

Carl Buckland, H-1

October 20, 1961

W. R. Kennedy, H-6

122518

"CLOSE IN FALLOUT" FROM CASTLE BRAVO

H-6

The following measurements were made at various times at the places indicated following the March 1, 1954 detonation at Bikini Atoll. Speed of movement to all points is based on a measurement by a recording gamma meter located on Eniwetok Island, Rongerik Atoll. The meter indicated start of arrival at H + 7-3/4 hours, with an estimated peak reading at H + 8-3/4 hours. The distance is 135 nautical miles, so a mean speed of 17 knots has been used in the calculations. Extrapolated decay has been based on the  $T^{1.2}$  rate. No allowance has been made for weathering prior to measurement, so the values are probably low.

The bomb was a surface burst of 15 Megatons, 50% fission. The "hot line" of the fallout pattern was somewhat to the north of all the locations listed below. Kabelle Island, Rongelap Atoll, is the closest to the "hot line", but still probably some distance from it.

Island Location	Date-time	Reading mr/hr	Distance sea miles	Estimated Arrival time	Estimated Peak reading	Estimated D $\infty$
Rongelap	D + 7	375	103	H + 6	20 R/hr	600 R
Kabelle	D + 25	1000	108	H + 6.35	235 R/hr	7500 R
Eniwetok	D + 7	280	135	H + 8	11 R/hr	440 R
Utirik	D + 3	170	276	H + 16.2	1 R/hr	81 R

Original Signed By  
WILLIAM R. KENNEDY

Wm. R. Kennedy

WRK:bg

cc: O.W. Stopinski  
E. Benis  
File

RG 326 US ATOMIC ENERGY  
COMMISSION F-23  
Location LAW B-195  
Collection Records Center  
Folder BRAVO

II

TROPO

MEAN WIND

11.5RAND TIME  
VARIANT

BRAVO

DATE TIME OF POST

TEAPOT

FOR DT

Ymost

LAYER	HODO		$\frac{\ln R}{\sigma}$	$\frac{q_1}{1.05} \Sigma$
	$\theta$	R		
93.75°	151	146	2.76	212
81.25°	94	187	3.26	332
68.75°	90	229	3.87	380
56.25°	89	250	4.24	112
43.75°	89	212	4.47	42
31.25°	95	124	41.54	15
18.75°				
6.25°				

x	TABLE OF W			$\theta_0 = 95$
	50	100	150	
1	21.00	54.0	36.0	+11
2	15.60	48.0	63.0	+4
3	18.10	15.60	7.00	0
4	6.300	3.000	1.000	-1
5	12.00	5.00	12.00	-1
6	3.50	-	-	+5
$\Sigma W$	51.650	28.770	19.340	

TABLE OF W ( $\theta - \theta_0$ )			
1	97	60	43
2	62	36	25
3	-	-	-
4	-6	-3	-2
5	-2	-1	-
6	2	-	-
$\Sigma (\theta - \theta_0)$	153	92	66
$(\bar{\theta} - \theta_0) = \bar{\theta} - \theta_0$	2.0	3.2	3.4
$\theta_0$	90	90	90
$\bar{\theta}$	92	93.2	93.4

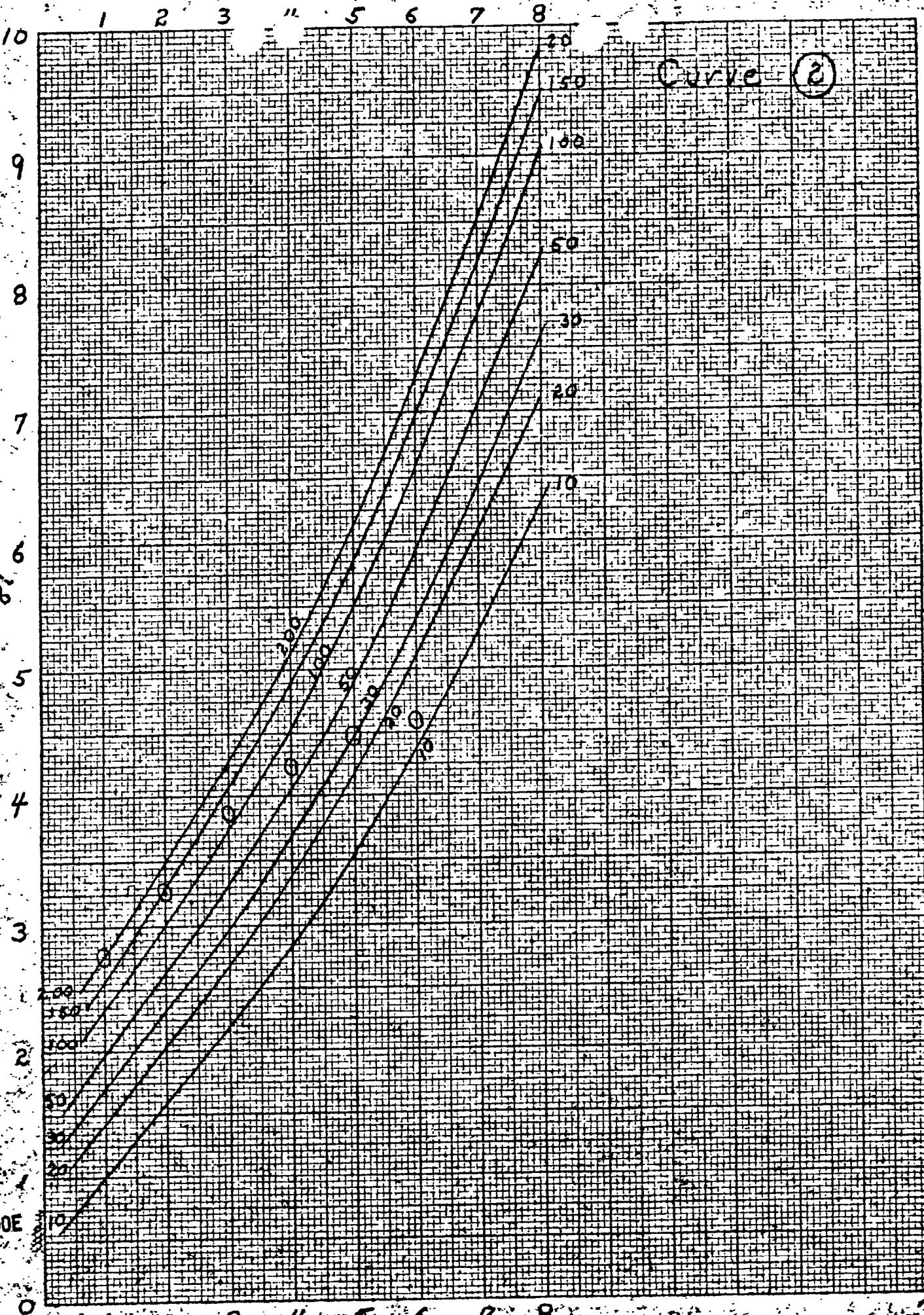
x	50	100	150
$\sigma_a$	4.24	2.44	1.60
$\sigma_\theta$	6.31	4.94	4.59
$\Sigma W$	39,600	14,200	6,750
$\frac{\partial W}{\partial \theta} = D P e k$	11,900	3,700	1,620
width (mi) of $\Sigma R$			
width (mi) of $\Sigma R$			

x	50	100	150
1	880	650	480
2	250	144	100
3	-	-	-
4	6	3	2
5	2	1	-
6	9	-	-
$\Sigma W(\theta - \theta_0)^2$	1150	810	580
$(\bar{\theta} - \theta_0)^2$	300	300	225
$= \Sigma W(\theta - \bar{\theta})^2$	850	510	355
$\div (\Sigma W) : (\sigma_\theta)^2$	16.4	10.4	18.4
$+ \sigma_\theta^2$	23.4	19.5	25.5

No. 95911. 10 x 10 to the half inch, 5th lines accent.  
Engineering, 7 x 10 in.  
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$$\ln x - \ln 0.822$$



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