$^{13}_{13}Al$	$\sigma_{p,kny}$	$\sigma(\theta_{n'}, E_{n'})$	I		600-	2				25	HASL	O'Brien	DBER	66
647	$^{13}_{13}Al$	$\sigma_{p,kny}$	$\sigma(\theta_{n'}, E_{n'})$	I			~10, 30				25	HASL	O'Brien	DBER	66
648	$^{13}_{13}Al$	$\sigma_{p,kpv}$	$\sigma(\theta_{p'}, E_{p'})$	II		~2000,	~10, 30				25	HASL	O'Brien	DBER	66
649	$^{13}_{13}Al$	$\sigma_{\alpha, kny}$	$\sigma(\theta_{n'}, E_{n'})$	II		100-	1				25	HASL	O'Brien	DBER	66
650	$^{40}_{20}Ca$	$\sigma_{p,x}$		III		25-600					10*	GSFC	Reames	NASA	67
651	$^{56}_{26}Fe$	$\sigma_{p,x}$		II		25-600					10*	GSFC	Reames	NASA	67
652	$^{56}_{26}Fe$	$\sigma_{p,x}$		I		25-600					10*	GSFC	Reames	NASA	67
653	$^{27}_{27}Co$	$\sigma_{p,kny}$	$\sigma(\theta_{n'}, E_{n'})$	I		600-	2				25	HASL	O'Brien	DBER	66
654	$^{27}_{27}Co$	$\sigma_{p,kny}$	$\sigma(\theta_{n'}, E_{n'})$	I			~10, 30				25	HASL	O'Brien	DBER	66
655	$^{27}_{27}Co$	$\sigma_{p,kpv}$	$\sigma(\theta_{p'}, E_{p'})$	II		~2000,	~10, 30				25	HASL	O'Brien	DBER	66

REQ #	TARGET # Z A	REACTION TYPE		PRI OR,	INCIDENT ENERGY			PERCENT ACCURACY				REQUESTER			YR
		QUANTITY	VARIABLE		keV	MeV	GeV	1-3	4-9	≤15	>15	LAB	PERSON	ORG	
656	83 ^{B1}	$J_{p,kny}$	$\sigma(\theta_n, E_n)$	I		600-	2				25	HASL	O'Brien	DBER	66
657	83 ^{B1}	$\sigma_{p,kny}$	$\sigma(\theta_n, E_n)$	II			~10,30				25	HASL	O'Brien	DBER	66
658	83 ^{B1}	$\sigma_{p,kpy}$	$\sigma(\theta_p, E_p)$	II		~2000,	~10,30				25	HASL	O'Brien	DBER	66

LIST OF REQUESTERS*

LAB	NAME	SPONSORING AND/OR REVIEWING AGENCY	FULL NAME OF CONTACT AND PHONE NUMBER	COMPLETE ADDRESS
AC	Greenhow	DNA	Charles R. Greenhow	Nuclear Effects Department , AEROSPACE CORPORATION
005	01	205	Phone:	P. O. Box 1308 San Bernadino, California 92401
ACRP	Hannum	DRDT	W. H. Hannum Chairman, ACRP	Division of Reactor Development & Tech. Reactor Physics Branch
010	01	135	Phone: 301-973-4181	U. S. Atomic Energy Commission Washington, D. C. 20545
AGC	Koebberling	DSNS	Karl O. Koebberling	Aerojet-General Corporation
015	01	165	Phone: 916-449-2000 Ask for: 355-3539	P. O. Box 15847 Sacramento, California 95813
AFIT	Dooley	DNA	John A. Dooley	Air Force Institute of Technology
020	01	201	Phone: 513-257-7266	Wright Patterson Air Force Base Space Systems Division Ohio 45433
AFWL	Enz	DNA	Major Richard Enz	USAF (SRUGT)
025	01	205	Phone: 505-247-1711 Ext-3636	Department of the Air Force Air Force Weapons Laboratory Kirtland Air Force Base New Mexico 87117
AI	Alter	DRDT	Harry Alter	Atomics International
030	01	135	Phone: 213-341-1000 Ext-2491 or 2492	P. O. Box 309 Canoga Park, California 91305

* Due to the many name and organizational changes during the past six years, the Laboratories are no longer listed alphabetically. The numbers which appear under the laboratory, name, and agency are those stored in the computer. Searches are therefore made on the numerical indices.

LAB	NAME	SPONSORING AND/OR REVIEWING AGENCY	FULL NAME OF CONTACT AND PHONE NUMBER	COMPLETE ADDRESS
ANL	Avery	DRDT	Robert Avery	Argonne National Laboratory 9700 S. Cass Ave. Argonne, Illinois 60439
035	01	135	Phone: 312-739-2275	
BET	Bayard	DNR	R. T. Bayard	Westinghouse Electric Company Bettis Atomic Power Lab P. O. Box 79 West Mifflin, Pennsylvania 15122
040	01	185	Phone: 412-462-0234	
BNL	Kouts	DNMS	Herbert J. Kouts	Brookhaven National Laboratory Upton, New York 11973
045	05	155	Phone: 516-924-7796	
DNA	Kaul	DNA	Captain Dean Kaul	HQ, Defense Nuclear Agency Department of Defense Washington, D. C. 20305
055	03	205	Phone: 202-694-5395	
GDFW	Western	DNA	G. T. Western	Nuclear Radiation Transport and Safety General Dynamics Fort Worth Division P. O. Box 748 Fort Worth, Texas 76101
060	01	201	Phone: 817-334-3011 Ask for: 732-4811 Ext-2895 or 2000	
			Others: Ernest Jones H. R. Dvorak	
GE	Snyder	DRDT	Thoma Snyder	General Electric Company Nuclear Energy Division Mail Code 581 175 Curtner Avenue San Jose, California 95125
065	01	135	Phone: 408-286-2525 Ask for: 297-3000 Ext-2404 or 2292	
GE	Hutchins	DRDT	Bruce Hutchins	General Electric Company BRDO 310 De Guigne Drive Sunnyvale, California 94086
065	02	135	Phone: 408-275-7011 Ask for: 297-3000 Ext- 330	

<u>LAB</u>	<u>NAME</u>	<u>SPONSORING AND/OR REVIEWING AGENCY</u>	<u>FULL NAME OF CONTACT AND PHONE NUMBER</u>	<u>COMPLETE ADDRESS</u>
IRT	Bramblett	DNMS	Richard L. Bramblett	Intelcom Rad Tech
070	04	155	Phone: 714-293-5000 Ask for: 453-1000 Ext-17351	Technical Applications Department P. O. Box 80817 San Diego, California 92138
IRT	Preskitt	DRDT	C. A. Preskitt	Intelcom Rad Tech
070	01	135	Phone: 714-293-5000 Ask for: 453-1000 Ext- 278	Technical Applications Department P. O. Box 80817 San Diego, California 92138
GSFC	Reames	NASA	D. V. Reames	Goodard Space Flight Center
075	01	301	Phone: 301-982-4917	Greenbelt, Maryland 20771
HASL	O'Brien	DBER	Keran O'Brien	Health and Safety Laboratory
080	01	105	Phone: 212-620-3632	Radiation Physics Division U. S. Atomic Energy Commission 376 Hudson Street New York, New York 10014
ANC	Brugger	DRDT	Robert M. Brugger	Aerojet Nuclear Corporation
085	01	135	Phone: 208-526-4387]	P. O. Box 1845 Idaho Falls, Idaho 83401
ANC	Heath	DNMS	Russell Heath	Aerojet Nuclear Corporation
085	05	155	Phone: 208-526-4447	P. O. Box 1845 Idaho Falls, Idaho 83401
KAPL	Ehrlich	DNR	Richard Ehrlich	Knolls Atomic Power Laboratory
090	01	185	Phone: 518-393-4312	P. O. Box 1072 Schenectady, New York 12301

LAB	NAME	SPONSORING AND/OR REVIEWING AGENCY	FULL NAME OR CONTACT AND PHONE NUMBER	COMPLETE ADDRESS
LASL	Various	DMA	Michael S. Moore (Contact) Phone: 505-667-5951	Los Alamos Scientific Laboratory P. O. Box 1663 Los Alamos, New Mexico 87544
100	Barr 12 Bell 14 Bennett 16 Biggers 18 Cowan 19 Diven 20 Hansen 24 Moore 26 Motz 28 Walton 40	DMA 115 DMA 115 DMA 115 DMA 115 DMA 115 DMA 115 DMA 115 DMA 115 DMA 115 DNMS 155	Donald W. Barr - 505-667-5328 George I. Bell - 505-667-4401 Elbert W. Bennett - 505-667-4143 Wendell Biggers - 505-667-5201 George A. Cowan - 505-667-5201 Ben C. Diven - 505-667-4504 Gordon Hansen - 505-667-4610 Michael S. Moore - 505-667-5951 Henry T. Motz - 505-667-4117 Roddy B. Walton - 505-667-6141	
LMFB	Hemmig - AEC	DRDT	Philip B. Hemmig	Division of Reactor Development & Tec U. S. Atomic Energy Commission Washington, D. C. 20545
105	01	135	Phone: 301-973-4181	
LRC	Westfall	DSNS	Robert M. Westfall	Reactor Section, Nuclear Systems Div. National Aeronautics and Space Admin.
110	01	165	Phone: 216-433-400 Ext- 394	Lewis Research Center 21000 Brookpark Road Cleveland, Ohio 44135
LLL	Howerton	DMA	Robert J. Howerton	Lawrence Livermore Laboratory P. O. Box 808 Livermore, California 94550
115	02	115	Phone: 415-447-3127	
NASA	Reetz	NASA	A. Reetz	National Aeronautics and Space Administration Headquarters Washington, D. C. 20546
120	12	301	Phone:	
NBS	Caswell	DPR	Randall S. Caswell	National Bureau of Standards Washington, D. C. 20234
125	01	145	Phone: 301-921-2551 or 2234	

LAB	NAME	SPONSORING AND/OR REVIEWING AGENCY	FULL NAME OF CONTACT AND PHONE NUMBER	COMPLETE ADDRESS
NDC	Caswell	DPR	Randall S. Caswell	National Bureau of Standards Washington, D. C. 20234
130	02	145	Phone: 301-921-2551 or 2234	
NEL	Eccleshall	DNA	Donald Eccleshall	Deputy Chief, Nuclear Effects Laboratory U. S. Army Ballistic Research Lab. Aberdeen Proving Ground Maryland 21005
135	01	205	Phone: 301-597-3311 Ask for: 676-1000	
ORNL	Maienschein	DNA	F. C. Maienschein	Oak Ridge National Laboratory P. O. Box X Oak Ridge, Tennessee 37830
145	05	205	Phone: 615-483-6601	
ORNL	Alsmiller	DPR	R. G. Alsmiller	Oak Ridge National Laboratory P. O. Box X Oak Ridge, Tennessee 37830
145	09	144	Phone: 615-483-1126	
ORNL	Perry	DRDT	A. M. Perry	Oak Ridge National Laboratory P. O. Box X Oak Ridge, Tennessee 37830
145	01	135	Phone: 615-483-5640	
ORNL	Clifford	DRDT	C. E. Clifford	Oak Ridge National Laboratory P. O. Box X Oak Ridge, Tennessee 37830
145	02	135	Phone: 615-483-6881	
ORNL	Macklin	DPR	R. L. Macklin	Oak Ridge National Laboratory P. O. Box X Oak Ridge, Tennessee 37830
145	04	145	Phone: 615-483-1967	
BNW	Leonard	DPMM	Bowen R. Leonard, Jr.	Battelle Northwest P. O. Box 999 Richland, Washington 99352
150	01	125	Phone: 509-942-7411 Ask for: 946-2558	
HEDL	McElroy	DRDT	W. N. McElroy	Hanford Engineering Development Lab. Westinghouse Hanford Company P. O. Box 1970 Richland, Washington 99352
150	02	135	Phone: 509-942-3791	

<u>LAB</u>	<u>NAME</u>	<u>SPONSORING AND/OR REVIEWING AGENCY</u>	<u>FULL NAME OF CONTACT AND PHONE NUMBER</u>	<u>COMPLETE ADDRESS</u>
SNS	McCallum	DSNS	Charles P. McCallum	Division of Space Nuclear Systems U. S. Atomic Energy Commission Washington, D. C. 20545
155	01	165	Phone: 301-973-4558	
SNS	Beard	DSNS	Donald S. Beard	Division of Space Nuclear Systems U. S. Atomic Energy Commission Washington, D. C. 20545
155	02	165	Phone: 301-973-4558	
SNPO	Fleishman	DSNS	Morton R. Fleisch	Space Nuclear Propulsion Office Cleveland Extension NASA 2100 Brookpark Road Cleveland, Ohio 44135
156	01	165	Phone: 216-443-6677	
SRL	Dessauer	DPMM	Gerhard Dessauer	Savannah River Laboratory E. I. du Pont de Nemours and Company Aiken, South Carolina 29801
160	01	125	Phone: 803-642-2195	
WAL	Drawbaugh	DSNS	Donald W. Drawbaugh	Westinghouse Astronuclear Laboratory P. O. Box 10864 Pittsburgh, Pennsylvania 15236
165	01	165	Phone: 412-384-6520	
WARD	Pitterle	DRDT	Thomas A. Pitterle	Westinghouse Electric Corporation Advanced Reactor Division Waltz Mill Site, P. O. Box 158 Madison, Pennsylvania 15663
170	01	135	Phone: 412-722-5338	