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Neutron Production from (a,n) Reactions and Spontaneous Fission in ThO<sub>2</sub>, UO<sub>2</sub>, and (U,Pu)O<sub>2</sub> Fuels

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# Neutron Production from (a,n) Reactions and Spontaneous Fission in ThO<sub>2</sub>, UO<sub>2</sub>, and (U,Pu)O<sub>2</sub> Fuels

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# NEUTRON PRODUCTION FROM $(\alpha, n)$ REACTIONS AND SPONTANEOUS FISSION IN ThO<sub>2</sub>, UO<sub>2</sub>, AND $(U, Pu)O_2$ FUELS

by

R. T. Perry and W. B. Wilson

#### ABSTRACT

Available alpha-particle stopping cross-section and  $17, 180(\alpha, n)$  cross-section data were adjusted, fitted, and used in calculating the thick-target neutron production function for alpha particles below 10 MeV in oxide fuels. The spent UO<sub>2</sub> function produced was folded with actinide decay spectra to determine ( $\alpha, n$ ) neutron production by each of 89 actinides. Spontaneous-fission (SF) neutron production for 40 actinides was calculated as the product of  $\overline{\nu}(SF)$  and SF branching-fraction values accumulated or estimated from available data. These contributions and total neutron production in spent UO<sub>2</sub> fuel are tabulated and, when combined with any calculated inventory, describe the spent UO<sub>2</sub> neutron source. All data are tabulated and methodology is described to permit easy extension to specialized problems.

### I. INTRODUCTION

Neutron sources are present in reactor fuel from the spontaneous-fission (SF) decay of actinide nuclides and from the interaction of their decay alpha particles with low- and medium-Z nuclides in  $(\alpha,n)$  reactions. The  $(\alpha,n)$  source in oxide fuels is dominated by reactions with <sup>17</sup>0 and <sup>18</sup>0, which are present in NATO in 0.038 and 0.204 atom percent abundancies, respectively.

The probability of neutron production by an alpha particle emitted at energy  $E_{\alpha}$  in the fuel is given by the thick-target neutron production function  $P(E_{\alpha})$ , which we have evaluated for four fuel compositions--clean ThO<sub>2</sub> thermal

reactor fuel, clean and spent UO<sub>2</sub> thermal reactor fuel, and clean (U,Pu)O<sub>2</sub> fast reactor fuel. The ( $\alpha$ ,n) neutron production function has been evaluated at the Hanford Engineering Development Laboratory (HEDL) by Ombrellaro and Johnson for alpha particles in FFTF fuel;<sup>1</sup> however, P(E $_{\alpha}$ ) has not been calculated for the fuels of interest here, and the change in P(E $_{\alpha}$ ) with exposure has not been evaluated. We have employed the methodology and data used in the HEDL work<sup>1</sup> with minor exceptions in data and energy range of calculation.

The equations describing  $(\alpha,n)$  and SF neutron production and the data quantities used in the calculations are given in Sec. II. The available data sources and adjustments made to the data are described in Sec. III. Details of the  $(\alpha,n)$  calculations are briefly discussed in Sec. IV. Resulting  $(\alpha,n)$ , SF, and total neutron production values are given in Sec. V for each of a variety of actinide nuclides produced in reactor fuels.

Selected results of these calculations have been reported previously.<sup>2-5</sup>

#### II. THEORY

The slowing and stopping of alpha particles in a material are described by the material's alpha-particle stopping power,

$$SP(E) = -\frac{dE}{dx} , \qquad (1)$$

which gives the energy-dependent energy loss of alpha particles of energy E per unit path length x.<sup>6</sup> The energy loss of an alpha particle of initial energy  $E_{\alpha}$  in traveling a distance X can be determined from the stopping power as

$$\Delta E = E_{\alpha} - E_{\alpha} = \int_{0}^{X} \left(-\frac{dE}{dx}\right) dx \qquad (2)$$

Similarly, the distance traveled in slowing from E  $_{\alpha}$  to E'  $_{\alpha}$  is

$$X = \int_{E_{\alpha}}^{E^{*}\alpha} \frac{1}{\left(\frac{dE}{dx}\right)} dE = \int_{E^{*}\alpha}^{E_{\alpha}} \frac{1}{\left(-\frac{dE}{dx}\right)} dE \qquad (3)$$

Neutrons may be produced within the material by  $(\alpha, n)$  reactions with nuclide i, which has atom density N<sub>i</sub> and microscopic  $(\alpha, n)$  cross section  $\sigma_i(E)$ . The probability of  $(\alpha, n)$  interaction with nuclide i by an alpha particle of energy E traveling from x to x + dx is

$$N_{i}\sigma_{i}(E)dx = \frac{N_{i}\sigma_{i}(E)dE}{\left(\frac{dE}{dx}\right)}$$
 (4)

The probability of  $(\alpha, n)$  interaction with nuclide i by an alpha particle in lieu of slowing from  $E_{\alpha}$  to E' $_{\alpha}$  is then

$$p_{i}(E_{\alpha}, E'_{\alpha}) = \int_{E_{\alpha}}^{E'_{\alpha}} \frac{N_{i}\sigma_{i}(E)dE}{\left(\frac{dE}{dx}\right)} = \int_{E'_{\alpha}}^{E} \frac{N_{i}\sigma_{i}(E)dE}{\left(-\frac{dE}{dx}\right)} .$$
(5)

The probability of  $(\alpha,n)$  interaction with nuclide i by an alpha particle prior to stopping in the material is given by the thick-target neutron production function

$$P_{i}(E_{\alpha}) = \int_{0}^{E_{\alpha}} \frac{N_{i}\sigma_{i}(E)dE}{\left(-\frac{dE}{dx}\right)}$$
 (6)

In addition to that of the above definition of Eq. (1), a variety of quantities are referred to as "stopping powers" or often alternately "stopping cross sections." These include (typically without explicit regard to sign) the quantities  $\frac{dE}{d\chi} = \frac{dE}{d(\rho x)} = \frac{dE}{\rho dx}, \frac{dE}{Z^2 dx}, \frac{\theta}{\rho} \frac{dE}{dx}$ , and  $\frac{dE}{N dx}$ . Here  $\chi$  is material thickness (mg/cm<sup>2</sup>), Z is atomic number,  $\rho$  is material density (g/cm<sup>3</sup>), and N is the total atom density of the material (atoms/cm<sup>3</sup>). The last quantity is also called the stopping cross section,

$$\varepsilon(E) = -\frac{1}{N} \frac{dE}{dx} , \qquad (7)$$

a notation adopted here. Equations above defining  $\textbf{p}_{i}$  and  $\textbf{P}_{i}$  may now be written in terms of  $\epsilon$  as

$$P_{i}(E_{\alpha}, E'_{\alpha}) = \frac{N_{i}}{N} \int_{E'_{\alpha}}^{E} \alpha \frac{\sigma_{i}(E)}{\varepsilon(E)} dE$$
(8)

and

$$P_{i}(E_{\alpha}) = \frac{N_{i}}{N} \int_{0}^{E_{\alpha}} \frac{\sigma_{i}(E)}{\varepsilon(E)} dE \qquad (9)$$

Note that  $p_i$  and  $P_i$  are related by

$$P_{i}(E_{\alpha}, E'_{\alpha}) = P_{i}(E_{\alpha}) - P_{i}(E'_{\alpha}) \qquad (10)$$

The stopping cross section  $\epsilon(E)$  of a material composed of J elemental constituents may be calculated using the Bragg-Kleeman<sup>10</sup> relationship, which may be written as

$$\varepsilon(E) \simeq \frac{1}{N} \sum_{j=1}^{J} N_{j} \varepsilon_{j}(E) , \qquad (11)$$

where

$$N = \sum_{j=1}^{J} N_{j}$$
 (12)

The accuracy of the approximation of Eq. (11) will be discussed in Sec. III.

A fraction of the decays of nuclide k within the material may be by alphaparticle emission. This fraction  $F_k^{\alpha}$  of alpha decays may occur with the emission of one of L possible alpha-particle energies. The intensity  $f_{k\ell}^{\alpha}$  is the fraction of all decays of nuclide k resulting in an alpha particle of energy  $E_{k\ell}$ , and

$$F_{k}^{\alpha} = \sum_{\ell=1}^{L} f_{k\ell}^{\alpha} .$$
 (13)

The fraction of nuclide k decays resulting in  $(\alpha, n)$  neutron production in a thick-target material containing I nuclides with  $(\alpha, n)$  cross sections is thus

$$R_{k}(\alpha,n) = \sum_{\ell=1}^{L} f_{k\ell}^{\alpha} \sum_{i=1}^{I} P_{i}(E_{k\ell}) \qquad (14)$$

The SF of an actinide nuclide k is accompanied by the emission of an average  $\overline{v}_k$  (SF) neutrons. The SF activity  $A_k^{SF}$  of nuclide k, having atom density  $N_k$ , is

$$A_{k}^{SF} = \lambda_{k}^{SF} N_{k} \qquad (15)$$

Here, 
$$\lambda_{k}^{SF}$$
 is the SF decay constant defined by

$$\lambda_{k}^{SF} = \ln 2/T_{1/2}^{k}(SF) , \qquad (16)$$

where  $T_{1/2}^k$  (SF) is the SF half-life of nuclide k. SF is typically only one of M modes of decay; the total activity due to nuclide k is

$$A_{k} = \lambda_{k} N_{k} = \sum_{m=1}^{M} A_{k}^{m} , \qquad (17)$$

where  $\lambda_k$  is the total decay constant of nuclide k,

$$\lambda_{k} = \sum_{m=1}^{M} \lambda_{k}^{m} = \ell_{n} 2/T_{1/2}^{k} , \qquad (18)$$

and  $T_{1/2}^k$  is the total half-life of nuclide k. The fraction of nuclide k decays by SF is given by the SF branching fraction

$$F_{k}^{SF} = A_{k}^{SF} / A_{k} = \lambda_{k}^{SF} / \lambda_{k} = T_{1/2}^{k} / T_{1/2}^{k} (SF)$$
 (19)

The average number of SF neutrons emitted per decay (by any mode) of nuclide k is then

$$R_{k}(SF) = F_{k}^{SF} \overline{v}_{k}(SF) \qquad (20)$$

The total number of neutrons, on the average, emitted due to  $(\alpha,n)$  reactions and SF is

$$R_{k} = R_{k}(\alpha, n) + R_{k}(SF)$$
 (21)

The total neutron source S from  $(\alpha, n)$  reactions and SF within a material containing K pertinent radionuclides is then

$$S = \sum_{k=1}^{K} \lambda_{k} N_{k} R_{k}$$
(22)

The evaluation of the quantities  $R_k(\alpha,n)$ ,  $R_k(SF)$ , and  $R_k$  for a number of actinide nuclides is described in the following sections.

### III. DATA

The data quantities required to compute the neutron production fractions  $R_k(\alpha,n)$  and  $R_k(SF)$  for each of the four fuels of interest include the following.

- For each major elemental constituent j of the material: N<sub>j</sub>, the atom density; and  $\varepsilon_{i}(E)$ , the alpha-particle stopping cross section.
- For each nuclide i within the material having an  $(\alpha, n)$  cross section: N<sub>i</sub>, the atom density; and  $\sigma_i(E)$ , the microscopic  $(\alpha, n)$  cross section.
- For each nuclide k decaying by alpha decay:  $f_{kl}^{\alpha}$ , the intensity for emission of each L alpha particles; and  $E_{kl}$ , the energy of each of L alpha particles,
- For each nuclide k decaying by SF:  $F_k^{SF}$ , the SF branching fraction; and  $\overline{v_k}$  (SF), the average number of neutrons emitted per SF.

# A. Stopping Cross Section $\epsilon(E)$

Densities of each constituent of each fuel type are given in Table I. The fuel compositon of UO<sub>2</sub> LWR fuel is given for clean and spent conditions for the evaluation of the effect of exposure-dependent fuel composition on stopping cross section  $\varepsilon$ ; here,  $_{41}$ Nb and  $_{59}$ Pr represent the low- and high-mass fission products, respectively. Concentrations of  $_{93}$ Np,  $_{95}$ Am, and  $_{96}$ Cm are given for the spent UO<sub>2</sub> fuel, although the minor contributions to  $\varepsilon$  from these nuclides are included as plutonium. Elements contributing to the material stopping cross sections are thus 0, Nb, Pr, Th, U, and Pu.

A bibliography of experimental and theoretical stopping-power references by Anderson<sup>11</sup> notes that some 900 papers have been published on the subject of ion energy loss in matter. Anderson, noting the observation by Bichsel<sup>12</sup> that stopping powers measured by different groups often did not agree within stated uncertainties, was unable to resolve discrepancies after careful analysis and cautioned that stopping-power data sources should be selected carefully. We have chosen as the major stopping cross-section data source the comprehensive volume edited by Ziegler,<sup>13</sup> which gives tabulated alpha stopping cross-section values and functional fits for elements in the range  $1 \leq Z \leq 92$ .

No values of the alpha-stopping cross section for plutonium were identified, although values for plutonium compounds were found.<sup>7</sup> Northcliffe and Schilling<sup>8</sup> have tabulated values of the stopping power  $dE/d\chi$  for  $Z \leq 92$ . They have shown graphically, for each Z including Z = 94, the energy-dependent ratio  $(dE/d\chi)_Z:(dE/d\chi)_{A_L}$ . In order to form a stopping cross section for plutonium consistent with the data of Ziegler,<sup>13</sup> we have used the stopping power ratio of Ref. 8 in the expression

$$\epsilon_{Pu} = \epsilon_{u} \frac{A_{Pu}}{A_{U}} \left[ (dE/d\chi)_{Pu} : (dE/d\chi)_{A\ell} \frac{(dE/d\chi)_{A\ell}}{(dE/d\chi)_{U}} \right] , \qquad (23)$$

where all quantities enclosed in brackets [] were taken from Ref. 8. Values used and produced in this calculation are given in Table II.

Fourth-degree polynomial functions of the form

$$\ln \varepsilon = C_0 + C_1 \ln E + C_2 \ln^2 E + C_3 \ln^3 E + C_4 \ln^4 E$$
(24)

# TABLE I

# PROPERTIES OF OXIDE FUELS

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	The	rmal Reactor	Fast Reactor Fuel		
	UO <sub>2</sub> Clean	UO <sub>2</sub> Spent	ThO <sub>2</sub> Clean	(U,Pu)02 Clean	
Fuel Density (g/cm <sup>3</sup> )	9.95	9.95	9.17	9.62	
Exposure GWd/t	0	34	0	0	
Atom Densities (atoms/b-cm)					
NAT 80	0.04372	0.04372	0.04184	0.04215	
<sup>1</sup> 6 <sub>0</sub>	0.04361	0.04361	0.04174	0.04205	
<sup>1</sup> 7 <sub>0</sub>	1.6614-5	1.6614-5	1.5899-5	1.6017-5	
<sup>18</sup> 0	8.9189-5	8.9189-5	8.5354-5	8.5986-5	
4 1Nb	0	7.893-4	0	0	
59Pr	0	7.893-4	0	0	
9 0 <sup>Th</sup>	0	0	0.02025	0	
9 2 <sup>U</sup>	0.02186	0.02085	6.724-4	0.01887	
9 3 <sup>N</sup> P	0	1.043-5	0	0	
ց <sub>կ</sub> Рս	0	2.037-4	0	0.002634	
9 5 <b>Am</b>	0	5.692-6	0	0	
9 6 <sup>Cm</sup>	0	1.131-6	0	0	

## TABLE II

DATA OF NORTHCLIFFE AND SCHILLING<sup>a</sup> AND ZIEGLER<sup>b</sup> USED IN CALCULATING THE ALPHA PARTICLE STOPPING CROSS SECTION OF PLUTONIUM

						and a state of the second states of the second states of the second states of the second states of the second s
Ĕα	$(dE/d\chi)_{Pu}$	(MeV/mg	/cm <sup>2</sup> )	$(dE/d\chi)_{Pu}$	eV/(10 <sup>1</sup>	<sup>5</sup> atoms/cm <sup>2</sup> )
MeV	$(dE/d\chi)_{\Lambda q}$	$(dE/d\chi)_{\Lambda}$	$(dE/d\chi)_{II}$	$(dE/d\chi)_{II}$	U(Ziegler)	Pu(Calculated)
	A.L.	A.L.				
0.100	0.150	0.752	0.135	0.837	75.80	63.74
0.320	0.188	1.219	0.243	0.942	139.93	132.48
0.500	0.214	1.317	0.286	0.986	165.64	164.08
0.805	0.235	1.299	0.312	0.978	178.59	175.40
1.281	0.256	1.170	0.307	0.977	166.77	163.72
2.402	0.291	0.904	0.269	0.978	129.15	126.86
4.003	0.322	0.682	0.223	0.982	100.57	99.23
6.404	0.350	0.512	0.183	0.978	78.65	77.29
10.007	0.382	0.379	0.148	0.980	60.67	59.71
16.010	0.418	0.270	0.114	0.991	47.09	46.90
24.016	0.448	0.200	0.090	1.000	37.01	37.18
48.031	0.490	0.118	0.059	0.983	23.64	23.35

Stopping Power Ratios and Values from Northcliffe and Schilling

 $\varepsilon(E)$  Stopping Cross Section

<sup>a</sup>Northcliffe and Schilling, Nucl. Data Tables <u>A7</u>, 233 (1970)

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<sup>b</sup>J. F. Ziegler, <u>Helium Stopping Powers and Ranges in All Elemental Matter</u>, Vol. 4 of The Stopping and Ranges of Ions In Matter Series (Pergamon Press, New York, 1977). were fit to each set of tabulated stopping cross-section values, representing the values within 1% at any energy over the range 0.5 MeV  $\leq E_{\alpha} \leq 10$  MeV. These functional stopping cross sections are shown in Fig. 1. Coefficients of the polynomial functions are given in Table III. Stopping cross sections of the oxide fuels were formed from these component stopping cross-section functions using the Bragg-Kleeman relationship of Eq. (11) and component densities given in Table I.

Stopping cross-section values of UO<sub>2</sub>, ThO<sub>2</sub>, and (U<sub>.8</sub>Pu<sub>.2</sub>)O<sub>2</sub> were computed over the range 2 MeV  $\leq E_{\alpha} \leq 8$  MeV and compared in Table IV with values of  $\epsilon$ converted from experimentally measured values of dE/dx reported by Nitzki and Matzke.<sup>7</sup> The measured and calculated values of  $\epsilon$  agree within 9% over this range, with calculated values generally lower than measured values.

### B. (α, n) Cross Sections

The cross sections for the <sup>17,18</sup>O( $\alpha$ ,n) reactions have been reported over four limited ranges of E<sub> $\alpha$ </sub>, although no single measurement extends over the entire range of our interest. Bair and Willard<sup>14</sup> plotted their measured <sup>18</sup>O( $\alpha$ ,n)<sup>21</sup>Ne cross-section values over the range 2.37 MeV  $\leq E_{\alpha} \leq 5.15$  MeV. Bair and Hass<sup>15</sup> extended the range of these data down to 1.14 MeV and plotted the <sup>17</sup>O( $\alpha$ ,n)<sup>20</sup>Ne cross section over the range 1.31 MeV  $\leq E_{\alpha} \leq 5.31$  MeV. Bair and del Campo<sup>16</sup> later plotted the NATO( $\alpha$ ,n) cross section over the range 3.1 MeV  $\leq E_{\alpha} \leq 8$  MeV and, based on their measured NATO( $\alpha$ ,n) neutron production by alpha particles in the range 4.62 MeV  $\leq E_{\alpha} \leq 4.8$  MeV, recommended that the <sup>17</sup>,<sup>18</sup>O( $\alpha$ ,n) cross sections reported in Refs. 14 and 15 be increased by 35%.

Differential cross sections  $d\sigma(E)/d\Omega$  for  $^{17,18}O(\alpha,n)$  reactions were measured at higher energies by Hansen et al.,  $^{17}$  who fit their measured angular distributions with Legendre polynomial expansions that they integrated to yield total  $\sigma(\alpha,n)$  values. These values were plotted for the range 4.3 MeV  $\leq E_{\alpha} \leq 12.3$  MeV, and smooth curves were plotted approximating each set of data.

Except for cross-section values given by Hansen et al.<sup>17</sup> at 9.8, 11.6, and 12.3 MeV, no data were available in other than graphic form-despite the best efforts of Bair,<sup>18</sup> del Campo,<sup>19</sup> and Hansen<sup>20</sup> to resurrect their numerical data. Data taken from the <sup>17,18</sup>O( $\alpha$ ,n) cross-section curves of Refs. 14 and 15 for the earlier HEDL work<sup>1</sup> were supplied to us.<sup>21</sup> These data were thinned to 744 values of the <sup>17</sup>O( $\alpha$ ,n) cross section and 687 values of the <sup>18</sup>O( $\alpha$ ,n) cross section. Fourth-degree polynomial fits were made to data taken from the



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Fig. 1. Stopping cross sections  $\varepsilon(E_\alpha)$  of 0, Nb, Pr, Th, U, and Pu.

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## TABLE III

Element	Co	C 1	C <sub>2</sub>	С 3	С 4
		-			
0	3.7213	-0.168700	-0.300138	0.0700466	-0.00377296
Ni	4.7872	-0.156294	-0.278932	0.0533399	0.00186590
Pr	4.9321	-0.192312	-0.199561	0.0592391	-0.00940776
Th	5.2027	-0.195369	-0.278809	0.105037	-0.0163945
U	5.1648	-0.161478	-0.279242	0.099232	-0.0146254
Pu	5.1486	-0.171158	-0.272723	0.100975	-0.0160365

# COEFFICIENTS OF POLYNOMIAL FITS TO STOPPING CROSS SECTIONS<sup>a</sup>

 $a_{ln\varepsilon} = C_0 + C_1 lnE + C_2 ln^2 E + C_3 ln^3 E + C_4 ln^4 E$ , E is alpha-particle energy in MeV, 0.5 < E (MeV) < 10.0, and c is stopping cross section in  $eV/(10^{15} \text{ atoms/cm}^2)$ .

## TABLE IV

# COMPARISON OF CALCULATED AND MEASURED ALPHA STOPPING CROSS SECTIONS FOR OXIDE FUELS

	ε(I	E) for ThO	2	ε(H	E) for UC	D <sub>2</sub>	ε(E) 1	for (U <sub>-8</sub> 1	2 .2)0 2
		From Table III		]	From Table III	[ · · ·		From Table III	[
E	From	and Eq.		From	and Eq.	•	From	and Eq.	,
MeV	<u>a</u>	(11)	<u>% Dif</u>	a	·(11)	<u>% Dif</u>	<u>a</u>	(11)	<u>% Dif</u>
2	68.96	69.40	0.6	71.10	68.73	-3.3	72.17	68.55	-5.0
3	59.38	56.27	-5.2	59.91	55.93	-6.6	60.48	55.84	-7.7
4	52.13	48.67	-6.6	51.76	48.13	-7.0	52.05	48.01	-7.8
5	46.46	42.43	-8.7	45.56	42.53	-6.6	45.69	42.43	-7.1
6	41.91	38.20	-8.9	40.69	38.37	-5.7	40.71	38.27	-6.0
7	38.16	34.87	-8.6	36.76	35.10	-4.5	36.71	35.00	-4.7
8	35.03	32.23	-8.0	33.52	32.50	-3.0	33.42	32.41	-3.0

<sup>a</sup>Nitzki and Matzke, Phys. Rev. <u>B8</u>, 1894 (1973).

 $NAT_{O(\alpha,n)}$  cross-section plot of Ref. 16 and to data taken from the  $1^{7,18}O(\alpha,n)$  cross-section plots of Ref. 17. These five cross-section descriptions are shown in Fig. 2.

The  $^{17,18}O(\alpha,n)$  cross sections used in the present calculations were composed of the lower energy data of Refs. 14 and 15 increased by 35% as recommended in Ref. 16 and joined with the adjusted higher energy data of Ref. 17. This adjustment, amounting to a 9.2% reduction, was determined by normalizing the integral of the  $^{NAT}O(\alpha,n)$  cross section formed from the functional fits to  $^{17,18}O(\alpha,n)$  cross sections of Ref. 17 to the integral of the  $^{NAT}O(\alpha,n)$  cross section of Ref. 16 over the range 5.15 MeV  $\leq E_{\alpha} \leq 8$  MeV. The resulting adjusted cross sections are shown in Fig. 3. The adjusted  $^{17}O(\alpha,n)$  cross section is given in Table V, and the adjusted  $^{18}O(\alpha,n)$  cross section is given in Table VI; cross sections are defined there by interpolation points at low energies ( $\leq$ 5 MeV) and by polynomial functions at higher energies.

## C. Alpha-Decay Data

A total of 144 actinide nuclides produced in reactor fuel have been identified,<sup>22</sup> using data of ENDF/B-V and Refs. 23-25. Of these, 89 decay at least partly by alpha decay. Each nuclide has some L different alpha-particle energies with  $1 \leq L \leq 26$  for the data collection used. Alpha-particle energies in the data collection fall in the range 3.71 MeV  $\leq E_{\alpha} \leq 8.78$  MeV. TABLE VII lists the alpha-particle energies and intensities for each nuclide.

# D. Spontaneous-Fission Data

Of the 144 actinide nuclides identified, 40 decay at least partly by spontaneous fission. Values of  $\overline{\nu_p}(SF)$ , the major prompt contribution to  $\overline{\nu}(SF)$ , are given by Manero and Konshin<sup>26</sup> for many of these. These values were used in Fig. 4 to estimate values of  $\overline{\nu_p}(SF)$  for nuclides without data.

Branching fractions  $F^{SF}$ , if not given in a data reference, were constructed from total and SF half-life values  $T_{1/2}(SF)$  using Eq. (19). Values of  $T_{1/2}(SF)$  given as limiting values were used and quoted without qualification. The values of  $\tilde{v}(SF)$ ,  $F^{SF}$ , and R(SF) for each of the 40 nuclides are given in Table VIII.



Fig. 2.  $^{17}$ O,  $^{18}$ O, and NATO ( $\alpha$ ,n) cross-section data.



Fig. 3.  $^{17}$ O and  $^{18}$ O adjusted (a,n) cross sections.

 

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 < ADJUSTED 170 ( $\alpha$ , n) CROSS SECTION

TABLE V

CX(mb) = 0 (assumed), E(MeV) < 1.31, = -126.76 + 89.624E - 9.0873E<sup>2</sup> + 0.647207E<sup>3</sup> - 0.0105365E<sup>4</sup>, 5.3127 ≤ (MeV) ≤ 12.3.

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.

TABLE VIADJUSTED180 (a,n) CROSS SECTION

E(MEV)	CX(MB)	E(MEV)	CX(MB)	E(MEV)	CX(MB)	E(MEV)	CX(MB)	E(MEV)	CX(MB)	E(MEV)	CX(MB)	E(MEV) CX(MB)	E(MEV) CX(Mb)	E(MEV) CX(MB)	E(MEV) UX(MD)
1.1448	0.00	1.5432	.68	1.8707	4.18	2.1957	27.20	2.5100	15.32	2.9240	168.47	3.3100 119.76	3.7240 177.86	4.1944 210.40	4.6848 413.82
1.1482	.07	1.5474	:45	1.8751	1.48	2.2004 2.2048	22.61 10.89	2.5140	17.46	2.9261 2.9281	187.69	3.3180 135.78	3.7401 177.88	4.1984 215.74 4.2064 230.70	4.6888 390.33
1.1553	.07 .05	1.5554	.38	1.8841	.43	2.2097	3.83 2.38	2.5261 2.5301	29.21 37.77	2.9306	190.90	3.3287 164.62	3.7522 192.83	4.2104 246.73	4.7009 305.98
1.1625	.05 .01	1.5637	.23	1.8936	.31 .23	2.2189	1.94	2.5341 2.5381	46.32	2.9356	163.13 142.84	3.3381 157.15	3.7682 209.94	4.2292 316.16	4.7170 275.02
1.1696	0.00	1.5719	.19 .19	1.9019	.23 .22	2.2287	1.62	2.5421	69.82 79.43	2.9406	117.22	5.3502 140.09	3.7750 235.85	4.2426 356.25	4.12-0 210.24
1.1982	.13 0.00	1.5802	. 16 . 16	1.9108	. 18 . 19	2.2383	1.65	2.5542	124.29	2.9457	90.53	3.3622 119.81	3.7964 264.44	4.2587 412.29	4.7411 266.50
1.2055	.01 0.00	1.5885	:13	1.9196	: 19 : 18	2.2478	1.80	2.5636	252.45 191.58	2.9522	54.23 46.76	3.3703 103.80	3.8044 299.69	4.2748 450.75	4.7572 259.85
1.2640	0.00	1.5965	.16	1.9286	. 19 . 18	2.2574	2.55 2.78	2.5743	100.82	2.9642	36.10 30.75	3.3810 90.99 3.3863 81.39	3.8205 349.88	4.2855 424.06	4.7692 223.82
1.2826	0.00	1.6051	.09 .09	1.9377	. 19 .23	2.2669	2.71	2.5864	35.69 25.02	2.9723	26.49 24.35	3.3904 69.65	3.8326 399.02	4.2949 337.58 4.3029 303.41	4.7813 213.15 4.7853 211.03
1.3013	0.00	1.6135	.09	1.9467	1.39	2.2764	1.97	2.5944	20.75 15.42	2.9843	22.23	3.4038 51.52 3.4105 45.12	3.8406 416.11 3.8486 400.10	4.3109 293.81 4.3150 287.41	4.7974 209.97 4.8014 212.11
1.3089	:03	1.6340	.08	1.9556	1.42	2.2859	1.98	2.6024	13.28	2.9964	19.05	3.4185 47.25	3.8527 373.41	4.3230 301.31	4.8054 217.46
1.3201	.43	1.6423	.08	1.9693	:30	2.3002	2.34	2.6185	9.02 1.97	3.0286	16.94	3.4346 64.35	3.8728 314.70	4.3431 364.32	4.8255 242.04
1.3217	. 15	1.6548	:01	1.9783	:27	2.3097	2.73	2.6386	6.90 6.91	3.0446	16.96	3.4453 47.29	3.8848 308.31	4.3592 433.75	4.8389 215.35
1.3353	.01	1.6631	.08	1.9876	.30	2.3195	4.20	2.6547	6.93	3.0567	19.10	3.4587 54.77	3.8969 336.08	4.3753 485.03	4.8577 249.55
1.3466	0.00	1.6841	:07	1.9967	:35	2.3290	9.46	2.6681	10.15	3.0728	21.26	3.4708 66.53	3.9130 357.45	4.3873 521.34	4.8737 438.57
1.3544	0.00	1.6930	.05	2.0055		2.3388	9.71	2.6788	14.43	3.0929	23.42	3.4868 86.85	3.9210 331.84	4.4034 517.09	4.8858 385.20
1.3619	.01	1.7613	.07 .08	2.0148	51	2.3485	6.10	2.6949	25.12	3.1009	27.70	3.4989 114.62	3.9371 273.12	4.4114 487.20	4.8579 302.98
1.3696	.01	1.7096	.09	2.0331	49 58	2.3581	4.23	2.7029	64.65	3,1090	30.91	3.5086 152.01	3.9532 208.01	4.4275 429.56	4.9180 305.14
1.3850	0.00 0.00	1.7228	.07 .09	2.0424	.62	2.3679	3.89	2.7190	245.13	3.1170	36.25 41.59	3.5198 179.78	3.9652 161.03 3.9733 141.82	4.4396 376.18	4.9300 343.59
1.4046	.01 0.00	1.7311	80. 80.	2.0515 2.0561	.63 .68	2.3777 2.3826	3.25	2.7311 2.7351	188.55	3.1291 3.1331	46.95 49.09	3.5311 210.76 3.5331 220.37	3.9813 129.01 3.9853 112.99	4.4516 330.26 4.4597 305.72	4.9582 369.25
1.4122	0.00	1.7398	.13 .07	2.0608	.69 .73	2.3877 2.3926	3.10 3.04	2.7391 2.7431	78.57 56.15	3.1411 3.1492	58.71 68.32	3.5351 237.45	3.9893 105.53	4.4637 272.62	4.9622 361.79
1.4239	.01	1.7483	.08 .09	2.0700	.74 .80	2.3934	4.52	2.7458	43.33	3.1572	76.88 84.36	3.5512 256.70	4.0054 95.93	4.4758 200.02	4.9783 323.35
1.4320	.03	1.7612	.08	2.0791	.95	2.4095	3.47	2.7512	30.52	3.1652	110.00	3.5672 242.82	4.0175 93.81 4.0255 94.89	4.4918 145.57	4.9903 294.53
1.4435	.26	1.7700	.00	2.0930	1.04	2.4376	§.70	2.7713	14.53	3.1813	128.16	3.5833 270.62	4.0456 101.32	4.5160 168.02	5.0104 166.41
1.4516	.24	1.7828	.11	2.1023	1.15	2.4497	7.78	2.7833	10.27	3.1974	147.39	3.5994 312.28	4.0577 121.62	4.5280 317.53	5.0,05 144.00
1.4594	.08	1.7914	.09 .08	2.1117	47	2.4537	14.19	2.7994	11.35	3.2054	147.41	3.6074 319 76	4.0738 172.89	4.5441 419.00	5.0506 137.62
1.4790	.05	1.8004	.09	2.1207	1.97	2.4577	18.47	2.8155	13.51	3.2148	130.34	3.6195 270.65	4.0858 246.59	4.5602 476.68	5.0667 177.15
1.4871 1.4910	.08 .11	1.8087	. 15	2.1300	2.52	2.4648	38.77 94.30	2.8316	16.73	3.2255	120.73	3.6316 233.29 3.6396 222.61	4.0979 312.81 4.1059 323.49	4.5763 413.69 4.5883 426.52	5.0828 288.22 5.0868 381.13
1.4952	. 16 . 19	1.8177	.22 .18	2.1392 2.1441	3.51	2.4708 2.4738	108.18 169.05	2.8436 2.8597	23.15 37.04	3.2376 3.2456	109.00 100.47	3.6436 213.02 3.6517 210.88	4.1140 309.62 4.1220 274.39	4.5950 432.93 4.6017 446.81	5.0989 434.54 5.1069 424.94
1.5031	.26	1.8266	. 19 . 24	2.1488	4.47	2.4754 2.4770	148.77 94.31	2.8637 2.8798	65.88 81.92	3.2497 3.2537	94.07 88.72	3.6597 205.55 3.6631 197.02	4.1260 237.02	4.6084 443.62 4.6124 436.16	5.1123 391.84 5.1176 366.21
1.5111	.51 .68	1.8352	.24	2.1580	5.09 4.87	2.4786	47.32 25.97	2.8838	95.81 104.36	3.2577 3.2617	85.52 83.39	3.6718 197.02 3.6798 194.90	4.1381 192.19	4.6205 439.37	5.1230 347.00 5.1310 353.42
1.5231	1.15	1.8440	.80	2.1673	4.58	2.4818	15.30	2.8999	126.79	3.2698	80.20 79.14	3.6878 193.83	4.1501 185.79	4.6446 430.85	5.1391 367.31
1.5312	1.20	1.8574	7.21	2.1769	4.25	2.4859	9.96	2.9160	148.10	3.2858	82.35	3.7039 187.45	4.1622 192.21	4.6526 427.65	5.1511 332.09
1:3333	:85	1.8663	7:69	2.1002	24.25	2:5019	13.18	2.9200	156.72	3:2979	103.72	3.7200 181.06	4.1823 200.77	4.6727 429.81	

CX(mb) = 0 (assumed), Threshold = 0.85 < E(MeV)<1.14, = -320.68 + 241.227E - 29.6216E<sup>2</sup> + 2.011956E<sup>3</sup> - 0.0511101E<sup>4</sup>, 5.1511 < E(MeV) < 12.3.

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# TABLE VII

ALPHA DECAY SPECTRA OF ACTINIDE NUCLIDES

82-PB-210   ALPHA REF B F MEV. DK FRACTION	83-BI-214 6 Alphas, REF B 8 Mey. DK Fraction	86-RN-218 2 Alphas, Ref B E,MEV. DK FRACTION	88-HA-223 12 ALPHAS, HEF B E,HEV. DR FRACTION	89-AC-227 8 ALPHAS, REF 5 E,MEV. DA FRACTION	90-TH-230 7 ALPHAS, HEF A E,MEV. DX FHACTION
3.7198 1.70000E-08	4.9420 5.25210E-07 5.0234 4.41176E-07 5.1824 1.26050E-06	6.5349 1.30091E-03 7.1331 9.98699E-01	5.2839 I.00000E-03 5.2885 I.30000E-03 5.3399 I.00000E-03	4.715 4.30252E-05 4.7701 1.94308E-04 4.7967 1.12421E-04 4.8656 5.13527E-04	4.2840 5.06746E-08 4.2780 8.01194E-08 4.3720 1.00149E-05 4.4380 3.00448E-04
2 ALPHAS, REF B E,MEV. DK FRACTION	5.2638 1.21849E-05 5.4508 1.13235E-04 5.5121 8.23529E-05	85-AT-219 1 ALPHA , REF B E,MEY. DK FRACTION	5.4347 2.30000E-02 5.4347 2.30000E-02 5.5025 1.00000E-02 5.5396 9.10000E-02	4.8733 8.46626E-04 4.9008 1.52670E-05 4.9416 5.55164E-03 4.6528 6.52318E-03	4.4800 1.20179E-03 4.6210 2.34349E-01 4.6875 7.64136E-01
4.6861 5.20000E-07 84-P0-210 2 ALPHAS, REF B	84-PO-214 2 ALPHAS, REF B E,HEV. DK FRACTION	6.2733 9.70000E-01 86-RN-219 ALPHAS, REF B	5.6073 2.40000E-01 5.7161 5.28900E-01 5.7474 9.10000E-02 5.8517 3.20000E-03	90-TH-227 19 ALPHAS, KEF B	91-PA-230 18 ALPHAS, REF L E,MEV. UN FRACTION
E,HEV. DK FRACTION 4.5168 1.07000E-05 5.3046 9.99989E-01	6.9025 1.00000E-04 7.6873 9.99900E-01 84-P0-215	6.4250 7.49101E-02 6.5310 1.19856E-03	88-RA-224 5 ALPHAS, REF A	5.5862 1.81892E-03 5.6021 1.71767E-03 5.6136 2.22312E-03	4.7653 6.40446E-08 4.7987 9.60672E-09 4.9343 1.28090E-07 4.9726 2.24157E-07
83-BI-211 2 ALPHAS, REF B E.MEV. DK FRACTION	3 ALPHAS, REF B 5,MEV. DK FRACTION 6.9497 2.20000E-04	6.8194 8.09029E-01 86-RN-220	5.0340 3.09945E-05 5.0470 7.19873E-05 5.1610 7.288726-05	5.6686 2.12207E-02 5.6940 1.51576E-02 5.7017 3.63783E-02 5.7097 8.28618E-02	5.0600 1.28090E-07 5.0836 2.24157E-07 5.1190 1.92134E-07 5.1534 1.28090E-07
6.2790 1.59562E-01 6.6233 8.37698E-01	6.9559 3.400005-04 7.3865 9.99440E-01 85-AT-215	5.7490 7.00000E-04	5.4490 4.89914E-02 5.6856 9.50833E-01 89-AC-225	5.7142 4.95150L-02 5.7572 2.02102L-01 5.7630 2.32417L-03 5.7952 3.13258E-03	5.1839 1.60112L-07 5.2173 1.60112L-07 5.2683 1.12078L-06 5.2762 9.60672L-07
84-PU-211 3 ALPHAS, REF B E,MEV. DK FRACTION	2 ALPHAS, HEF E,MEV. DK FRACTION 7.6285 5.00000E-04	87-FR-221 4 ALPHAS, REF B F MFV UK FRACTION	13 ALPHAS, REF B E,MEV. DK FRACTION 5.2871 2.30161E-03	5.8076 1.31366E-02 5.8667 2.42522E-02 5.9103 1.71787E-03 5.9166 7.88197E-03	5.2880 9.60072E-07 5.3008 5.44381E-06 5.3126 4.16291E-06 5.3263 5.76403E-06
6.5694 5.40000E-03 6.8914 5.50000E-03 7.4502 9.89100E-01	84-P0-216 2 ALPHAS, REF A	6.0752 1.36426E-03 6.1275 1.37335E-01 6.2434 1.11236E-02	5.4432 1.50105E-03 5.5539 1.00070E-03 5.5809 1.20084E-02 5.6093 1.20084E-02	5.95999 3.03153E-02 5.9779 2.32417E-01 6.0089 2.93048E-02 6.0383 2.42522E-01	92- U-230
83-51-212 8 ALPHAS, REF B E,MEV. DK FRACTION	5.9850 2.10000E-05 6.7785 9.99979E-01	6.3411 8.49477E-01 86-RN-222 2 ALPHAS, REF B	5.6377 4.35305E-02 5.6824 1.25088E-02 5.7235 3.40238E-02 5.7320 1.01071E-01	90-TH-228 5 ALPHAS, KEF A E,MEV. DK FRACTION	4 ALPHAS, REF B E,MEV. UK FHACTION 5.6622 2:30023E-03
5.3024 3.95857E-07 5.3456 3.59870E-06 5.4849 5.39805E-05 5.6069 3.95857E-03	85-AT-217 4 Alphas, REP B E,MEV. DK FRACTION	E. HEV. DK FRACTION 4.9870 7.80172E-04 5.4898 9.99220E-01	5.7921 9.00630E-02 5.7939 1.80126E-01 5.8043 3.00210E-03 5.8299 5.06855E-01	5.1380 5.00050E-04 5.1770 1.80018E-03 5.2110 3.60036E-03	5.8001 3.8003022-03 5.8176 3.190322-01 5.8886 6.750682-01
5.7684 6.00983E-03 6.0511 2.51549E-01 6.0902 9.78847E-02	6.4846 4.00100E-04 6.6113 1.00025E-04 6.8134 2.50063E-04 7.0677 9.99250E-01	87-FR-222 1 ALPHA , REF B E.MEV. DK FRACTION	88-RA-226 2 Alphas, Ref B E,Mev. DK Fraction	5.4233 7.27073L-01 90-TH-229	19 ALPHAS, NEF A E,NEV. DK FHAUTIUN
84-PO-212 1 ALPHA , REF B E,MEV. DK FRACTION	86-RN-217 1 ALPHA , REF B E.MEV. DK FRACTION	5.7092 1.00000E-03 88-RA-222	4.6017 5.55000E-02 4.7846 9.44500E-01	4.7626 6.36107E-03	4.5660 8.07526E-05 4.6000 1.51411E-04 4.6330 1.00941E-03 4.6440 1.00941E-03
8.7846 1.00000E+00 83-BI-213 2 ALPHAS, REF B	7.7426 1.00000E+00 84-P0-218	2 ALPHAS, REF B E,MEV. DK FRACTION 6.2373 3.10000E-02	89-AC-226 1 ALPHA , REF B E,MEV. DK FRACTION	4.1907 1.202314-02 4.8148 8.48142E-02 4.8390 4.84653E-02 4.8460 5.67447E-01 4.8460 5.67447E-03	4.6820 1.51411E-02 4.7130 1.00941E-02 4.7360 8.47902E-02 4.7360 4.03763E-04
E, MEV. DK FRACTION 5.5508 1.62963E-03 5.8687 2.03704E-02	2 ALPHAS, REF B E,MEV. DK FRACTION 5.1810 1.10000E-05	6.5557 9.69000E-01 87-FR-223 1 ALPHA & REF B	90-TH-226 5 ALPHAS, REF B	4.9017 1.09047E-01 4.6309 1.11066E-03 4.9686 6.46204E-02 4.9795 3.23102E-02	4.8540 1.41317E-02 4.9020 2.01882E-05 4.9340 3.02822E-02 4.9517 2.30145E-01
84-PO-213 2 ALPHAS, REF B E.HEV. DA FRACTION	6.0027 9.999895-01 85-AT-218 3 ALPHAS, REF B	5.3330 4.00000E-05	6.0258 2.00682E-03 6.0414 1.90648E-03 6.0414 1.20648E-03	5.0363 2.42326L-03 5.0492 5.25040E-02 5.0534 1.61551L-02 5.0783 1.00969E-04	4.9760 4.03763E-03 4.9860 1.41317E-02 5.0141 2.56390E-01 5.0297 2.01882E-01
7.6123 3.00000E-05 8.3757 9.99970E-01	E, MEV. DK FRACTION 6.6625 6.40000E-02 6.7045 9.00000E-01 6.7567 3.60000E-02		6.2284 2.30785E-01 6.3375 7.52559E-01		5.0320 2.52352E-02 5.0590 1.11035E-01

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# TABLE VII (cont.)

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# TABLE VII (cont.)

94-PU-244 2 Alphas, Ref A	97-BK-249 7 Alphas, ref a	98-CF-252 5 ALPHAS, REF A	99-ES-254 8 ALPHAS, REF B
E,MEY. DK FRACTION	É, HEV. DK FRACTION	E, HEV. DK FRACTION	E, HEV. DK FRACTION
4.5860 1.93757E-01 4.5890 8.04993E-01	5.0450 1.45291E-00 5.1150 3.92285E-07	5.6160 5.00623E-07 5.8263 1.93541E-05	6.2758 1.61421E-03
96-CH-244	5.3510 3.77756E-07 5.3800 2.67335E-06	0.0757 1.519302-01 6.1183 8 14807E-01	0.3595 2.92575E-02 6.3841 1.31154E-03
E, HEV. DK FRACTION	5.4168 1.00541E-05 5.4373 9.73447E-07	98-CF-253	6.4155 1.71509E-02 6.4283 9.38257E-01
4.9200 8.99767E-07 4.9600 1.99948E-06	98-CF-249	2 ALPHÁS, REF A E,MEV. DK FRACTION	6.4780 2.72397E-03
5.2150 1.19969E-06 5.3130 3.99896E-07	16 ALPHAS, REF A E, HEV. DK FRACTION	5.9210 1.64300E-04	99-ES-254M 7 ALPHAS, REF B
5.5130 3.49909E-05 5.6640 2.19943E-04	5.3510 1.99410E-05	5.9790 2.935708-03	6 2872 7 220565-05
5.8050 7.63802E-01	5.5020 <b>1.38701E-04</b>	28 ALPHAS, REF A	6.2797 2.78071E-04 6.3045 2.51269E-03
96-CH-245	5.6230 1.99410E-04 5.6940 2.99115E-03	5.7300 8.00043E-07	6.3405 6.03046E-05 6.4361 4.69036E-05
E, MEV. DK FRACTION	5.7597 4.78583E-02 5.7840 2.49262E-03	5.9100 2.70015E-07 5.9350 4.00022E-07	6.4791 1.94315E-04 6.5130 1.34010E-04
5.2346 3.20256E-03 5.3038 4.97398E-02	5.8120 8.23562E-01 5.8495 1.39587E-02	5.9440 1.50008E-06 6.0190 1.80010E-06	100-FH-254
5.3620 9.32546E-01 5.4363 4.00320E-04	5.9034 3.19056E-02 5.9462 3.38997E-02	6.0370 2.90016E-06 6.0460 4.00022E-06	3 ALPHAS, REF B 5,MEV. DK FRACTION
5.4087 8.30665E-03 5.5292 5.80464E-03	6.0000 5.98229E-04 6.0720 3.98819E-03	6.1000 3.40018E-05	7.0492 9.00369E-03
96-CH-246	6.1940 2.39292E-02	6.1660 1.50002E-00 6.2110 3.00021E-04	1:1889 8:50349E-01
E, MEV. DK FRACTION	98-CF-250 A ALPHAS, REF A	6.2170 1.50008E-05 6.2300 1.20006E-05	99-ES-255 3 ALPHAS, REF B
5.3430 2.09945E-01 5.3860 7.89793E-01	E.MEV. DK FRACTION	6.2500 4.50024E-04 6.2660 8.00043E-06	E,MEV. DK FRACTION
96-CH-247	5.7367 9.99130E-05 5.8900 2.99739E-03	6.3250 4.00022E-06 6.3540 8.20044E-05	6.2137 2.00000E-03 6.2609 7.84000E-03
7 ALPHAS, REF A E,MEV. DK FRACTION	5.9891 1.61859E-01 6.0308 8.34274E-01	6.4080 1.30007E-04 6.4320 6.10033E-04	6.2996 7.01600E-02
4.8140 4.70000E-02	98-CF-251	6.4980 2.60014E-03	6 ALPHAS, REF B
4.0000 7.10000E-01 4.9410 1.60000E-02 4.9830 2.00000E-02	E, MEV. DK FRACTION	6.5520 7.10038E-03	6,8069 1,10375E-03
5.1450 1.20000E-02 5.2100 5.70000E-02	5.5010 3.04569E-03 5.5660 1.52284E-02	6.5940 7.00038E-03 6.6240 8.00043E-03	6.8915 6.22115E-03 6.9634 5.01706E-02
5.2650 1.38000E-01	5.6030 2.03046E-03 5.6320 4.56853E-02	6.6327 8.98048E-01	6.9829 1.30444E-03 7.0225 9.37186E-01
96-CH-248 2 ALPHAS, REF A	5.6480 3.55330E-02 5.6770 3.53299E-01	98-CF-254 2 ALPHAS, REF B	7.0800 4.01365E-03
E,MEV. DK FRACTION	5.7380 1.01523E-02 5.7620 3.85787E-02	E,MEV. DK FRACTION	1 ALPHA , REF B
5.0780 7.51351E-01	5.8140 4.26396E-02 5.8520 2.781735-01	5.8366 2.57300E-03	6.9152 1.00000E+00
98-CF-248 2 ALPHAS, REF B	5.9430 6.09137E-03 6.0140 1.21827E-01		100-FH-257
E, MEV. DK FRACTION	6.0740 2.74112E-02		5 ALPHAS, REF B E, NEV. DK FRACTION
6.2241 1.80000E-01 6.2663 8.20000E-01			6.3467 3.01811E-03
			6.4410 2.01207E-02 6.5199 9.35614E-01
			6.7572 6.03622E-03

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REFERENCE A: ENDFB/B-V Hefehence 8: Table of Isutupes, seventh edition

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Fig. 4. Values of  $v_p(SF)$ .

# TABLE VIII

NUCLIDE	PROMPT	NU-BAR VALUES DELAYED	с тотаl	SPONTANEOUS FISSION BRANCHING	NEUTRONS PER NUCLIDE DECAY
	2.12		2 14	5 220-12 0	1 14 -12
90-1H-230	2.13	.01	1 92	2 000-12 D	5 75 -12
91-PH-231	1.72	.01	2 14	1 410-11 0	3.73 - 12
90-1H-232	2.130+.200 #	.01	2.14	1.410-11 H	3.02 -11
92- 0-232	1.70	. 01	1.71	9.000-13 C	1.54 -12
92- 0-233	1.75	.01	1.76	1.300-12 C	2.29 -12
92- U-234	1.80	.01	1.81	1.200-11 C	2.17 -11
92- 0-235	1.85	.01	1.00	2.011-09 8	3.74 -09
92- 0-236	1.900+.050 E	.01	1.91	1.200-09 C	2.29 -09
94-PU-236	2.120+.130 E	.01	2.13	8.100-10 0	1.73 -09
93-NP-237	2.04	.01	2.05	2.140-12 H	4.39 -12
92- U-238	2.000+.030 E	.01	2.01	5.450-07 C	1.095-06
94-PU-238	2.210+.130 E	.01	5.55	1.840-09 C	4.08 -09
94-PU-239	2.15	.01	2.16	4.400-12 C	9.37 -12
94-PU-240	2.151+.006 E	.01	2.16	5.000-08 C	1.08 -07
96-(M-240	2.38	.01	2.39	3.860-08 A	9.23 -08
95-AM-241	2.26	.01	2.27	4.100-12 C	9.31 -12
94-PU-242	2.141+.190 E	.01	2.15	5,500-06 C	1.18 -05
95-AM-242M	2.33	.01	2.34	1.600-10 C	3.74 -10
96-CM-242	2.510+.060 E	.01	2.52	6.800-08 C	1.71 -07
95-AM-243	2.41	. 01	2.42	2.200-10 C	5.32 -10
94-PU-244	2.290+.190 H	.01	2.30	1.250-03 C	2.88 -03
96-CM-244	2.681+.011 H	.01	2.69	1.347-06 C	3.62 -06
96-CM-246	3.170+.220 H	.01	3.18	2.614-04 C	8.31 -04
96-CM-248	3.100+.090 H	.01	3.11	8.260-02 C	2.569-01
98-CF-248	3.33	. 01	3.34	2.850-05 A	9.52 -05
97-BK-249	3.590+.160 H	.01	3.60	4.600-10 C	1.66 -09
98-CF-249	3.400+.400 H	3.01	3.41	5.020-09 A	1.71 -08
96-CM-250	3.300+.080 H	.01	3.31	7.000-01 D	2.32 +00
98-CF-250	3.520+.090 H	.01	3.53	3.092-02 C	2.72 -03
98-CF-252	3.756+.012 H	.009 B	3.765+.010 B	3.092-02 C	1.164-01
99-ES-253	3.92	. 01	3.93	8.700-08 C	3.42 -07
98-CF-254	3.890+.050 H	.01	3.890+.050 E	9.969-01 A	3.88 +00
99-ES-254	3.94	.01	3.95	3.020-08 A	1.19 -07
99-ES-254M	3.94	.01	3.95	4.500-08 A	1.78 -07
100-FM-254	3.980+.140 H	3.01	3.96 +.14 F	5.900-04 A	2.34 -03
99-ES-255	3.96	.01	3.97	4.000-05 A	1.59 -04
100-FM-255	3.99	.01	3.73 +.18 F	2.290-07 A	8.54 -07
100-FM-256	4.00	.01	4.01	9.190-01 A	3.69 +00
100-FM-257	4.010+.130 H	3.01	3.85 +.05 6	2.100-03 A	8.09 -03
100-FM-258	4.02	.01	4.03	1.000+00 A	4.03 +00
DATA REFERE A=TABLE OF B=MANERO A	NCES USED ISOTOPES, SE ND KONSHIN, F	EVENTH EDITION TOMIC ENERGY	REV. 10,637-75	6 (1972)	
C=ENDF/B-V					
D=U IORIUZ	JU.K. PRIVATE				
E=C.J.DRTH	HUCL.SCI.ENG	3.43134(19/1)	E (1077)		
F=Y.A.LAZA	PEV, HTOMIC EN	HEREY REV.15,7	2(1977)		
G≖D.C.HDFF ADDITIONAL	REFERENCES SU	ITS.REV.C21963	(1980)		
J.W.BOLDEM	AN, IN NEUTRON	STD. REF.DAT	A, I. <mark>A.</mark> E.A. VI	ENNA (1974)	
J.F.BHLHGN	n EI NE.FFMY3	.KEY.LEII.ED!	140112112		

# SPONTANEOUS-FISSION NEUTRON PRODUCTION BY ACTINDE DECAY

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PPDMPT NU-BAR VALUES GIVEN WITHDUT REFERENCE HAVE BEEN ESTIMATED FROM THE VALUES OF PEFERENCE B. DELAYED NU-BAR VALUES GIVEN WITHDUT REFERENCE HAVE BEEN ARBITRARILY ASSUMED.

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# IV. CALCULATION OF THE THICK-TARGET NEUTRON-PRODUCTION FUNCTION $P_i(E_{\alpha})$

The neutron-production function  $P_i(E_{\alpha})$  defined by Eqs. (6) and (9) gives the contribution from reactions with nuclude i to the probability of neutron production by a decay alpha particle of energy  $E_{\alpha}$  emitted within the material. The POFEAL code calculates values of  $\underline{P}_i$  <u>OF</u> <u>E-ALPHA</u> using the algorithm

$$P(J) = 1.E + 6* \frac{N_{i}}{N} \sum_{j=2}^{J} \frac{\left[\sigma_{i}(j-1)+\sigma_{i}(j)\right]/2}{\left[\epsilon(j-1)+\epsilon(j)\right]/2} [E(j)-E(j-1)] , \qquad (25)$$

where

- $N_{i}$  is the atom density of nuclide i (atoms/cm<sup>3</sup>),
- N is the total atom density  $(atoms/cm^3)$ ,
- Ej is the jth regular energy point at or above the cross-section threshold (MeV),

 $\sigma_i(j)$  is the value of the  $(\alpha, n)$  cross section of nuclide i at  $E_j$  (mb),

 $\epsilon(j)$  is the value of the stopping cross section ( $eV/10^{15}$  atoms/cm<sup>2</sup>),

and the leading quantity of 1 x 10  $^6$  is required because of the units of  $\sigma,\ \varepsilon,$  and E.

The <sup>17</sup>O and <sup>18</sup>O contributions to the ( $\alpha$ ,n) neutron-production rate are given in Tables IX-XII for each of the four fuel compositions given in Table I. Values for the four compositions at any energy differ by less than 4%. The <sup>17</sup>O and <sup>18</sup>O contributions to ( $\alpha$ ,n) neutron production in spent UO<sub>2</sub> fuel are shown in Fig. 5.

#### V. RESULTS

The half-lives, average decay energies, and spent UO<sub>2</sub> fuel neutronproduction values  $R_k(\alpha,n)$ ,  $R_k(SF)$ , and  $R_k$  for each of the actinide nuclides k are given in Table XIII. Values of  $R_k(SF)$  are repeated from Table VIII. Values of  $R_k(\alpha,n)$  were obtained using the alpha spectra data of Table VII and  $P(E_{\alpha})$ values given in Table XI for <sup>17,18</sup>0( $\alpha$ ,n) in spent UO<sub>2</sub> fuel.

# TABLE IX

# <sup>17</sup>, <sup>18</sup>O(α, n) NEUTRON PRODUCTION IN CLEAN ThO<sub>2</sub> FUEL BY ALPHA PARTICLES BELOW 10 MeV

			BRUTHTOMP DEP. ALDUAR	BENALTTOOLS_PLU_AL PHAR	
E.HEV	0-17 0-18 TOTAL	E,MEV 0-17 0-18 TOTAL	E,HEV 0-17 0-18 TOTAL	E,HEV 0-17 0-18 TUTAL	E, HEV 0-17 0-18 TUTAL
<b>E</b> , <b>WEY</b> <b>O</b> .0000 <b>1</b> , <b>1</b> , <b>1</b> , <b>3</b> , <b>1</b> <b>1</b> , <b>1</b> , <b>3</b> , <b>1</b> <b>1</b> , <b>1</b> ,	**REUTRONS_PER-ALPHA* 0-17 0-18 TOTAL 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	Bit and the second se	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	E. MCV 0-17 0-18 TUTAL 6.424 3.01-9 3.43-8 3.733-8 6.489 3.05-9 3.47-8 3.717-8 6.475 3.05-9 3.52-8 3.824-8 6.499 3.13-9 3.56-8 3.817-8 6.574 3.25-9 3.65-8 3.966-8 6.599 3.21-9 3.65-8 3.966-8 6.659 3.22-9 3.65-8 4.061-8 6.669 3.37-9 3.76-8 4.061-8 6.669 3.37-9 3.76-8 4.061-8 6.669 3.37-9 3.76-8 4.061-8 6.669 3.37-9 3.76-8 4.051-8 6.669 3.37-9 3.76-8 4.051-8 6.624 3.77-9 3.86-8 4.255-8 6.6724 3.50-9 3.77-8 4.052-8 6.624 3.76-9 4.03-8 4.255-8 6.6724 3.50-9 3.95-8 4.352-8 6.774 3.55-9 4.03-8 4.552-8 6.6824 3.76-9 4.32-8 4.652-8 6.699 3.85-9 4.35-8 4.950-8 6.052-8 3.65-8 3.25-8 4.950-8 6.924 3.95-9 4.45-8 4.850-8 6.939 3.90-9 4.45-8 4.850-8 6.939 3.95-9 4.45-8 4.850-8 6.939 3.95-9 4.45-8 4.850-8 6.939 3.95-9 4.45-8 4.850-8 6.939 3.95-9 4.45-8 4.950-8 6.949 3.95-9 4.45-8 4.950-8 6.949 3.95-9 4.45-8 4.950-8 6.949 3.95-9 4.45-8 4.950-8 6.954 4.855-8 7.224 4.41-9 4.85-8 5.774-8 7.224 4.41-9 4.85-9 5.784 5.785-8 7.224 4.41-9 4.85-8 5.774-8 7.224 4.41-9 4.85-8 5.774-8 7.224 4.41-9 4.85-8 5.774-8 7.224 4.41-9 4.85-9 5.785-8 7.224 4.85-9 5.724-8 7.224 4.85-9 5.724-8 7.224 4.85-9 5.794-8 7.224 4.85-9 5.795-8 7.224 4.85-9 5.724-8 7.224 4.85-9 5.795-8 7.224 4.85-9 5.724-8 7.224 4.85-9 5.724-8 7.245 4.85-9 5.724-8 7.245 4.85-9 5.724-8 7.245 4.85-9 5.754-8 7.245 4.85-9 5	$\begin{array}{c c c c c c c c c c c c c c c c c c c $
1.236 1.261 1.286 1.309	0.0- 0 2.6-14 2.61-14 0.0- 0 2.6-14 2.61-14 0.0- 0 3.0-14 3.03-14 0.0- 0 3.2-14 3.19-14	2.974 7.0-11 7.7-10 8.42-10 2.999 7.5-11 7.8-10 8.59-10 3.024 8.3-11 7.9-10 8.78-10 3.049 9.5-11 8.1-10 9.01-10	4.774 1.01-9 1.24-8 1.343-0 4.799 1.03-9 1.26-8 1.361-8 4.624 1.04-9 1.28-8 1.360-8 4.824 1.04-9 1.28-8 1.380-8	6.574 3.22-9 3.73-8 4.061-8 6.699 3.29-9 3.73-8 4.061-8 6.649 3.37-9 3.78-8 4.109-8 6.649 3.37-9 3.82-8 4.157-8	8.399 7.05-9 7.47-8 8.173-8 8.424 7.11-9 7.53-8 8.240-8 8.439 7.18-9 7.53-8 8.240-8
1.319 1.324 1.349	1.5-15 5.7-14 5.84-14 2.4-15 8.0-14 8.26-14 4.2-15 9.8-14 1.02-13	3.099 1.2-10 8.3-10 9.52-10 3.124 1.3-10 8.5-10 9.81-10 3.149 1.4-10 8.9-10 1.024-9	4.899 1.09-9 1.35-8 1.457-8 4.924 1.10-9 1.37-8 1.482-8 4.949 1.12-9 1.40-8 1.512-8 4.949 1.12-9 1.40-8 1.512-8	6.699 3.46-9 3.91-8 4.255-8 6.724 3.50-9 3.95-8 4.303-8 6.749 3.54-9 4.00-8 4.353-8 6.774 3.50-9 4.08-8 4.353-8	8.499 7.31-9 7.71-8 8.442-8 8.524 7.37-9 7.77-8 8.510-8 8.549 7.44-9 7.83-8 8.578-8 8.549 7.44-9 7.83-8 8.578-8
1.399	6.2-15 1.0-13 1.07-13 1.0-14 1.0-13 1.13-13 1.2-14 1.1-13 1.19-13 4 8-14 1.1-13 1.19-13	3.174 1.4-10 9.4-10 1.087-9 3.199 1.5-10 1.03-9 1.180-9 3.224 1.6-10 1.11-9 1.269-9 3.244 1.6-10 1.14-9 1.269-9	4.974 1.14-9 1.43-8 1.543-0 4.999 1.17-9 1.45-8 1.570-8 5.024 1.20-9 1.47-8 1.587-8 5.089 1 22-9 1.47-8 1.587-8	6.774 3.59-9 4.09-8 4.402-8 6.799 3.63-9 4.09-8 4.452-8 6.824 3.67-9 4.13-8 4.502-8 6.849 3.72-9 4.18-8 4.502-8	8.514 7.51-9 7.90-8 8.715-8 8.599 7.57-9 7.96-8 8.715-8 8.624 7.64-9 8.02-8 8.784-8 8.649 7.71-9 8.08-8 8.854-8
1.474	9.1-14 2.1-13 3.01-13 1.0-13 2.6-13 3.60-13 1.1-13 5.2-13 6.33-13	3.274 1.6-10 1.23-9 1.395-9 3.299 1.7-10 1.29-9 1.454-9 3.324 1.7-10 1.37-9 1.538-9	5.074 1.24-9 1.49-8 1.615-8 5.099 1.26-9 1.52-8 1.646-8 5.124 1.29-9 1.55-8 1.680-8	6.874 3.76-9 4.23-8 4.602-8 6.899 3.81-9 4.27-8 4.653-8 6.924 3.85-9 4.32-8 4.704-8	8.674 7.77-9 8.15-8 8.923-8 8.699 7.84-9 8.21-6 8.993-8 8.724 7.91-9 8.27-8 9.064-6
1.549	1.2-13 9.2-13 1.04-12 1.3-13 1.0-12 1.17-12 1.4-13 1.1-12 1.25-12	3.349 1.7-10 1.47-9 1.641-9 3.374 1.8-10 1.54-9 1.724-9 3.399 1.9-10 1.59-9 1.780-9	5.149 1.32-9 1.58-8 1.712-8 5.174 1.35-9 1.61-8 1.747-8 5.199 1.38-9 1.64-8 1.781-8	6.949 3.90-9 4.37-8 4.755-8 6.974 3.94-9 4.41-8 4.807-8 6.999 3.99-9 4.46-8 4.858-8	8.749 7.98-9 8.34-8 9.134-6 8.774 8.05-9 8.40-8 9.205-6 8.799 8.12-9 8.46-8 9.276-8
1.649	1.6-13 1.2-12 1.31-12 1.9-13 1.2-12 1.38-12 2.2-13 1.2-12 1.44-12	3.424 1.9-10 1.63-9 1.820-9 3.449 2.0-10 1.66-9 1.864-9 3.474 2.1-10 1.70-9 1.908-9	5.224 1.41-9 1.67-8 1.814-8 5.249 1.44-9 1.70-8 1.848-8 5.274 1.47-9 1.74-8 1.883-8	7.024 4.03-9 4.51-0 4.910-0 7.049 4.06-9 4.55-8 4.962-8 7.074 4.13-9 4.60-8 5.015-8	8.849 8.26-9 8.59-8 9.415-8 8.874 8.33-9 8.66-8 9.415-8
1.699 1.724 1.749	2.7-13 1.3-12 1.52-12 3.2-13 1.3-12 1.60-12 4.0-13 1.3-12 1.73-12	3.499 2.2-10 1.76-9 1.976-9 3.524 2.2-10 1.87-9 2.090-9 3.549 2.3-10 2.02-9 2.253-9	5.299 1.50-9 1.77-0 1.918-0 5.324 1.53-9 1.80-8 1.953-8 5.349 1.56-9 1.83-8 1.988-8	7.124 4.22-9 4.70-8 5.121-8 7.149 4.27-9 4.70-8 5.121-8 7.149 4.27-9 4.75-8 5.174-8	8.949 8.48-9 8.79-8 9.635-8 8.949 8.48-9 8.79-8 9.635-8 8.949 8.55-9 8.85-8 9.708-8
1.17	5.7-13 1.4-12 1.94-12 7.9-13 1.4-12 2.20-12 8.7-13 1.5-12 2.36-12	3.574 2.4-10 2.19-9 2.927-9 3.599 2.5-10 2.37-9 2.626-9 3.624 2.7-10 2.57-9 2.843-9	5.399 1.61-9 1.90-8 2.059-8 5.424 1.64-9 1.93-8 2.095-8	7.199 4.36-9 4.84-8 5.281-8 7.224 4.41-9 4.89-8 5.335-8	8.999 8.69-9 8.98-8 9.854-8 9.024 8.77-9 9.05-8 9.928-8
1.849 1.874 1.899	9.7-13 1.7-12 2.66-12 1.1-12 4.3-12 5.39-12 1.2-12 4.5-12 5.73-12	3.649 2.9-10 2.72-9 3.011-9 3.674 3.0-10 2.66-9 3.162-9 3.699 3.2-10 2.99-9 3.306-9	5.474 1.70-9 2.00-8 2.167-8 5.499 1.73-9 2.03-8 2.204-8	7.274 4.51-9 4.99-8 5.444-8 7.299 4.56-9 5.04-8 5.499-8	9.074 8.92-9 9.18-8 1.008-7 9.099 8.99-9 9.25-8 1.015-7
1.924	1.3-12 4.6-12 5.93-12 1.5-12 4.8-12 6.26-12 2.1-12 5.2-12 7.30-12	3.724 3.3-10 3.11-9 3.446-9 3.749 3.6-10 3.24-9 3.590-9 3.774 3.7-10 3.38-9 3.750-9	5.524 1.76-9 2.06-8 2.240-8 5.549 1.79-9 2.10-8 2.278-8 5.574 1.82-9 2.13-8 2.315-8	7.324 4.01-9 5.09-8 5.554-8 7.349 4.66-9 5.14-8 5.609-8 7.374 4.71-9 5.19-8 5.665-8	9.124 9.07-9 9.32-0 1.023-7 9.149 9.14-9 9.39-8 1.030-7 9.174 9.22-9 9.45-8 1.038-7
1.999 2.024 2.049	2.6-12 5.3-12 7.96-12 3.2-12 5.6-12 8.74-12 3.8-12 5.8-12 9.64-12	3.799 3.9-10 3.55-9 3.939-9 3.824 4.1-10 3.77-9 4.181-9 3.849 4.3-10 4.05-9 4.476-9	5.599 1.85-9 2.17-8 2.352-8 5.624 1.88-9 2.20-8 2.390-8 5.649 1.91-9 2.24-8 2.428-8	7.399 4.76-9 5.25-8 5.721-8 7.424 4.61-9 5.30-8 5.777-8 7.449 4.86-9 5.35-8 5.833-8	9.199 9.29-9 9.52-0 1.045-7 9.224 9.37-9 9.59-8 1.053-7 9.249 9.45-9 9.66-8 1.060-7
2.074 2.099 2.124	4.3-12 6.2-12 1.05-11 5.0-12 6.7-12 1.17-11 6.0-12 7.5-12 1.35-11	3.874 4.4-10 4.29-9 4.730-9 3.899 4.6-10 4.51-9 4.964-9 3.924 4.7-10 4.75-9 5.218-9	5.674 1.95-9 2.27-8 2.467-8 5.699 1.98-9 2.31-8 2.505-8 5.724 2.01-9 2.34-8 2.544-8	7.474 4.91-9 5.40-8 5.890-8 7.499 4.96-9 5.45-8 5.947-8 7.524 5.02-9 5.50-8 6.004-8	9.274 9.22-9 9.13-0 1.000-7 9.299 9.60-9 9.80-8 1.076-7 9.324 9.68-9 9.87-8 1.083-7
2.149	7.8-12 9.2-12 1.69-11 1.0-11 1.2-11 2.17-11 1.3-11 1.9-11 3.16-11	3.949 4.8-10 4.94-9 5.426-9 3.974 5.0-10 5.07-9 5.563-9 1.999 5.1-10 5.15-9 5.661-9	5.749 2.04-9 2.38-8 2.583-8 5.774 2.07-9 2.42-8 2.623-8 5.799 2.11-9 2.45-8 2.662-8	7.549 5.07-9 5.55-8 6.062-8 7.574 5.12-9 5.61-8 6.119-8 7.599 5.17-9 5.66-8 6.177-8	9.349 9.76-9 9.94-8 1.091-7 9.374 9.84-9 1.00-7 1.099-7 9.399 9.92-9 1.01-7 1.107-7
2.224	1.5-11 2.2-11 3.66-11 1.6-11 2.3-11 3.89-11 1.7-11 2.4-11 4.06-11	4.024 5.4-10 5.21-9 5.751-9 4.049 5.6-10 5.29-9 5.850-9 4.074 5.9-10 5.38-9 5.971-9	5.824 2.14-9 2.49-8 2.702-8 5.849 2.17-9 2.52-8 2.742-8 5.874 2.21-9 2.56-8 2.782-8	7.624 5.23-9 5.71-8 6.235-8 7.649 5.28-9 5.77-8 6.294-8 7.674 5.34-9 5.82-8 6.353-8	9.42400-9 1.01-7 1.115-7 9.449 1.01-8 1.02-7 1.122-7 9.474 1.02-8 1.03-7 1.130-7
2.299	1.7-11 2.5-11 4.24-11 1.8-11 2.7-11 4.53-11 1.9-11 3.2-11 5.05-11	4.099 6.1-10 5.56-6 6.170-9 4.124 6.2-10 5.78-9 6.403-9 4.149 6 4-10 5.92-9 6.563-9	5.899 2.24-9 2.60-8 2.823-8 5.924 2.27-9 2.64-8 2.864-8 5.949 2.31-9 2.67-8 2.905-8	7.699 5.39-9 5.87-8 6.412-8 7.724 5.44-9 5.93-8 6.471-8 7.749 5.50-9 5.98-8 6.530-8	9.499 1.02-8 1.04-7 1.138-7 9.524 1.03-8 1.04-7 1.146-7 9.549 1.04-8 1.05-7 1.154-7
2.376	2.1-11 3.4-11 5.45-11 2.2-11 3.6-11 5.76-11 2.4-11 3.6-11 5.76-11	4.174 6.6-10 6.06-9 6.725-9 4.199 6.8-10 6.21-9 6.894-9 4.224 7.0-10 6.39-9 7.091-9	5.974 2.34-9 2.71-8 2.946-8 5.999 2.38-9 2.75-8 2.988-8 6.024 2.41-9 2.79-8 3.030-8	1.174 5.55-9 6.03-8 6.590-8 7.799 5.61-9 6.09-8 6.650-8 7.824 5.67-9 6.14-8 6.711-8	9.574 1.05-8 1.06-7 1.162-7 9.599 1.06-8 1.06-7 1.170-7 9.624 1.07-8 1.07-7 1.178-7
2.449	2.5-11 4.1-11 6.58-11 2.5-11 7.2-11 9.68-11 2.5-11 7.2-11 9.68-11	4.249 7.1-10 6.66-9 7.368-9 4.274 7.2-10 6.97-9 7.690-9 4.200 7.3-10 7.26-9 7.690-9	6.049 2.45-9 2.83-8 3.072-8 6.074 2.48-9 2.87-8 3.114-8 6.099 2.52-9 2.90-8 3.157-8	7.849 5.72-9 6.20-8 6.771-8 7.874 5.78-9 6.25-8 6.832-8 7.899 5.84-9 6.31-8 6.893-8	9.649 1.07-8 1.08-7 1.186-7 9.674 1.08-8 1.09-7 1.194-7 9.694 1.09-8 1.09-7 1.203-7
2.524	2.8-11 9.7-11 1.25-10 2.9-11 1.3-10 1.58-10	4.324 7.5-10 7.48-9 8.227-9 4.349 7.6-10 7.73-9 8.496-9	6.124 2.55-9 2.94-8 3.200-8 6.149 2.59-9 2.98-8 3.243-8 6.149 2.59-9 2.98-8 3.243-8	7.924 5.89-9 6.37-8 6.955-8 7.949 5.95-9 6.42-8 7.016-8 7.949 5.95-9 6.42-8 7.016-8	9.724 1.10-8 1.10-7 1.211-7 9.749 1.11-8 1.11-7 1.219-7 0 775 1 12-8 1.12-7 1.219-7
2.599	3.1-11 2.5-10 2.82-10 3.2-11 2.6-10 2.82-10 3.2-11 2.6-10 2.89-10	4.399 7.9-10 8.44-9 9.225-9	6.199 2.66-9 3.06-8 3.330-8 6.224 2.70-9 3.10-8 3.373-8	7.999 6.07-9 6.53-8 7.141-8	9.799 1.13-8 1.12-7 1.236-7 9.824 1.13-8 1.13-7 1.24-7 6.846 1.13-8 1.13-7 1.24-7
2.674	3.8-11 2.7-10 3.03-10 4.2-11 2.8-10 3.18-10	4.474 8.2-10 9.30-9 1.012-8 4.499 8.3-10 9.42-9 1.025-8	6.274 2.78-9 3.18-8 3.462-8 6.299 2.81-9 3.23-8 3.507-8	8.074 6.24-9 6.70-8 7.329-8 8.099 6.30-9 6.76-8 7.329-8	9.874 1.15-8 1.15-7 1.261-7 9.899 1.16-8 1.15-7 1.261-7 9.894 1.17-8 1.15-7 1.267-7
2.749	4.5-11 4.5-10 4.93-10 4.6-11 4.6-10 5.06-10	4.549 8.5-10 9.84-9 1.040-8 4.574 8.5-10 9.84-9 1.069-8 4.574 8.6-10 1.02-8 1.105-8	6.349 2.89-9 3.31-8 3.596-8 6.374 2.93-9 3.35-1 3.642-8	8.149 6.42-9 6.88-8 7.520-8 8.174 6.48-9 6.94-8 7.520-8 8.174 6.48-9 6.94-8 7.544-8	9.949 1.18-8 1.17-7 1.206-7 9.974 1.19-8 1.18-7 1.294-7 9.904 1.20-8 1.18-7 1.294-7
2.144	9.0-11 9.7-10 5.12-10	9.749 0.0-10 1.05-0 1.139_8	0.199 2.9/-9 1.19-0 1.00/-0	0.133 0.77-3 0.33-0 (.040-0	

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# TABLE X <sup>17,18</sup>O( $\alpha$ ,n) NEUTRON PRODUCTION IN CLEAN UO<sub>2</sub> FUEL BY ALPHA PARTICLES BELOW 10 MeV

0.000 0. 0. 0. 2.824 4.7-11 4.7-10 5.17-10 4.624 8.9-10 1.07-8 1.158-8 6.424 2.96-9 3.37-8 3.667-8 8.224 6.48-9 5.91- 1.139 0. 0. 2.849 4.8-11 4.8-10 5.30-10 4.649 9.1-10 1.10-8 1.192-8 6.449 2.99-9 3.47-8 3.667-8 8.224 6.48-9 5.91- 1.141 0. 0. 0. 2.874 4.9-11 5.10 5.53-10 4.649 9.1-10 1.10-8 1.192-8 6.449 2.99-9 3.45-8 3.712-8 8.249 6.56-9 7.02- 1.161 0.0- 0 1.5-14 1.53-14 2.899 5.2-11 5.7-10 6.25-10 4.699 9.4-10 1.18-8 1.257-8 6.499 3.07-9 3.50-8 3.603-8 8.299 6.66-9 7.02- 1.860 0.0- 0 1.5-14 1.76-14 2.924 5.7-11 6.5-10 7.14-10 4.749 9.8-10 1.18-8 1.257-8 6.499 3.107-9 3.50-8 3.803-8 8.299 6.66-9 7.02- 1.860 0.0- 0 1.8-14 1.76-14 2.924 5.7-11 6.5-10 7.14-10 4.749 9.8-10 1.21-8 1.303-8 6.5549 3.15-9 3.58-8 3.895-8 8.394 6.72-9 7.20- 1.210 0.0- 0 2.6-14 2.63-14 2.974 7.0-11 7.6-10 8.33-10 4.749 9.8-10 1.22-8 1.303-8 6.574 3.19-9 3.56-8 3.895-8 8.394 6.84-9 7.26- 1.261 0.0- 0 2.6-14 2.63-14 2.974 7.0-11 7.6-10 8.33-10 4.774 9.0-10 1.22-8 1.323-8 6.579 3.15-9 3.56-8 3.895-8 8.394 6.84-9 7.26- 1.261 0.0- 0 2.6-14 2.63-14 2.974 7.0-11 7.8-10 8.33-10 4.774 9.0-10 1.22-8 1.323-8 6.579 3.15-9 3.56-8 3.995-8 8.394 6.84-9 7.26- 1.261 0.0-0 2.6-14 2.63-14 2.974 7.0-11 7.6-10 8.33-10 4.774 9.0-10 1.22-8 1.323-8 6.579 3.15-9 3.56-8 3.995-8 8.394 6.80-9 7.26- 1.261 0.0-0 2.6-14 2.63-14 2.990-9 0.90-17 3.20-10 4.774 9.0-10 1.22-8 1.323-8 6.579 3.15-9 3.56-8 3.995-8 0.990-9 7.26- 1.261 0.0-0 2.6-14 2.63-14 2.990-9 7.4-11 7.6-10 8.93-10 1.21-8 1.323-8 6.579 3.15-9 3.56-8 3.995-8 0.990-9 7.26- 1.261 0.0-0 2.6-14 2.63-14 2.990-9 7.90-10 4.774 9.0-10 1.22-8 1.323-8 6.579 3.15-9 3.56-8 3.995-8 0.990-9 7.90-9 7.26- 1.261 0.0-0 2.6-14 2.63-14 2.990-9 7.90-

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# TABLE XI

17,180( $\alpha$ ,n) NEUTRON PRODUCTION IN SPENT UO<sub>2</sub> FUEL BY ALPHA PARTICLES BELOW 10 MeV

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# TABLE XII <sup>17</sup>, <sup>18</sup> $O(\alpha,n)$ NEUTRON PRODUCTION IN CLEAN (U,Pu)O<sub>2</sub> FUEL BY ALPHA PARTICLES BELOW 10 MeV

		**NEUTKUNS-PEK-ALPHA* N.MEV 0-17 0-18 TGTAL	**NEUTHONS-PER-ALPHA* E,MEV 0-17 0-18 TOTAL	**NEUTRUNS-PER-ALPHA* E.MEV 0-17 G-18 TUTAL	**NEUTHONS-PER-ALPHA* E.MEV 0-17 0-18 TUTAL	**NEUTRUNS-PER-ALPHA* 5,MEV G-17 U-18 TUTAL
2.349 1.0-11 2.2-11 3.0-11 4.149 6.2-10 3.26-9 6.30-9 5.949 2.26-9 2.00-8 2.825-8 7.149 5.41-9 5.88-8 9.428-8 9.549 1.02-8 1.03-7 1.13- 2.374 2.1-11 3.4-11 5.43-11 4.174 6.6-10 6.00-9 6.657-9 5.974 2.31-9 2.67-8 2.906-8 7.774 5.46-9 5.94-8 6.483-8 9.574 1.03-8 1.03-7 1.14- 2.399 2.3-11 3.6-11 5.77-11 4.190 6.8-10 6.15-9 6.823-9 5.999 2.34-9 2.34-8 2.906-8 7.774 5.46-9 5.94-8 6.483-8 9.574 1.03-8 1.03-7 1.14- 2.484 2.4-11 3.8-11 6.15-11 4.224 6.9-10 6.33-9 7.018-9 6.024 2.38-9 2.71-8 2.988-8 7.829-8 5.57-9 6.08-8 6.542-8 9.654 1.05-8 1.05-7 1.156- 2.484 2.5-11 4.1-11 6.57-11 4.224 6.9-10 6.50-9 7.292-9 6.019 2.31-9 2.475-8 2.988-8 7.829-8 6.601-8 9.654 1.05-8 1.05-7 1.156- 2.484 2.5-11 4.1-11 6.57-11 4.224 6.9-10 6.50-9 7.292-9 6.019 2.31-9 2.475-8 2.988-8 7.829-8 6.484 5.680-8 9.654 1.05-8 1.05-7 1.156- 2.484 2.5-11 4.1-11 6.57-11 4.224 6.9-10 6.50-9 7.292-9 6.019 2.31-9 2.479-8 7.829-8 7.829-8 6.484 5.680-8 9.654 1.05-8 1.05-7 1.156- 2.484 2.5-11 4.1-11 9.55-11 4.274 7.1-10 6.50-9 7.292-9 6.019 2.34-9 2.45-8 2.988-8 7.829-8 7.829 6.10-8 9.654 1.05-8 1.05-7 1.156- 2.484 2.5-11 4.1-11 9.55-11 4.274 7.1-10 6.50-9 7.292-9 6.019 2.34-9 2.45-8 2.988-8 7.829-8 7.824 5.68-9 6.10-8 9.654 1.05-8 1.05-7 1.156- 2.484 2.5-11 4.1-11 9.55-11 4.274 7.1-10 6.50-9 7.292-9 6.019 2.34-9 2.45-8 2.988-8 7.829-8 7.849 5.68-9 6.10-8 9.654 1.05-8 1.05-7 1.156- 2.484 2.5-11 4.1-11 9.55-11 4.274 7.1-10 6.50-9 7.292-9 6.019 2.34-9 2.45-8 3.029-8 7.849 5.68-9 6.10-8 9.654 1.05-8 1.05-7 1.156- 2.484 2.5-11 4.1-11 9.55-11 4.274 7.1-10 6.50-9 7.292-9 6.019 2.34-9 2.45-8 3.029-8 7.849 5.68-9 6.10-8 9.674 1.05-8 1.05-7 1.156- 3.444 2.5-11 4.1-11 9.55-11 4.274 7.1-10 6.50-9 7.292-9 6.019 2.34-9 2.45-8 3.029-8 7.849 5.68-9 6.10-8 9.674 1.05-8 1.00-7 7.1172-10-10-10-10-10-10-10-10-10-10-10-10-10-	2.524 2.611 9.6-11 1.24-10 4.329 7.4-10 7.80-9 7.908-9 6.099 2.80-9 2.60-8 3.152-8 7.992 5.80-9 6.26-8 6.800-8 9.724 1.08-8 1.04-7 1.188-1 2.549 2.9-11 1.3-10 1.57-10 4.324 7.4-10 7.65-9 8.405-9 6.149 2.55-9 7.94-8 3.197-8 7.949 5.85-9 6.32-8 6.901-8 9.749 1.09-8 1.09-7 1.196-7 1.204-7 2.599 3.1-11 2.5-10 2.56-10 4.374 7.7-10 7.95-9 8.405-9 6.149 2.55-9 7.94-8 3.197-8 7.949 5.85-9 6.32-8 6.901-8 9.749 1.09-8 1.09-7 1.196-7 1.204-7 2.599 3.1-11 2.5-10 2.56-10 4.374 7.7-10 7.97-9 8.730-9 6.179 4.55-9 7.949 5.85-9 6.32-8 6.901-8 9.749 1.09-8 1.09-7 1.196-7 1.204-7 2.599 3.1-11 2.5-10 2.56-10 4.374 7.7-10 7.97-9 8.730-9 6.179 2.65-9 2.94-8 3.197-8 7.949 5.85-9 6.32-8 6.901-8 9.749 1.09-8 1.09-7 1.204-7 2.599 3.1-11 2.5-10 2.56-10 4.374 7.7-10 7.97-9 8.730-9 6.179 2.65-9 3.02-8 3.203-8 7.999 5.97-9 6.37-8 6.561-8 9.774 1.10-8 1.09-7 1.204-7 2.599 3.1-11 2.5-10 2.56-10 2.87-10 4.349 7.6-10 8.35-9 9.125-9 6.199 2.63-9 3.02-8 3.202-8 5.907-9 6.37-8 7.052-8 9.799 1.10-8 1.10-7 1.224-7 2.599 3.1-11 2.5-10 2.87-10 4.349 7.9-0 8.35-9 9.125-9 6.32-8 6.029 8.360-8 7.392-8 6.02-9 6.34-8 7.052-8 9.929 1.10-8 1.10-7 1.224-7 2.624 3.4-11 2.6-10 2.87-10 4.849 8.0-10 8.99-9 9.766-9 6.226 2.60-9 3.02-8 3.302-8 8.049 6.08-9 6.34-8 7.054-8 9.849 1.12-8 1.12-7 1.224-7 2.644 3.8-11 2.6-10 2.97-10 4.849 8.0-10 8.99-9 9.786-9 6.274 2.74-9 3.18-8 3.43-8 8.049 6.08-9 6.54-8 7.145-8 9.849 1.12-8 1.12-7 1.224-7 2.644 3.8-11 2.6-10 3.02-10 4.478 810 9.19-9 1.00-8 6.274 2.74-9 3.18-8 3.43-8 8.049 6.08-9 6.54-8 7.207-8 9.874 1.12-8 1.12-7 1.224-7 2.644 3.8-11 2.6-10 3.02-10 4.478 8.2-10 9.19-9 1.00-8 6.274 2.74-9 3.18-8 3.45-8 8.049 6.08-9 6.54-8 7.207-8 9.874 1.12-8 1.12-7 1.224-7 2.644 3.8-11 2.6-10 3.02-10 4.478 8.2-10 9.19-9 1.00-8 6.274 2.74-9 3.18-8 3.43-8 8.049 6.08-9 6.54-8 7.207-8 9.874 1.12-8 1.12-7 1.224-7 2.644 3.8-11 2.6-10 3.02-10 4.478 8.2-10 9.39-9 7.746-9 3.18-8 3.43-8 8.049 6.08-9 6.54-8 7.207-8 9.874 1.13-8 1.12-7 1.224-7 2.644 3.8-11 2.6-10 3.02-10 4.479 8.249 2.749 3.18-8 3.449-8 8.049 6.08-9 6.54-8 7.207-8 9.874 1.12-8 1	**NLUTKONS-PEK-ALPHA*           b. MEY         U-17         U-18         UTAL           0.000         0.         0.         0.         0.           1.199         0.         0.         0.         0.           1.199         0.         0.         0.         0.           1.181         0.         0.         0.         0.           1.181         0.         0.         1.5-14         1.79-14           1.211         0.0         0.2.6-14         2.64-14         2.64-14           1.2261         0.0         0.2.6-14         2.64-14         3.26-14           1.266         0.0         0.0         3.1-14         3.20-14         3.26-14           1.261         0.0         0.3.1-14         3.66-14         3.3-14         3.32-14           1.311         1.0-16         3.7-14         3.26-14         3.22-14         3.311           1.342         2.4-15         8.1-14         0.3-13         1.34-13           1.312         1.0-14         1.0-13         1.14-13         1.26-13           1.344         1.2-14         1.1-13         1.26-13         1.36-12           1.446         1.2-13         1.0-12 </td <td>***         HEUTHONS-PER-ALPHA*           2.824         4.7-11         4.7-10         5.19-10           2.824         4.7-11         4.7-10         5.19-10           2.824         4.7-11         4.7-10         5.19-10           2.824         4.7-11         4.7-10         5.19-10           2.874         5.0-11         5.2-10         5.65-10           2.874         5.0-11         6.5-17-10         6.55-10           2.974         5.0-11         7.7-10         8.36-10           2.974         5.0-11         7.7-10         8.36-10           2.974         7.4-11         8.0-10         8.36-10           3.024         8.1-10         9.4-10         9.5-11           3.024         9.5-11         8.1-10         9.4-10           3.024         9.5-11         8.10         1.00         9.7-10           3.024         1.2-10         8.5-10         9.7-10         1.360-10         9.7-10           3.024         1.3-10         9.4-10         9.4-10         9.4-10         9.4-10           3.11         7.10         1.36-9         1.260-9         9.27-10           3.24         1.7-10         1.36-9         1.260-9</td> <td>**NEUTRONS-PER-ALPHA*           L.HEV         0-17         0-18         TUTAL           4.624         8.9-10         1.07-8         1.162-8           8.649         9.1-10         1.1-8         1.27-8           8.649         9.1-10         1.1-8         1.231-8           8.659         0.8-10         1.7-8         1.262-8           8.749         0.8-10         1.7-8         1.262-8           8.724         0.6-10         1.7-8         1.262-8           8.724         0.6-10         1.2-8         1.308-3           8.724         0.6-10         1.23-8         1.308-3           8.774         .00-19         1.26-8         1.368-8           8.749         0.04-9         1.308-1         1.452-8           8.889         1.00-9         1.308-1         1.458-8           8.889         1.09-9         1.308-1         1.458-8           8.899         1.19-9         1.458-8         1.568-8           9.024         1.99-9         1.458-8         1.568-8           9.024         1.99-9         1.458-8         1.568-8           9.024         1.99-9         1.458-8         1.568-8           9.024</td> <td>************************************</td> <td>•••         •••         •         •</td>	***         HEUTHONS-PER-ALPHA*           2.824         4.7-11         4.7-10         5.19-10           2.824         4.7-11         4.7-10         5.19-10           2.824         4.7-11         4.7-10         5.19-10           2.824         4.7-11         4.7-10         5.19-10           2.874         5.0-11         5.2-10         5.65-10           2.874         5.0-11         6.5-17-10         6.55-10           2.974         5.0-11         7.7-10         8.36-10           2.974         5.0-11         7.7-10         8.36-10           2.974         7.4-11         8.0-10         8.36-10           3.024         8.1-10         9.4-10         9.5-11           3.024         9.5-11         8.1-10         9.4-10           3.024         9.5-11         8.10         1.00         9.7-10           3.024         1.2-10         8.5-10         9.7-10         1.360-10         9.7-10           3.024         1.3-10         9.4-10         9.4-10         9.4-10         9.4-10           3.11         7.10         1.36-9         1.260-9         9.27-10           3.24         1.7-10         1.36-9         1.260-9	**NEUTRONS-PER-ALPHA*           L.HEV         0-17         0-18         TUTAL           4.624         8.9-10         1.07-8         1.162-8           8.649         9.1-10         1.1-8         1.27-8           8.649         9.1-10         1.1-8         1.231-8           8.659         0.8-10         1.7-8         1.262-8           8.749         0.8-10         1.7-8         1.262-8           8.724         0.6-10         1.7-8         1.262-8           8.724         0.6-10         1.2-8         1.308-3           8.724         0.6-10         1.23-8         1.308-3           8.774         .00-19         1.26-8         1.368-8           8.749         0.04-9         1.308-1         1.452-8           8.889         1.00-9         1.308-1         1.458-8           8.889         1.09-9         1.308-1         1.458-8           8.899         1.19-9         1.458-8         1.568-8           9.024         1.99-9         1.458-8         1.568-8           9.024         1.99-9         1.458-8         1.568-8           9.024         1.99-9         1.458-8         1.568-8           9.024	************************************	•••         •••         •         •

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Fig. 5.  $^{17,18}$ O( $\alpha$ ,n) neutron production by decay alphas in LWR irradiated UO<sub>2</sub> fuel.

# TABLE XIII

# NEUTRON PRODUCTION FROM ACTINIDE DECAY IN UO $_{\rm 2}$ fuel

			DECAY	DE-		ONS PER I	ECRY+++
	NUCLIDE	(SECONDS)	(MEV)	REF	IN UD2	FISSION	TOTAL
;		=========	======	===		========	
	80-HG-206	4.89000+2	0.5274	<b>H</b>	0.	0.	0.
	81-TL-206	2.50980+2	0.5402	Ħ	0.	0.	0.
	82-FB-206	STABLE	0.	_	0.	0.	0.
	81-TL-207	2.87400+2	0.5194	н	U.	U.	U.
	82-PB-207	SIMBLE	0.0700	-	0.	0.	0.
	81-11-208	1.84200+2	3.7702	Ð	0.	0.	0.
	82-PB-208	STABLE	0.	-	0.	0.	0.
	81-TL-209	1.32000+2	2.8315	A.	· <b>0</b> .	0.	0.
	82-FB-209	1.17108+4	0.2234	A	0.	0.	0.
	83-BI-209	6.3115+25	0.	<b>A</b>	0.	0.	Û.
	81-TL-210	7.80000+1	4.2765	<b>H</b>	0.	0.	7.00 -05
	82-PB-210	7.02472+8	0.0441	Ħ	5.68 -17	0.	5.68 -17
	83-BI-210	4.33123+5	0.3899	A	1.56 -14	0.	1.16 -14
	84-FD-210	1.19557+7	5.4076	Ĥ	1.87 -08	0.	1.87 -08
	82-PB-211	2.16600+3	0.5353	A	0.	0.	0.
	83-BI-211	1.29000+2	6.7881	A	3.88 -08	0.	3.88 -08
	84-PD-211	0.5160000	7.5942	<u> </u>	5.64 -08	0.	5.64 -08
	82-PB-212	3.83040+4	0.3180	В	U.	U.	0.
	83-BI-212	3,63600+3	2.9030	A	1.076-08	0.	1.076-08
	84-PD-212	2.96000-7	8,9536	A	8.94 -08	0.	8.94 -08
	83-BI-213	2.73540+3	0.7172	A	5.85 -10	0.	5.85 -10
	84-PO-213	4.20000-6	8.5360	A	7.86 -08	0.	7.86 -08
	82-PB-214	1.60800+3	0.5389	A	0.	Û.	0.
	83-BI-214	1.18200+3	2.1923	A	4.39 -12	0.	4.39 -12
	84-PD-214	1.63700-4	7.8337	A	6.19 -08	0.	6.19 -08
	83-BI-215	4.44000+2	0.8445	Ĥ	Û.	0.	0.
	84-PD-215	1.77800-3	7.5265	A	5.52 -08	0.	5.52 -08
	85-AT-215	1.00000-4	8.1780	A	6.98 -08	0.	6.98 -08
	84-PD-216	0.1500000	6.9064	B	4.28 -08	0.	4.28 -08
	85-AT-217	0.0323000	7.2004	н	4.85 -08	υ.	4.85 -08
	86-RN-217	5.40000-4	7.8880	A	6.32 -08	0.	6.32 -08
	84-PD-218	1.83000+2	6.1149	A	2.909-08	0.	2.909-08
	85-AT-218	1.7500000	6.8830	A	4.14 -08	0.	4.14 -08
	86-RN-218	0.0350000	7.2664	A	4.99 -08	0.	4.99 -08
	85-AT-219	5.40000+1	6.2165	<b>H</b>	3.26 -08	0.	3.26 -08
	86-RN-219	3.9600000	6.9463	н	4.25 -08	0.	4.25 -08
	86-RN-220	5.56000+1	6.4048	B	3.39 -08	0.	3.39 -08
	87-FR-221	2.88000+2	6.4580	Ĥ	3.45 -08	0.	3.4508
	86-RN-222	3.30351+5	5.5905	<b>H</b>	2.129-08	0.	2.129-08
	87-FR-222	8.64000+2	0.7450	A	2.45 -11	0.	2.45 -11
	88-RA-222	3.80000+1	6.6760	Ĥ	3.846-08	U.	3.846-08
	87-FR-223	1.30800+3	0.4559	н	7.65 -13	U	r.60 -13
	90_00 000	0 07040.F		~	0.00.00		o oo
	98- <b>88-88</b> -224	3.16224+5	5.7902	רת פו	2 40 -08	0. 0	2.39 -08
	88-RA-225	1.27872+6	0.1433	P A	0. 0.	0. 0	0 - 08
	89-80-225	8.64000+5	5.9354	Ä	2.57 -08	0.	2.57 -09
	88-RA-226	5.0461+10	4.8708	Ĥ	1.304-08	ō.	1.304-08
	89-AC-226	1.04400+5	0.4099	6	1.24 -12	Ú.	1.24 -12

# TABLE XIII (cont.)

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		DECAY	DE-	++++NEUTF	RONS PER D	ECAY++++
	HALF-LIFE	ENERGY	CAY	ALPHA, N	SPONT.	
NUCLIDE	(SECONDS)	(MEV)	REF	IN UD2	FISSION	TOTAL
		<b>E</b> ==== <b>X</b>	XEE	AFCAJEEZ	TEXTETE	******
90-TH-226	1.85400+3	6.4517	A	3.42 -08	0.	3.42 -08
89-AC-227	6.87097+8	0.0878	A	2.01 -10	0.	2.01 -10
90-TH-227	1.61720+6	6.1466	A	2.72 -08	0.	2.72 -08
88-RA-228	1.82087+8	0.0146	0	Û.	Û.	0.
89-AC-228	2.20680+4	1.3696	Ĥ	0.	0.	0.
90-TH-228	6.03725+7	5.5176	B	2.004-08	0.	2.004-08
90-TH-229	2.3163+11	5.1686	A	1.391-08	0.	1.391-08
90-TH-230	2.4299+12	4.7609	B	1.207-08	1.14 -12	1.21 -08
91-PA-230	1.52928+6	0.6577	A	6.03 -13	0.	6.03 -13
92- U-230	1.79712+6	5.9928	A	2.69 -08	0.	2.69 -08
90-TH-231	9.18720+4	0.1537	B	0.	0.	0.
91-PA-231	1.0338+12	5.0601	В	1.478-08	5.75 -12	1.48 -08
92- U-231	3.62880+5	0.1017	A	1.14 -12	0.	1.14 -12
90-TH-232	4.4337+17	4.0862	B	5.52 -09	3.02 -11	5.55 -09
91-PA-232	1.13184+5	1.098	Б	Ο.	0.	0.
92- U-232	2.26263+9	5.4145	B	1.871-08	1.54 -12	1.87 -08
90-TH-233	1.33800+3	0.4422	B	0.	0.	0.
91-PA-233	2.33280+6	0.4080	В	Û.	0.	0.
92- U-233	5.0232+12	4.8978	в	1.336-08	2.29 -12	1.34 -08
90-TH-234	2.08233+6	0.1473	A	0.	0.	0.
91-PA-234	2.43000+4	2.2453	<b>A</b>	0.	0.	Û.
91-PA-234M	7.05000+1	0.8141	A	0.	0.	0.
92- U-234	7.7188+12	4.8685	в	1.299-08	2.17 -11	1.301-08
90-TH-235	4.14000+2		Ĥ	Ú.	0.	0.
91-PA-235	1.45200+3		A	0.	0.	0.
92- U-235	2.2210+16	4.6651	в	8.89 -09	3.74 -09	1.26 -08
92- U-235M	1.48080+3	0.0001	<b>A</b>	0.	0.	0.
93-NP-235	3.42230+7	0.0810	<b>A</b>	2.44 -13	0.	2.44 -13
94-PU-235	1.53600+3	5.8675	Ĥ	3.48 -12	0.	3.48 -12
92- U-236	7.3890+14	4.5809	B	9.89 -09	2.29 -09	1.218-08
93-NP-236	3.6290+12	0.3390	в	0.	0.	0.
93-NP-236M	8.10000+4	0.1353	B	0.	0.	Û.
94-PU-236	8.99688+7	5.8634	В	2.517-08	1.73 -09	2.69 -08
92- U-237	5.83200+5	0.3103	B	0.	0.	0.
93-NP-237	6.7532+13	4.9470	B	1.303-08	4.39 -12	1.303-08
94-PU-237	3.94243+6	0.0628	B	6.72 -13	0.	6.72 -13
92- U-238	1.4100+17	4.2755	в	6.64 -09	1.095-06	1.102-06
93-NP-238	1.82908+5	0.7916	B	0.	Q. (	0.
94-PU-238	2,76912+9	5.5871	B	2.124-08	4.08 -09 8	2.532-08
92- U-239	1.41000+3	0.4650	B	0.	0.	0.
93-NP-239	2.03385+5	0.4180	B	0.	<b>Q.</b>	0.
94-PU-239	7.6084+11	5.2396	B	1.664-08	9.37 -12 :	1.665-08
92- U-240	5.07600+4	0.1755	A	0.	0.	<b>0.</b>
93-NP-240	4.02000+3	1.5755	A	0.	0.	0.
93-NF-240M	4.50000+2	1.0407	Ħ	0.	0.	0.
94-PU-240	2.0670+11	5.3274	B	1.676-08	1.08 -07 :	1.25 -07
95-HM-240	1.82880+5	1.0920	B	3.74 -14	0. (	3.74 -14
96-08-240	2.31552+6	ь.3844	Ħ	3.37 -08	9.23 -08 :	1.26 -07
94-PU-241	4.63886+8	0.0054	B	3.39 -13	0. :	3.39 -13
95-HM-241	1.3639+10	5.6131	B	2.115-08	9.31 -12 8	2.116-08
96-UM-241	2.83392+6	1.1100	B	2.79 -10	0. 6	2.79 -10
94-PU-242	1.18/5+13	4.9812	R	1.406-08	1.18 -05 :	1.18 -05
90-00-242 95-0M-949M	J. 10000074	0.1744	ສ ຄ	0.00.44	U. 1 0 74 40	
	101200042	0.0001	Ð	2.CC -11	⊡•r⊶ —10 4	+.36 -10

# TABLE XIII (cont.)

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	DECAY DE- ++++NEUTRONS PER DECAY+++ HALF-LIFE ENERGY CAY ALPHA,N SPONT. NUCLIDE (SECONDS) (MEY) REF IN UD2 FISSION TOTAL								
	=========	======	===			=========			
96-CM-242 94-PU-243 95-AM-243 96-CM-243 94-PU-244 95-AM-244	1.40745+7 1.78452+4 2.3289+11 8.99372+8 2.5877+15 3.63600+4	6.2169 0.1957 5.4224 6.1598 4.6510 1.1177	B B B R B	3.07 -08 0. 1.82 -08 2.62 -08 1.083-08 0.	1.714-07 0. 5.32 -10 0. 2.875-03 0.	2.02 -07 0. 1.87 -08 2.62 -08 2.88 -03 0.			
95-AM-244M 96-CM-244 94-PU-245 95-AM-245 96-CM-245 94-PU-246	1.56000+3 5.71495+8 3.78280+4 7.38000+3 2.6744+11 9.37440+5	0.5088 5.9010 0.8103 0.3199 5.5881 0.2514	B A A B A	0. 2.582-08 0. 0. 1.948-08 0.	0. 3.623-06 0. 0. 0.	0. 3.65 -06 0. 0. 1.95 -08 0.			
95-AM-246M 96-CM-246 96-CM-247 96-CM-248 97-BK-248 97-BK-248	1.50000+3 1.4926+11 4.9229+14 1.0720+13 2.84018+8 8.46000+4	1.4433 5.4714 5.3522 4.7270  0.1684	A B B B A A	0. 1.971-08 1.466-08 1.441-08 0.	0. 8.313-04 0. 2.569-01 	0. 8.31 -04 1.47 -08 2.57 -01  0.			
98-CF-248 96-CM-249 97-BK-249 98-CF-249 96-CM-250 97-BK-250	2.88144+7 3.84900+3 2.76480+7 1.1064+10 3.5660+11 1.15812+4	6.3613 0.2932 0.0331 6.2903 1.1829	A B B B C B	3.336-08 0. 2.906-13 2.646-08  0.	9.519-05 0. 1.656-09 1.712-08 2.32 +00 0.	9.52 -05 0. 1.66 -09 4.36 -08 2.32 +00 0.			
98-CF-250 96-CM-251 97-BK-251 98-CF-251 98-CF-252 98-CF-252	4.12764+8 1.00800+3 3.33600+3 2.8338+10 8.32471+7 1.53878+6	6.1227 0.5925 0.4988 6.0260 6.0317 0.0980	8 A 8 8 8 8 8 8	2.941-08 0. 2.532-08 2.996-08 8.89 -11	2.718-03 0. 0. 0. 1.164-01 0.	2.72 -03 0. 0. 2.53 -08 1.164-01 8.89 -11			
99-ES-253 98-CF-254 99-ES-254 99-ES-254 100-FM-254 98-CF-255	1.76860+6 5.22720+6 2.38205+7 1.41480+5 1.16640+4 6.84000+3	6.7367 0.0184 6.6172 0.7351 7.2996	8 8 8 8 8 8	3.995-08 8.167-11 3.627-08 1.138-10 5.08 -08 0.	3.419-07 3.88 +00 1.193-07 1.778-07 2.34 -03 0.	3.82 -07 3.88 +00 1.56 -07 1.78 -07 2.34 -03 0.			
99-ES-255 100-FM-255 99-ES-256 100-FM-256 100-FM-257 100-FM-258	3.30912+6 7.22520+4 1.32000+3 9.45720+3 8.68320+6 3.80000-4	0.5956 7.2407 0.6169 7.0250 6.8640	A A A A A A	2.72 -09 4.75 -08 0. 4.55 -08 3.81 -08 0.	$\begin{array}{r} 1.59 & -04 \\ 8.54 & -07 \\ 0. \\ 3.69 & +00 \\ 8.09 & -03 \\ 4.03 & +00 \end{array}$	$\begin{array}{rrrr} 1.59 & -04 \\ 9.02 & -07 \\ 0. \\ 3.69 & +00 \\ 8.09 & -03 \\ 4.03 & +00 \end{array}$			
DECAY DATA REFERENCES A=TABLE DF ISDTOPES B=ENDF/B-V C=A.TOBIAS;U.K.,PRIVATE COMMUNICATION									
ADDITIONAL NOTES MISSING DATA NOTED AS 81-TL-210, NEUTRONS FROM DELAYED NEUTRON EMISSION FROM 82-PB-210 LEVELS PRODUCED IN BETA DECAY.									
92- U-235, SPONTANEOUS FISSION BRANCHING IN ENDF/B-V IS ZERO BY OMISSION. S.F. BRANCHING(2.011-9) TAKEN FROM REFERENCE A.									
97-BK-248 DECAY CHARACTERISTICS UNKNOWN.									

These values of  $R_k$  may be used with detailed calculated activity inventory to determine total neutron production within oxide fuel, using Eq. (22).

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